## Useful data for Noise Prototype Quad assembly

## 1. DESIGN MASS FOR ALL MASSES

Top mass: 22kg

UI mass: 22kg
Penultimate mass: $\quad 40 \mathrm{~kg}$
Test mass: 40kg

Once the mass of all the glass masses is known these numbers will be revised and the mass of the pen-re mass will be set as flows:

TTM = test mass
PTM = Penultimate test mass
TRM = Test reaction mass
PRM = Penultimate reaction mass

## 2. BLADE TIP POSITIONS

The blade tips in the TM and UIM should be central in the blade tip stop ( 5 mm from either side).

The Height of the blade tips is more complex. It is belived that the correct blade top to blade gate mark dimensions (Final A) are as follows:

| Top mass | 6.6 mm |
| :--- | :--- |
| UI mass | 12 mm |

If these dimensions turn out to be incorrect then the correct values should be able to be derived from the following:


|  | A | B | C | Target C <br> dimension * |
| :--- | :--- | :--- | :--- | :--- |
| Top Mass | 5.0 | 1.28 | 2.28 | 3.9 |
| UI Mass | 4.6 | -3.50 (no prism) | -2.5 | 4.12 |

*dimensions of target C come from T060042-01
So the target blade top to gate dimension (Final A) are derived as follows; Target C C + A= Final A

## 3. MASSES REQUIRED TO DEFLECT BLADES

When the blades are loaded with a vertical mass to set the blade tip positions during mass assembly the mass needs to be adjusted to allow for the loading wire being vertical and the final wire angled.

|  | Angle form vertical (+ is toward blade root) theta | Mass that will ultimately be upon blade (M) | Vertical load required to deflect blade as masses will* |
| :---: | :---: | :---: | :---: |
| Top Wire | $21.07^{\circ}$ | $62 \mathrm{~kg} \mathrm{136.69lb}$ | 66.44 kg |
| Mid Wire | $26.99^{\circ}$ | $51 \mathrm{~kg} \mathrm{112.43lb}$ | 57.23 kg |
| Btm Wire | $6.09{ }^{\circ}$ | 40kg 88.18lb | 40.22 kg |

## 4. WIRE TENSIONS

Frequency of a wire is defined by:
$f=\frac{\sqrt{\frac{t}{m}}}{2 l}$
$\mathrm{m}=$ mass applying tension to wire
$\mathrm{g}=$ acceleration due to gravity
$\mathrm{m}_{1}=$ mass per unit length of wire
$\mathrm{l}=$ length of wire
$\mathrm{f}=$ natural frequency

The wires we have in the quad can have there natural frequency defined from this

|  | Top <br> Wire | Mid Wire | Btm <br> Wire | Final <br> Wire | Units |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Diameter | 1.1 | 0.71 | 0.635 | 0.457 | mm |
| Density | 7900 | 7900 | 7900 | 7900 | $\mathrm{~kg} / \mathrm{m}^{\wedge} 3$ |
| mass per unit | $7.51 \mathrm{E}-$ |  | $2.50 \mathrm{E}-$ | $1.30 \mathrm{E}-$ |  |
| length | 03 | $3.13 \mathrm{E}-03$ | 03 | 03 | $\mathrm{~kg} / \mathrm{m}$ |
| Angle to vertical | 22 | 27 | 8 | 0 | degrees |
| Length | 0.455 | 0.311 | 0.348 | 0.604 | metres |
| Load in kg | 66.9 | 28.6 | 20.2 | 10.0 | kg |
| gravity | 9.81 | 9.81 | 9.81 | 9.81 | $\mathrm{~m} / \mathrm{s}^{\wedge} 2$ |
|  |  |  |  |  |  |
| frequency | 332 | 482 | 404 | 228 | Hz |

Even if the lengths deviate slightly from these frequencies should be used as a baseline with a $\pm 2 \mathrm{hz}$ tolerance.

## 5. FLEXURE DISTANCES

Effective flexure lengths vary depending upon the connection method between the wire clamp and what it is attached to. In the quad the flexure lengths have been demonstrated to be as follows:

|  | fl with static clamp | Fl on blade |
| :--- | :--- | :--- |
| Top Wire | 5.1 | $\mathrm{n} / \mathrm{a}$ |
| Mid Wire | 3.2 | 3.9 |
| Btm Wire | 2.9 | 4.12 |
| Final Wire | 2.0 | $\mathrm{n} / \mathrm{a}$ |

## 6. LENGTH OF WIRES

The wire lengths are as follows:

|  | Nominal Length (no d's) | Real length excluding <br> flexure |
| :--- | :--- | :--- |
| Top | 445 | 455.2 |
| Mid | 308.5 | 315.6 |
| Btm | 341 | 348.02 |
| final | 600 | 604 |

## 7. SUSPENSION STABILITY

Reference T070073


This is illustrative of mass stability, it can be seen that at approximately 10 degrees the mass will topple. This was shown to be true

## 8. APPENDIX A, CONDENSED ESSENTIAL DATA

Target mass weights (nominal including wire clamps)
Top mass:
22kg
UI mass: 22kg
Penultimate mass: $\quad 40 \mathrm{~kg}$
Test mass: 40kg

Target blade wire clamp underside positions

| Top Stage | 41 mm | from stiff back |
| :--- | :--- | :--- |
|  | 104 mm | from optics table |
| Top mass | 6.6 mm | from gate notch |
| UI mass | 12 mm | from gate notch |

Vertical load requited to deflect blade to correct position (load resolved to wire angle)

| Top Wire | 66.44 kg |
| :--- | :--- |
| Mid Wire | 57.23 kg |
| Btm Wire | 40.22 kg |

Pitches, lengths and diameters of wires in wire jig

|  | Diameter | Target <br> Length* | Natural <br> Frequency | Jig length (inc <br> 2x 10mm slip) | Slip gauge <br> sum (mm) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Top Wire | 1.1 mm | 455.2 | 332 | 445 | $20(0.787 ")$ |
| Mid Wire | 0.71 mm | 311 | 482 | 310.5 | $20(0.787 ")$ |
| Btm Wire | 0.635 mm | 348.02 | 404 | 347.4 | $20(0.787 ")$ |
| Final Wire | 0.35 mm | 604 | 228 | 602 | $22(0.866 ")$ |

* Copied from dirty quad at RAL

