## LIGO-T070130-00-K

Effect of steel base blocks on frequency measurements on BS structure - 2

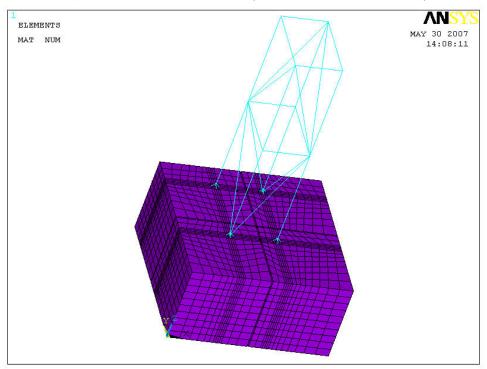
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#### 1. MOTIVATION

Tests on the behaviour of the structures continue to produce anomalous results. A test was made to check the motion of the structure at, or near, the feet where the structure is fixed to the blocks. The results are given in T070135, and show that the feet move in the "X" direction (see below) about a factor 0.1 less than points on about the middle ring of the structure. But the predictions from the existing FEA model say that the feet should only move about a factor 0.001 times the motion of the middle ring. This work explores whether that might be due to the blocks moving because they are not perfectly fixed on the floor.

#### 2. MODEL

The model from previous work (T070117) was used. It consists of an aluminium alloy simple beam model, fixed to four blocks of steel (meshed with brick elements).

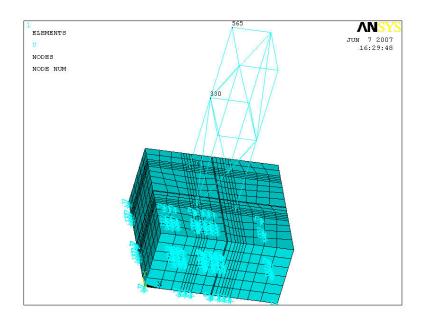


#### 3. RESULTS

#### 3.1 Initial result – concrete blocks fixed to floor

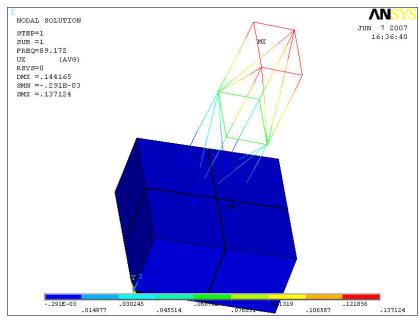
Frequencies below 200 Hz:

ŜET	TIME/FREQ	LOAD STEP	SUBSTEP	CUMULATI VE
1	89. 172	1	1	1
2	138. 10	1	2	2
3	194. 17	1	3	3



Three nodes were chosen along one leg.

NODE	Χ	Υ	Z	THXY	THYZ	THZX
174	0. 38000	1. 0200	0.61000	0.00	0.00	0.00
330	0. 38000	1. 0200	1. 4100	0.00	0.00	0.00
565	0. 38000	1. 0200	2. 2100	0.00	0.00	0.00

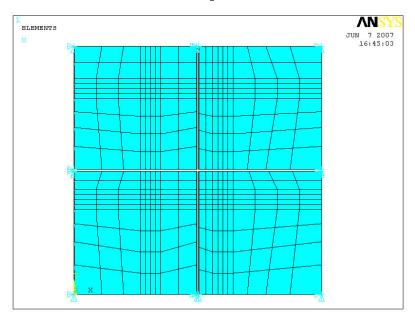


# The results for the first mode were:

NODE	UX	UY	UZ	USUM
174	-0. 70957E-04	-0. 83481E-04	0. 73282E-03	0.74096E-03
330	0. 61409E-01	-0. 27995E-01	0. 16824E-01	0.69554E-01
565	0. 13529	-0. 42635E-01	0. 16829E-01	0. 14284

So we can see that the movement at the foot should be three orders of magnitude smaller than that at the middle ring.

### 3.2 Block fixed at three corner points



It is likely that in practice the steel blocks are supported at three points, and the three points I used above are widely-separated. It is therefore surprising to see such a large effect on the first mode. I note that supporting at single points as I have done there is perhaps pessimistic in terms of the support stiffness – on the other hand the floor on which the blocks are resting is not infinitely stiff, so these two effects will cancel out to some extent.

```
Frequencies:
```

```
SET TIME/FREQ
1 80.322 cantilever, mostly in X, not much block movement
2 111.46 cantilever in X, and top surface of blocks moving in Z
3 121.91 cantilever in Y, blocks moving.
4 127.13 One block moving, structure not moving much
5 137.82
6 144.07
7 187.27
```

Note that the first frequency has dropped 10 Hz.

Results at the three leg nodes, mode 1:

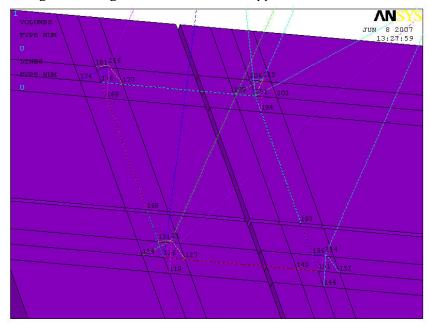
THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN THE GLOBAL COORDINATE SYSTEM

```
NODE UX UY UZ USUM
174 -0. 27769E-02 0. 15187E-02 0. 24795E-02 0. 40207E-02
330 0. 56097E-01-0. 26329E-01 0. 15835E-01 0. 63959E-01
565 0. 12681 -0. 40565E-01 0. 15843E-01 0. 13408
```

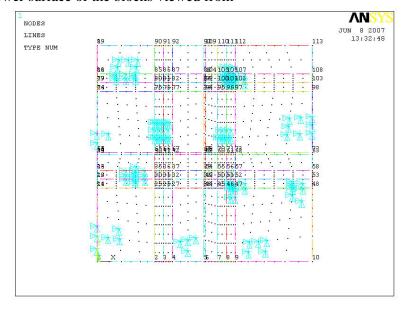
Note that the movements at the foot (node 174), even in this mode with little motion of the blocks in the mode shape, is only about a factor 20 smaller than the motion at the middle ring.

### 3.3 More realistic support

For this run I included the bars in the bottom ring, modelling them with 50\*50 solid cross section. To address the fact that they are clamped to the blocks along their length, but without too much additional modelling work, I fixed them to the bocks at the point where they cross the edge – see diagram and see macro in appendix 1.



I then chose some more "realistic" constraints, shown on this plot of the constrained nodes on the lower surface of the blocks viewed from



above:

The frequencies were

\*\*\*\*\* INDEX OF DATA SETS ON RESULTS FILE \*\*\*\*\*

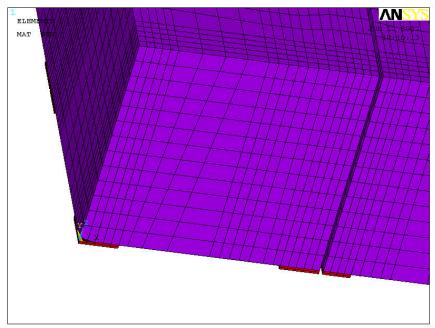
SET	TIME/FREQ	LOAD STEP	SUBSTEP	CUMULATI VE
1	89. 324	1	1	1
2	138. 41	1	2	2
3	195. 35	1	3	3

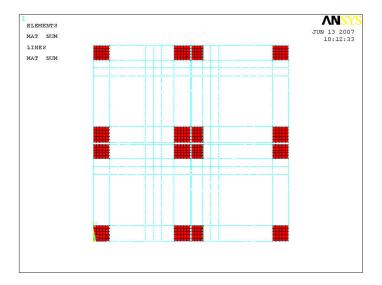
Which are basically the same as with the blocks fixed completely.

It seems we need to untangle the question of just how stiff the floor is. One interesting data point as that a block on its own was found to have a "roll" mode of about 15 Hz.

#### 4. MODEL WITH SOFT PADS SUPPORTING THE BLOCKS

The idea here is to put pads of a soft material under the blocks – the underneath of the pads is constrained, and by varying the modulus of the pads we can vary the amount of constraint on the blocks. See macro in appendix 2, and diagrams below. The location and dimensions of the pads are rather arbitrary; I chose them to minimise the additional model features required. The square pads at the outside corners are 100mm on a side, and they are all 10 mm thick.





The model has ~23000 elements.

### 4.1 Initial results – pad modulus 5GPa

With the modulus of the pads set to 5 GPa, the modes were

SET	TIME/FREQ	LOAD STEP	SUBSTEP	CUMULATI VE
1	86. 519	1	1	1
2	141. 92	1	2	2
3	185. 35	1	3	3

These are similar to the fully-constrained case.

Three nodes along one leg are 168, 255 and 485:

NODE	X	Υ	Z	IHXY	THYZ	THZX
168	0. 38000	1. 0900	0.61000	0.00	0.00	0.00
255	0.38000	1.0900	1. 4100	0.00	0.00	0.00
485	0. 38000	1. 0900	2. 2100	0.00	0.00	0.00
Movemen	ts in the first	mode are				
NODE	UX	UY	UZ	USUM		
140	0.20400E.02	0 0 057475 03	0 0 101125 02	O 1062EE	02	

So the movement at the foot is about a factor 30 smaller than that at the middle ring.

# 4.2 Pad modulus = 45 MPa

To get a frequency in the right range for the blocks, set the modulus of the pads so that the first "bounce" mode of a block is around 50 Hz (cf 15 Hz measured roll mode).

$$f = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$$

$$k = (2\pi f)^2 m$$

So desired k = 180 E6 N/m

$$k = \frac{aE}{l}$$

$$E = \frac{kl}{a}$$

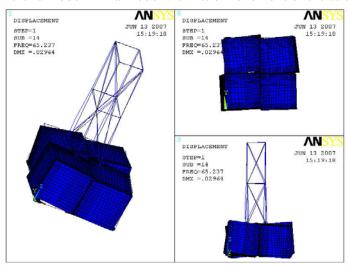
E = 180E6\*0.01/(0.1\*0.1\*4) = 45E6 Pa. Since the pads are not meant to be real rubber, simply a device to allow us to simulate an unknown degree of constraint of the blocks, we are free to set the modulus to any value (subject to stability of the solver).

MPTEMP,1,0 MPDATA,EX,3,,45E6 MPDATA,PRXY,3,,0.3 MPDATA,DENS,3,,2.0e3

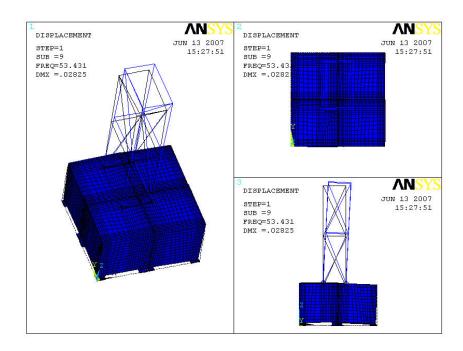
### This looks more like it:

```
TIME/FREQ
SET
       24.315
                      Pads shear in X
   2
       24.722
                      Pads shear in Y
       30.718
                      Blocks yaw en masse on pads about Z
       39.149
                      two blocks yaw out of phase on pads
                      two blocks yaw on pads, structure cantilevers in X two blocks yaw one way en masse; two the other way
       43. 789
       44.304
   6
       44.580
                      similar to mode 5
       51.809
                      structure cantilevers in Y
                      two blocks lift (stretching pads in Z); structure cantilevers in X two blocks roll (about Y) in opposition blocks pitch and/or roll
       53.431
       56. 862
 10
 11
       58.670
       60.153
                      blocks pitch and/or roll
                      blocks pitch, roll and yaw
blocks pitch, roll and yaw (see diagram below)
blocks roll about Y, structure cantilevers in X
       62.954
       65. 237
72. 035
 14
 15
                      two blocks yaw in opposition
 16
       83. 259
                      blocks pitch; structure cantilevers in X
 17
       87.424
                      blocks roll; structure goes in torsion
blocks pitch, structure cantilever in Y
block roll, structure cantilevers in X
       101.58
 18
 19
       103.19
       125.84
```

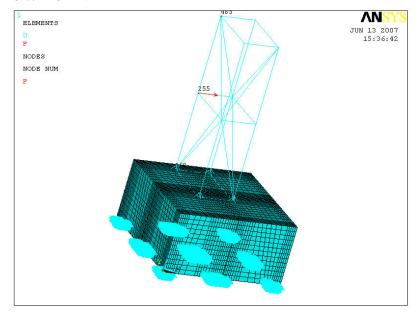
#### Here is mode 14 - a mode with little movement of the structure



Here is mode 9 in which the structure moves:

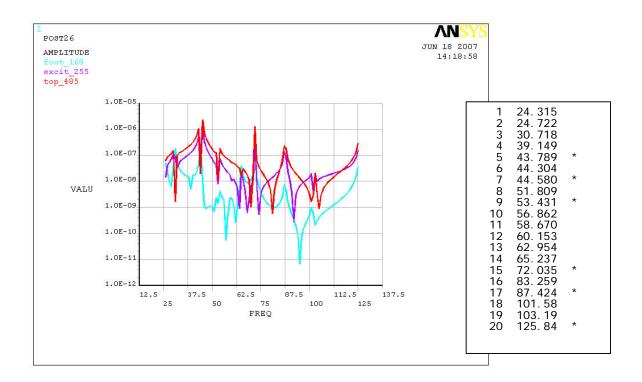


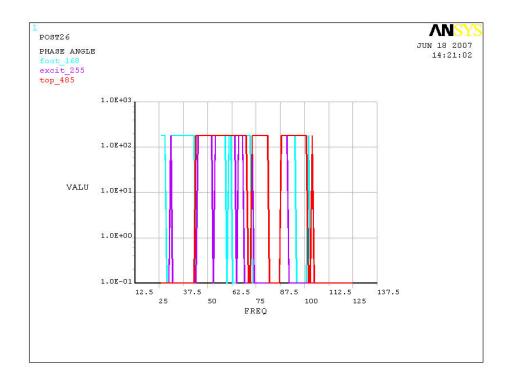
So what happens if we subject this structure to an excitation part-way up the structure? I applied a force to node 255 (half way up the structure), and ran a full harmonic analysis from 25 to 125 Hz.



This will take a while...

(weekend run)...





Qualitatively, I see peaks at varying heights

Appendix – macro for section 3.	3	
FINISH ! Make sure we are at	z0 = 0	LGEN,2,P51X, , , ,gap, , ,0
BEGIN level	z1 = bsizev	
/CLEAR	z2 = z1 + zstruct1	adrag,90,91,92,93,,,13,14,15,16
*abbr,doit,doit	z3 = z1 + zstruct2	adrag,94,95,96,97,,,13,14,15,16
*abbr,jreplo,/replot /PREP7	!	vdrag,all,,,,,17
// KEI /	keypoints	varag,aii,,,,,, i i
! to build a simple beam model on	-21	/VIEW, 1, -0.236620128544 , -
steel blocks	k, 1, x0,y0,z0	0.782474382372 ,
!	k, 2, x6,y0,z0	0.575972877572
!Element types !*	k, 3, x1,y0,z0	/ANG, 1, 10.5782042749 /REPLO
: ET,1,BEAM4	k, 4, x7,y0,z0 k, 5, x2,y0,z0	/REPLO
!*	k, 6, x3,y0,z0	!restart line numbering from 500
ET,2,SOLID186	k, 7, x8,y0,z0	NUMSTR,LINE,500,
!*	k, 8, x4,y0,z0	
If an the hearns 1 hellows 2 solid	k, 9, x9,y0,z0	!line 500 - 502
!For the beams 1 = hollow; 2 = solid	k,10, x5,y0,z0	l,126,21 ,21,22
R,1,0.0009,3.08E-07,3.08E-	!lines 1 to 4	,22,23
07,0.025,0.025		,==,==
R,2,0.0025,5.21E-07,5.21E-	I,1,2	!vertical legs
07,0.025,0.025	,2,3	ldrag,151,201,176,,,,500,501,502
	,3,4	les talalla eta e
!materials 1 = aluminium; 2 = steel	,4,5 !lines 5 to 8	!middle ring I,22,219
MPTEMP,,,,,,	I,6,7	,219,218
MPTEMP,1,0	,7,8	,218,217
MPDATA,EX,1,,70E9*4	,8,9	,217,22
MPDATA,PRXY,1,,0.3	,9,10	
MPDATA,DENS,1,,2.7E3*2	1. 4400 =0	! diagonals
	k,11,x0,y6,z0 k,12,x0,y1,z0	l,126,219 ,219,201
MPTEMP,,,,,,,	k,12,x0,y1,z0 k,13,x0,y7,z0	,201,217
MPTEMP,1,0	k,14,x0,y2,z0	,217,126
MPDATA,EX,2,,210E9	k,15,x0,y3,z0	
MPDATA,PRXY,2,,0.3	k,16,x0,y8,z0	1,23,219
MPDATA,DENS,2,,7.8E3	k,17,x0,y4,z0	,219,221
! geometry	k,18,x0,y9,z0 k,19,x0,y5,z0	,221,217 ,217,23
: geometry	K, 19,X0,y3,20	,217,23
xoff = 0.23	!lines 9 to 12	!top ring lines 524-527
yoff = 0.14	I,1,11	1,23,222
xstruct = 0.36	,11,12	,222,221
ystruct = 0.55 bsize = 0.610	,12,13 13,14	,221,220
bsize = 0.610 bsizev = 0.610	,13,14	,220,23
gap = 0.010	!lines 13 to 16	!bottom ring lines 528 - 533
zstruct1 = 0.8	I,15,16	I,176,201
zstruct2 = 1.6	,16,17	,201,193
fixoff = 0.05	,17,18	,193,151
X0 = 0	,18,19	,151,126 ,126,168
X1 = bsize - xoff	!z dimension	,168,176
x2 = bsize	k,20,x0,y0,z1	,, -
x3 = x2 + gap	k,21,x1,y1,z1+fixoff	!fixings
x4 = x1 + xstruct	k,22,x1,y1,z2	1,21,124
x5 = x3 + bsize	k,23,x1,y1,z3	,21,131
x6 = x1 - fixoff x7 = x1 + fixoff	!line 17	,21,119 ,21,127
x8 = x4 - fixoff	I,1,20	,21,127
x9 = x4 + fixoff	, , -	,214,156
	adrag,1,2,3,4,,,9,10,11,12	,214,152
y0 = 0	adrag,5,6,7,8,,,9,10,11,12	,214,144
y1 = bsize - yoff	FLST 3.8.4 ORDE 9	,214,149
y2 = bsize y3 = y2 + gap	FLST,3,8,4,ORDE,8 FITEM,3,45	,215,202
y4 = y1 + ystruct	FITEM,3,48	,215,206
y5 = y3 + bsize	FITEM,3,50	,215,194
y6 = y1 - fixoff	FITEM,3,52	,215,199
y7 = y1 + fixoff	FITEM,3,81	040.477
y8 = y4 - fixoff	FITEM,3,84 FITEM 3.86	,216,177 216,160
y9 = y4 + fixoff	FITEM,3,86 FITEM,3,88	,216,169 ,216,181
		,= 10, 101

ksel,s,kp,,126 ,a,kp,,176 ,a,kp,,201 ,a,kp,,151 real,2 Imesh,all ,216,174 !top ring lines !meshing !set element size !volumes dk,all,ux,0 ,all,uy,0 ,all,uz,0 :nofix allsel lsel,s,line,,500,600 lesize,all,0.01 mat,2 type,2 ! structure except top & bottom ring Isel,u,line,,524,533 vmesh,all allsel \*go, :nofix !constraints dk,219,UX,1 mat, 1 !constraints
!fix points on the ground
kpsel,s,loc,z,-0.01,0.01
kpsel,u,kp,,11,19
dk,all,ux,0
,all,uy,0
,all,uz,0 real,1 type,1 sbctra Imesh,all :end

!top & bottom ring lsel,s,line,,524,533 ! fix leg ends

Appendix 2 – macro with pads u	nder the blocks	
FINISH! Make sure we are at	x11 = x10 + fixoff	16 17
BEGIN level	x11 = x10 + 11x011 $x13 = x8 + bsize$	,16,17 ,17,18
/CLEAR	x13 = x0 + bsize x12 = x13-xpad	!lines 17 to 22
*abbr,doit,doit	X12 - X10 Xpaa	1,19,20
*abbr,jreplo,/replot	y1 = 0	,20,21
/PREP7	y14 = ypad	,21,22
	y16 = bsize - yoff	,22,23
! to build a simple beam model on	y15 = y16-fixoff	,23,24
steel blocks	y17 = y16 + fixoff	,24,25
! modified to include support pads	y18 = bsize	
12 jun 07	y19 = y18 + gap	!z dimension
!Element types !*	y20 = y19 + ypad	k,26,x1,y1,z1
: ET,1,BEAM4	y22 = y16 + ystruct y21 = y22 - fixoff	k,27,x4,y16,z1+fixoff
[*	y23 = y22 + fixoff	k,28,x4,y16,z2 k,29,x4,y16,z3
ET,2,SOLID186	y25 = y19 + bsize	k,30,x1,y1,z4
!*	y24 = y25 - ypad	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	, , ,	!lines 23 and 24 for vdrags
!For the beams 1 = hollow; 2 = solid	z0 = 0	I,1,26
!	z1 = bsize	I,1,30
R,1,0.0009,3.08E-07,3.08E-	z2 = z1 + zstruct1	
07,0.025,0.025	z3 = z1 + zstruct2	adrag,1,2,3,4,5,6,12,13,14,15,16
R,2,0.0025,5.21E-07,5.21E-	z4 = -zpad	adrag,7,8,9,10,11,,12,13,14,15,16
07,0.025,0.025		
	!	
Impataniala 4 - alumnimiumu 2 - ata alu	keypoints	lsel,s,loc,y,bsize-0.001,bsize+0.001
!materials 1 = aluminium; 2 = steel; 3 = rubbery stuff	k 1 v1 v1 <del>z</del> 0	lgen,2,all,,,,gap allsel
MPTEMP,,,,,,	k, 1, x1,y1,z0 k, 2, x2,y1,z0	alisei
MPTEMP,1,0	k, 3, x3,y1,z0	adrag,145,146,147,148,149,150,12,
MPDATA,EX,1,,70E9*4	k, 4, x4,y1,z0	13,14,15,16
MPDATA,PRXY,1,,0.3	k, 5, x5,y1,z0	adrag,151,152,153,154,155,
MPDATA,DENS,1,,2.7E3*2	k, 6, x6,y1,z0	,12,13,14,15,16
	k, 7, x7,y1,z0	
	k, 8, x8,y1,z0	vdrag,all,,,,,,23
MPTEMP,,,,,,,	k, 9, x9,y1,z0	
MPTEMP,1,0	k,10, x10,y1,z0	!select corner areas
MPDATA,EX,2,,210E9	k,11, x11,y1,z0	FLST,5,16,5,ORDE,16
MPDATA,PRXY,2,,0.3	k,12, x12,y1,z0	FITEM,5,1
MPDATA,DENS,2,,7.8E3	k,13, x13,y1,z0	FITEM,5,6
		FITEM,5,25 FITEM,5,30
MPTEMP,,,,,,,	!lines 1 to 6	FITEM,5,30 FITEM,5,-31
MPTEMP,1,0	inies i to o	FITEM,5,35
MPDATA,EX,3,,5e9	I,1,2	FITEM,5,51
MPDATA,PRXY,3,,0.3	,2,3	FITEM,5,55
MPDATA,DENS,3,,2.0e3	,3,4	FITEM,5,-56
	,4,5	FITEM,5,61
! geometry	,5,6	FITEM,5,80
	,6,7	FITEM,5,85
xoff = 0.23	llines 7 to 11	FITEM,5,-86
yoff = 0.14	1,8,9	FITEM,5,90
xstruct = 0.36	,9,10	FITEM,5,106
ystruct = 0.55	,10,11	FITEM,5,110
bsize = 0.610 bsizev = 0.610	,11,12 12,13	ASEL,S, , ,P51X
gap = 0.010	,12,13	vdrag,all,,,,,24
zstruct1 = 0.8	k,14,x1,y14,z0	varag,aii,,,,,,24
zstruct2 = 1.6	k,15,x1,y15,z0	allsel
fixoff = 0.05	k,16,x1,y16,z0	/VIEW, 1, -0.236620128544 , -
xpad = 0.1	k,17,x1,y17,z0	0.782474382372 ,
ypad = 0.1	k,18,x1,y18,z0	0.575972877572
zpad = 0.01	k,19,x1,y19,z0	/ANG, 1, 10.5782042749
	k,20,x1,y20,z0	vplot
x1 = 0	k,21,x1,y21,z0	
x2 = xpad	k,22,x1,y22,z0	
x4 = bsize - xoff	k,23,x1,y23,z0	!restart line numbering from 1500
x3 = x4-fixoff	k,24,x1,y24,z0	NUMSTR,LINE,1500,
x5 = x4+fixoff	k,25,x1,y25,z0	lling 1500 1502
x6 = bsize - xpad x7 = bsize	!lines 12 to 16	!line 1500 - 1502 I,198,27
x7 = DSIZE x8 = x7 + gap	Ines 12 to 16 I,1,14	,198,27 ,27,28
x0 = x7 + yap x10 = x4 + xstruct	,14,15	,28,29
x9 = x10 - fixoff	,15,16	,,
	, -1:=	

lmesh,all !vertical legs ldrag,236,276,314,,,,1500,1501,150 allsel !volumes !middle ring Isel,u,loc,z,-10,0.001 1,28,397 Isel,u,loc,z,bsize-0.001,10 ,397,399 lesize,all,fixoff ,398,28 allsel ! diagonals vsel,s,loc,z,0,z2 1,276,28 mat,2 ,28,401 type,2 ,401,399 ,399,276 vmesh,all 1,236,28 vsel,s,loc,z,-bsize,0 ,28,400 ,400,399 mat,3,type,2 vmesh,all ,399,236 !\*go,:end !top ring lines 1524-1527 | |,29,400 !constraints !fix points on the ground ,400,402 asel,s,loc,z,-zpad-0.001,-,402,401 zpad+0.001 da,all,ux,0 ,401,29 ,all,uy,0 !bottom ring lines 1528 - 1533 ,all,uz,0 1,198,258 ,258,276 !\*go, :nofix ! fix leg ends ksel,s,kp,,126 ,276,314 ,314,298 ,298,236 ,a,kp,,176 ,a,kp,,201 ,236,198 ,a,kp,,151 !fixings 1,27,199 ,27,191 dk,all,ux,0 ,27,197 ,all,uy,0 ,all,uz,0 ,27,205 :nofix ,394,237 ,394,230 allsel ,394,234 ,394,242 sbctra ,395,269 ,395,275 ,395,277 ,395,283 :end ,396,308 ,396,312 ,396,315 ,396,320 !meshing !set element size Isel,s,line,,1500,1600 lesize,all,0.01 ! structure except top & bottom ring Isel,u,line,,1524,1533 mat, 1 real,1 type,1 Imesh,all !top & bottom ring lsel,s,line,,1524,1533

real,2