



Status Report: Adaptive Thermal Compensation & Determination of Thermophysical Constants

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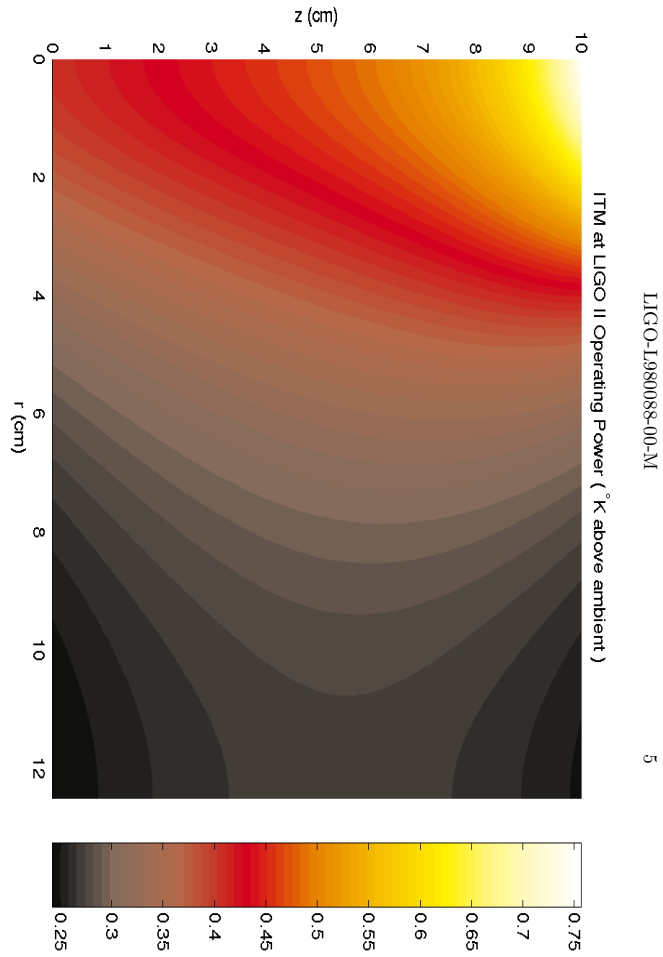
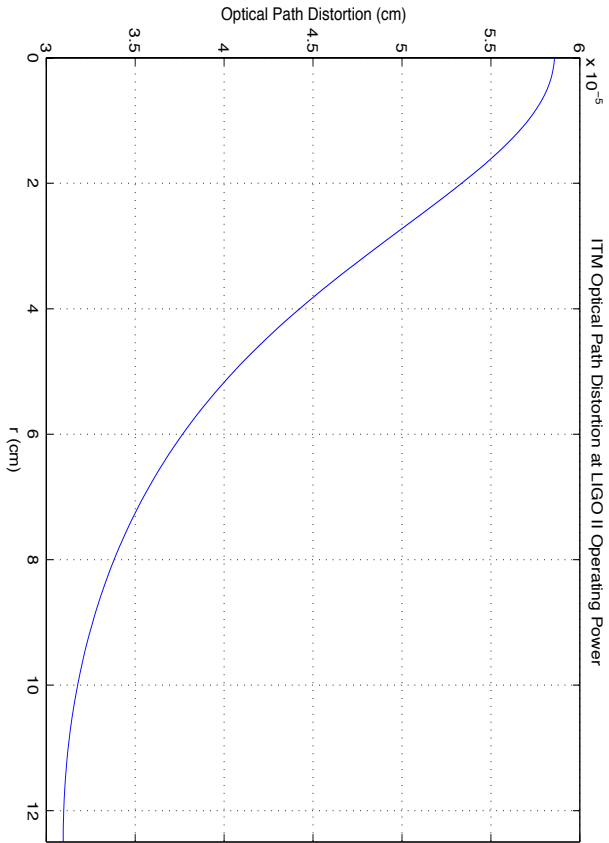
LSC Lasers and Optics Working Group

LIGO Science Collaboration Meeting

LIGO Livingston Observatory
20-23 March, 2002



FEA model: uncorrected SiO₂ ITM





Adaptive Compensation of Thermal Lensing in Advanced LIGO Core Optics

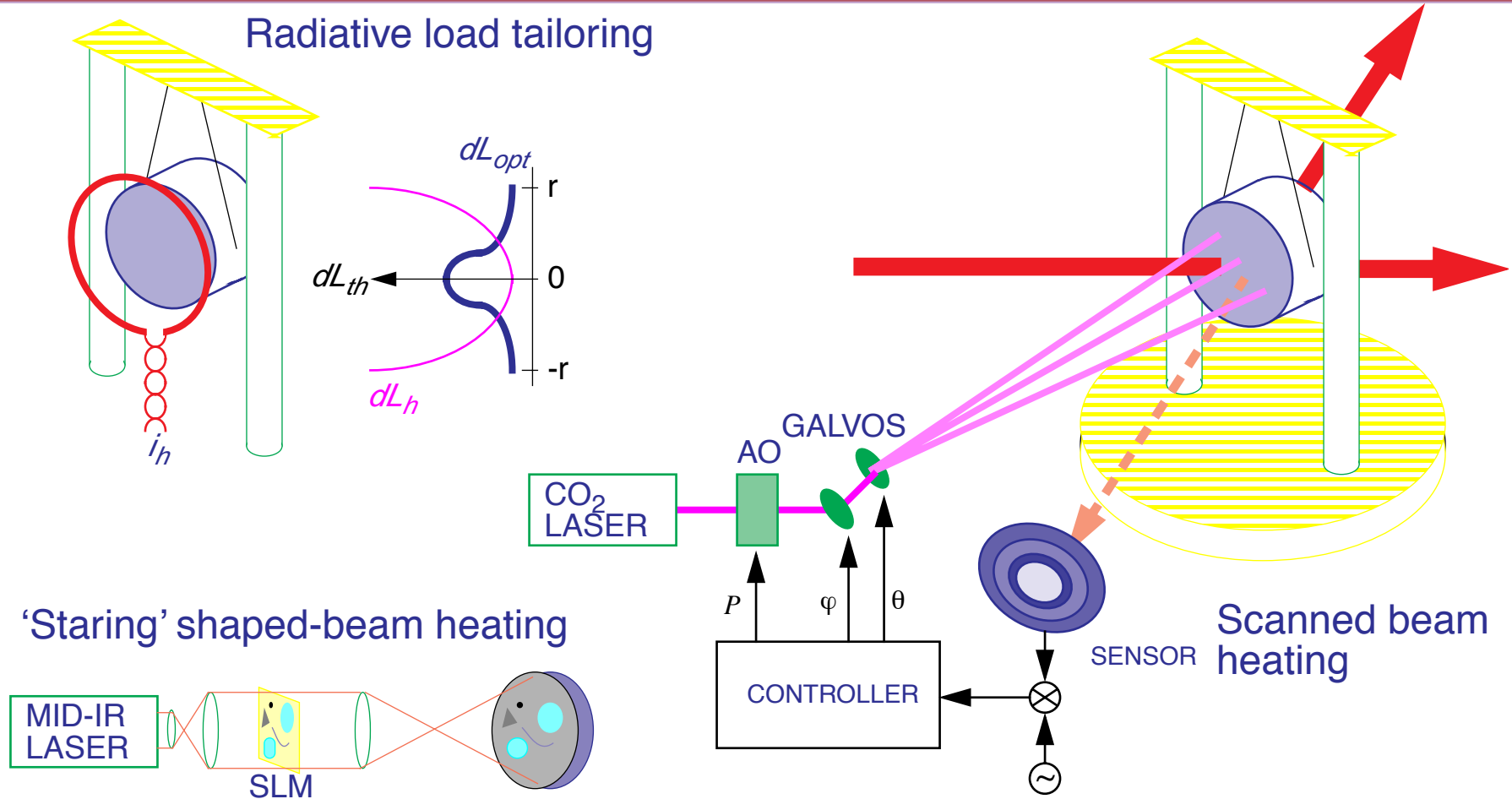
- Thermal distortions expected to limit AdLIGO
 - ◇ Thermal lens aspherical; refocusing, curvature 'preload' not adequate
 - ◇ Cold-start 'bootstrap' problem
 - ◇ Strong possibility of spatially inhomogeneous absorption in Al_2O_3
- Test mass & coating improvements not guaranteed adequate
- Real-time not especially difficult w/current technology
 - Scanning "Phase Camera" (Adhikari, MIT)
 - Staring "Bullseye WFS" (Mueller, UF)
 - Hartmann & Shack-Hartmann methods (Veitch & McLelland, ACIGA)
- Actuation tricky; can't "touch" anything (no PZT mirrors, etc.)



Thermal Actuation

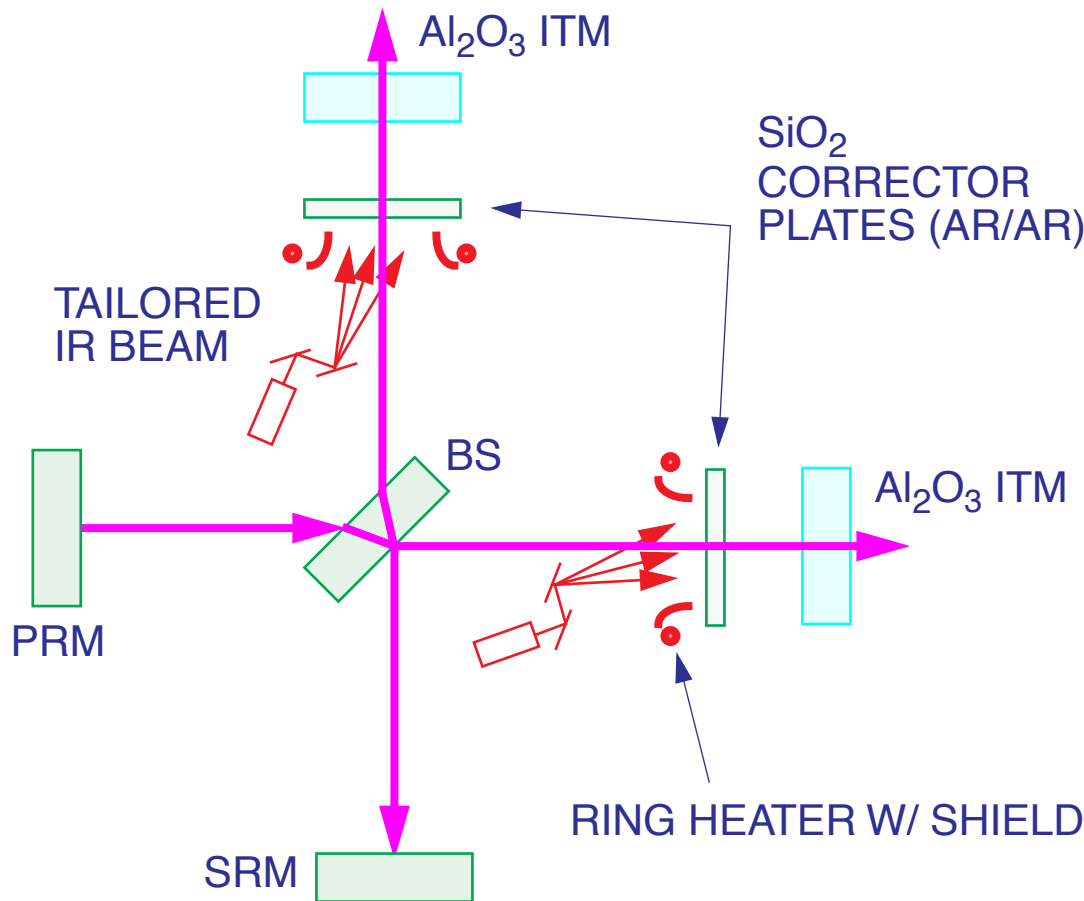
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- Thermal actuation on core optics (Lawrence, MIT)
 - Noncontact actuators with low spurious phase noise potential
 - Time constants & spatial scales matched to disturbances
 - Radiative ring heater (“Toaster”)
 - Simple nichrome ring near optic, aided by passive low-emissivity shield
 - Purely axisymmetric, but efficient and low potential for spurious noise
 - Directed beam heating (“Star Wars”)
 - Can deal with (nearly) arbitrary error function (e.g., absorption ‘hot spots’)
 - Potential for noise if directed at main cavity optics
 - Not efficient for first-order effect (simple lensing)
 - **USE BOTH** on **TRANSMISSIVE OPTICS** (not cavity mirrors)

Thermal OPD Actuators





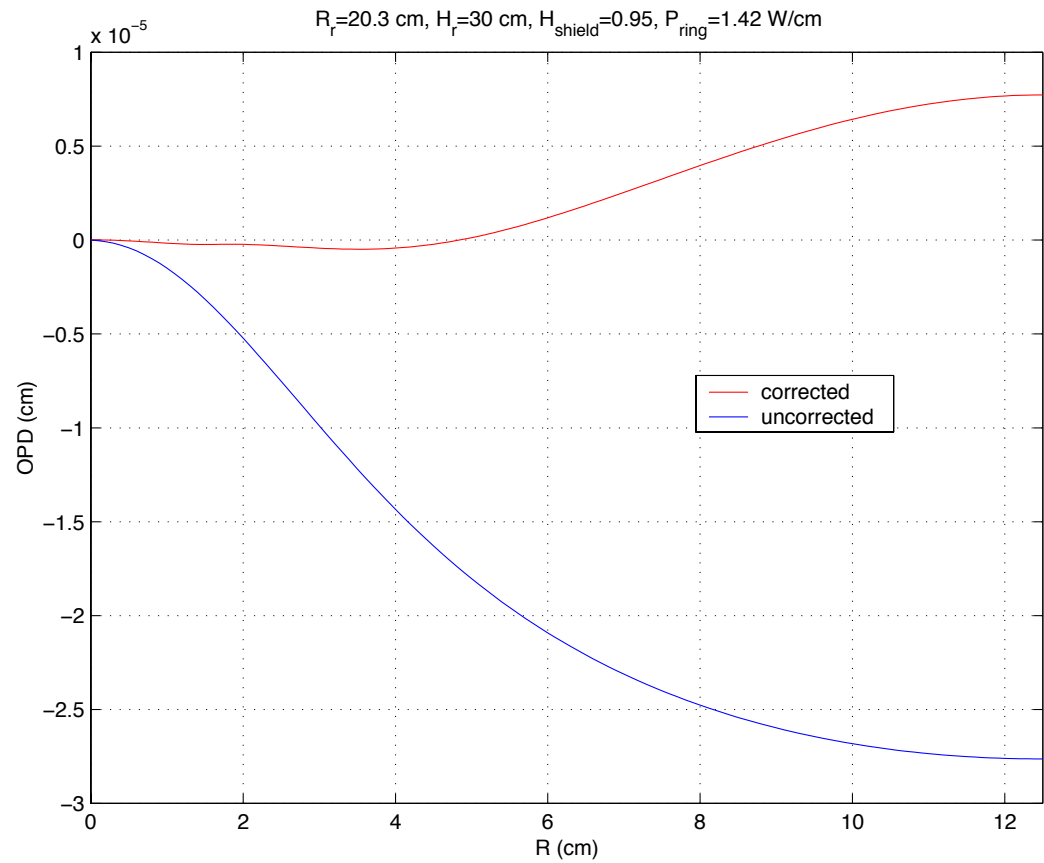
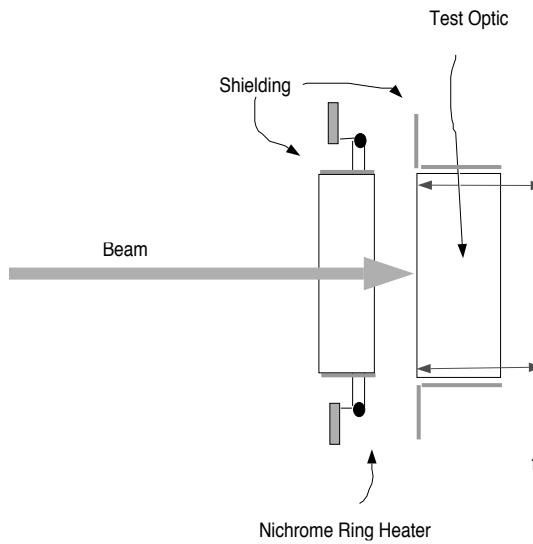
Proposed Implementation: Corrector Plates w/ Dual Actuators



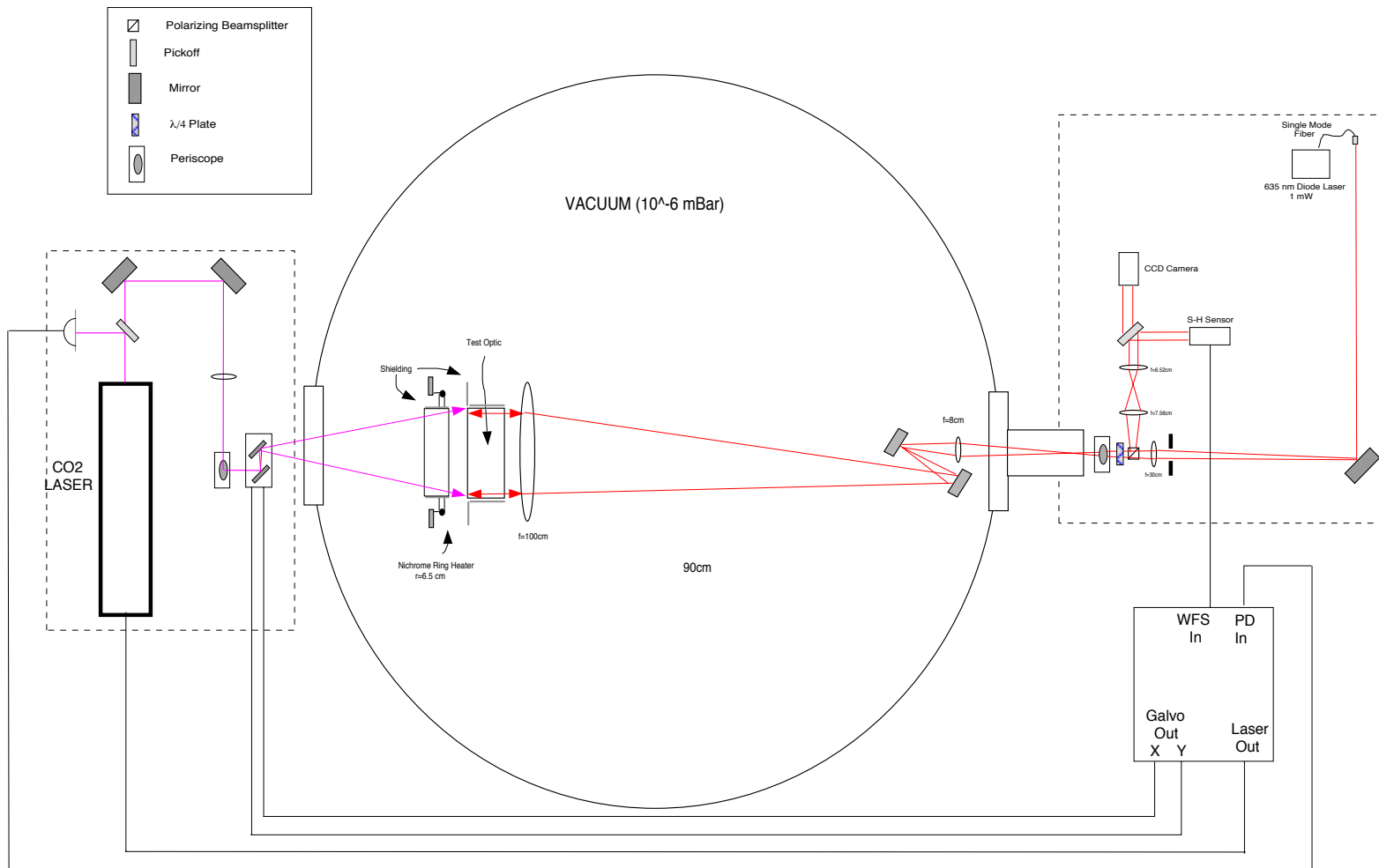
- minimize cavity mirror ΔT
- minimize IR beam noise influence
- thin plate gives added “bowing” leverage
- use fused silica for dn/dT , low k (spatial contrast)
- alternate: use PRM and BS (harder to model!)



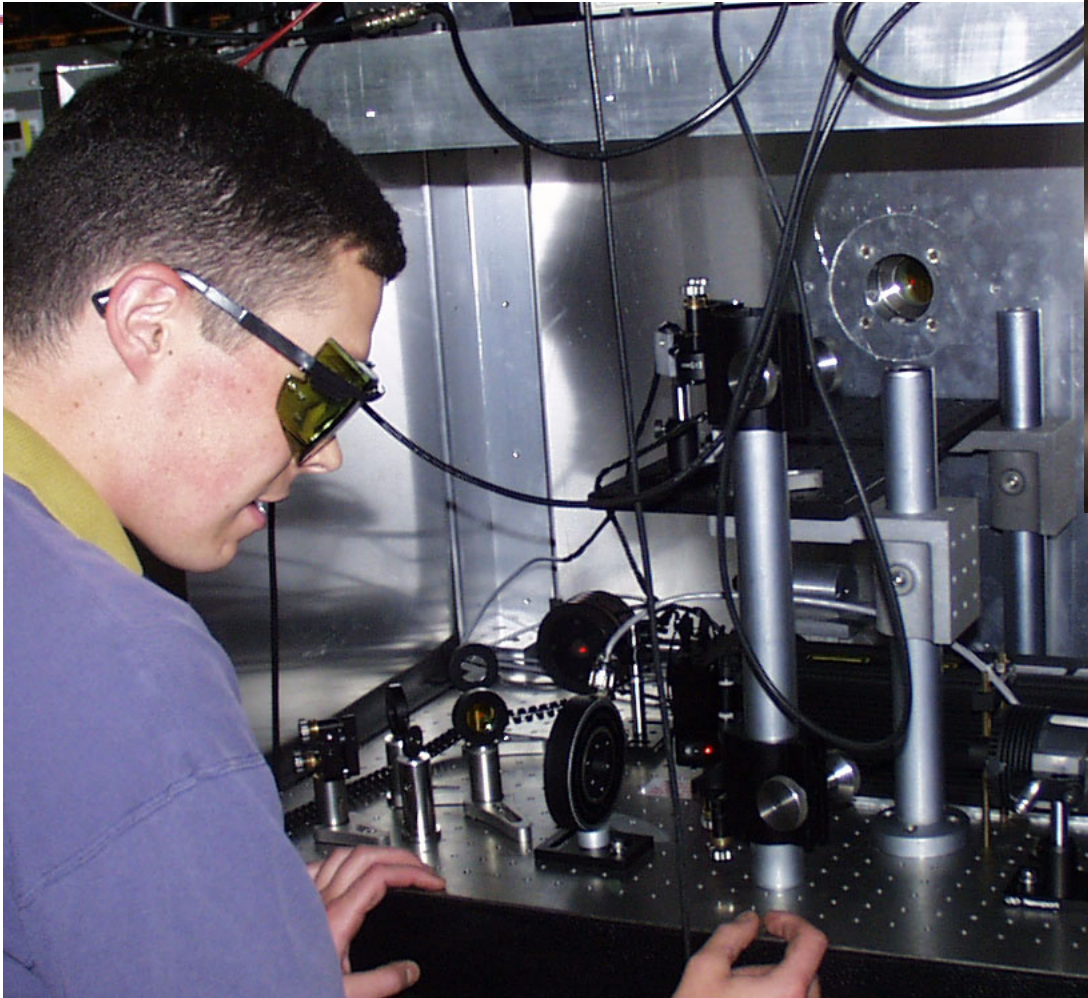
FEA model w/correction: ring heater + cylindrical radiation shield



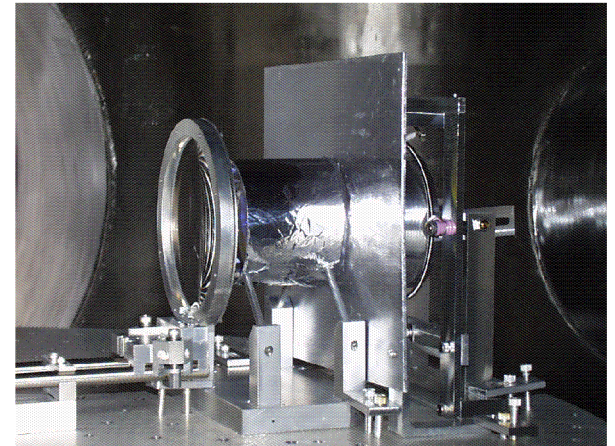
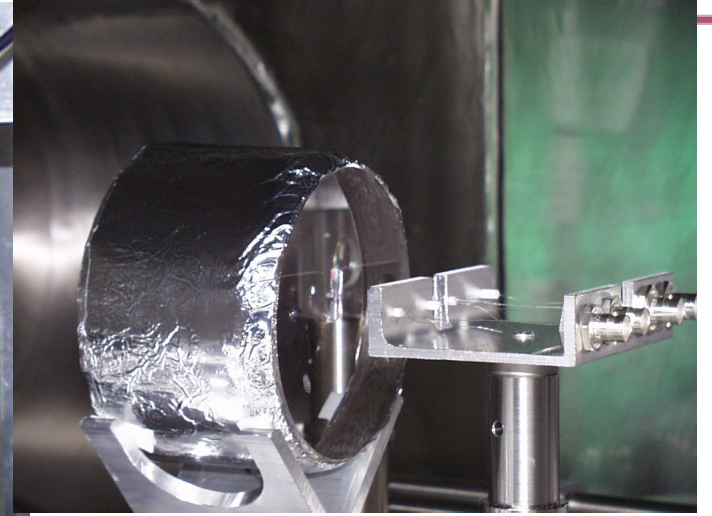
ATC Experiment



ATC Experiment



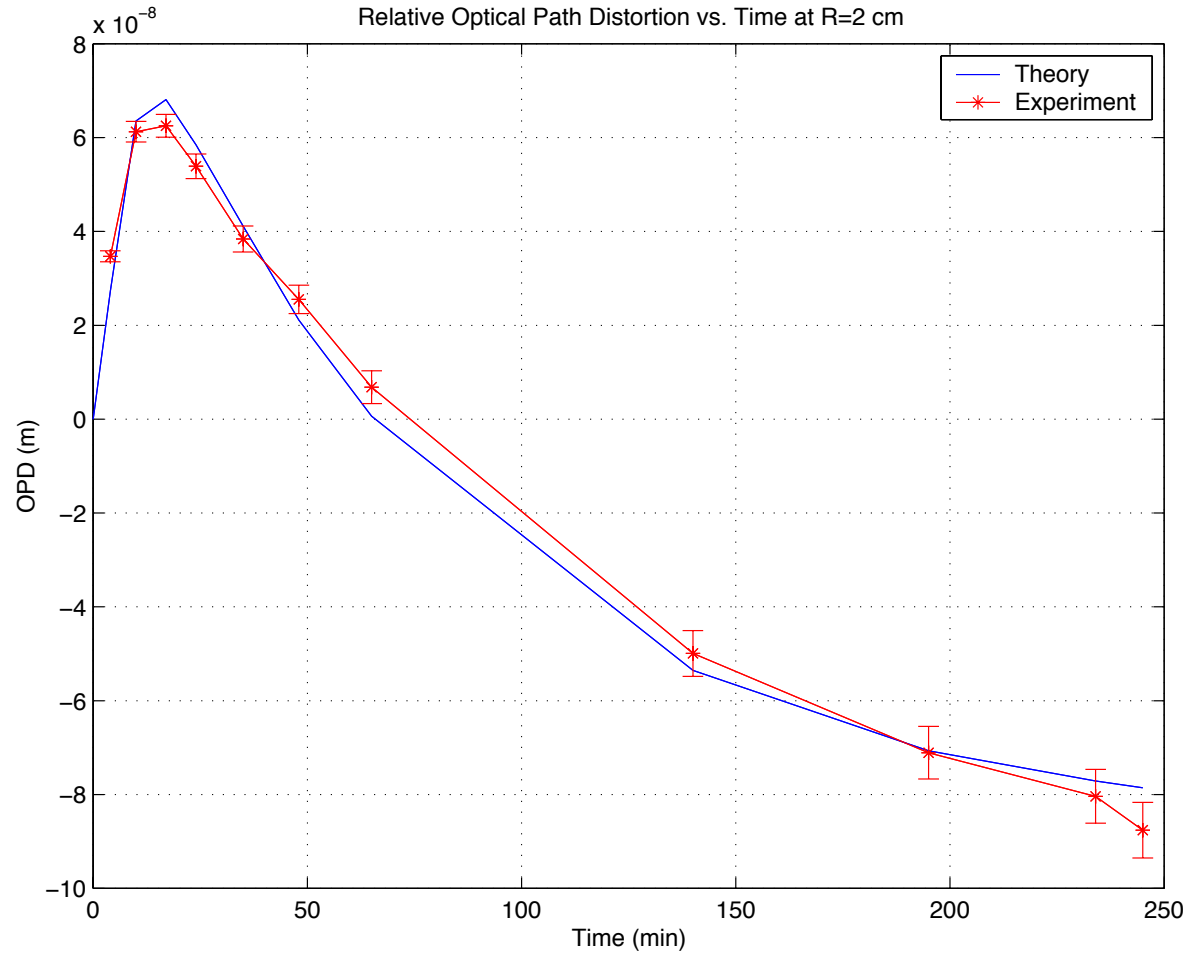
LIGO-G020069-00-R



Zucker



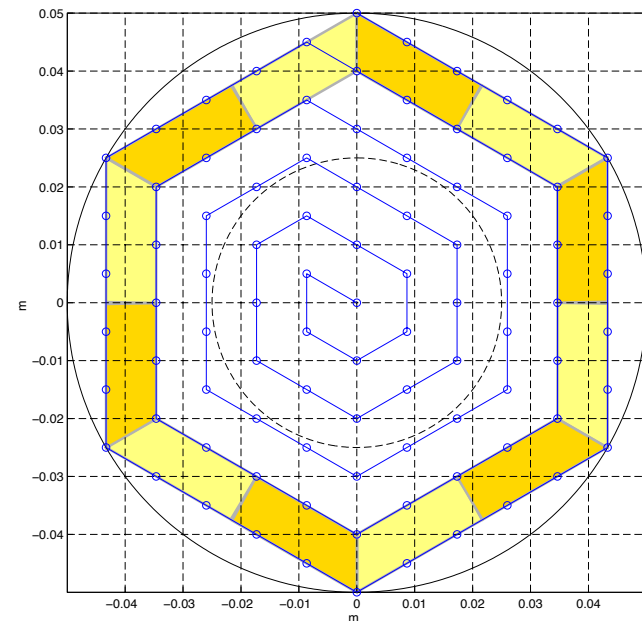
OPD vs. t, ring heater w/SiO₂ test optic



Tailored Beam Heating Progress

- Tailored beam actuation (RCL & undergrads)

- ◇ FEA of actuation “kernel” (R. Bennett thesis), showed edge effects negligible
- ◇ Developed actuation basis & generated “arbitrary” Zernike distortions (P. Marfuta thesis); found hard to control net lens (‘power’) with finite heat
- ◇ Efficient “spiral” scan pattern (minimum move/settle time for galvos)
- ◇ Inversion (distortion map --> heat map) converges well if outer periphery is lumped into single zone





Other Progress

- Interferometer modeling (RCL)
 - ◇ Applied Melody to case of 150W in LIGO I with SV glass ; thermal compensation makes it work! (LIGO-P010023)
 - ◇ Added angled optics (e.g., beamsplitters) to Melody (LIGO-T020001)
 - ◇ Added anisotropic material (e.g., sapphire) capability to Melody (LIGO-T020001)
- Sensing & interpretation (SH sensors are deceptive!)
 - ◇ Imaging of optic at SH CCD plane is critical (test target & second CCD)
 - ◇ Edge diffraction causes bias (throw away periphery, use big optics)
 - ◇ Don't trust "wavefront reconstruction" algorithm; use raw gradients
 - ◇ Calibrate magnification using tilted mirror for pure shear
- Still need **measurements of absorption inhomogeneity**



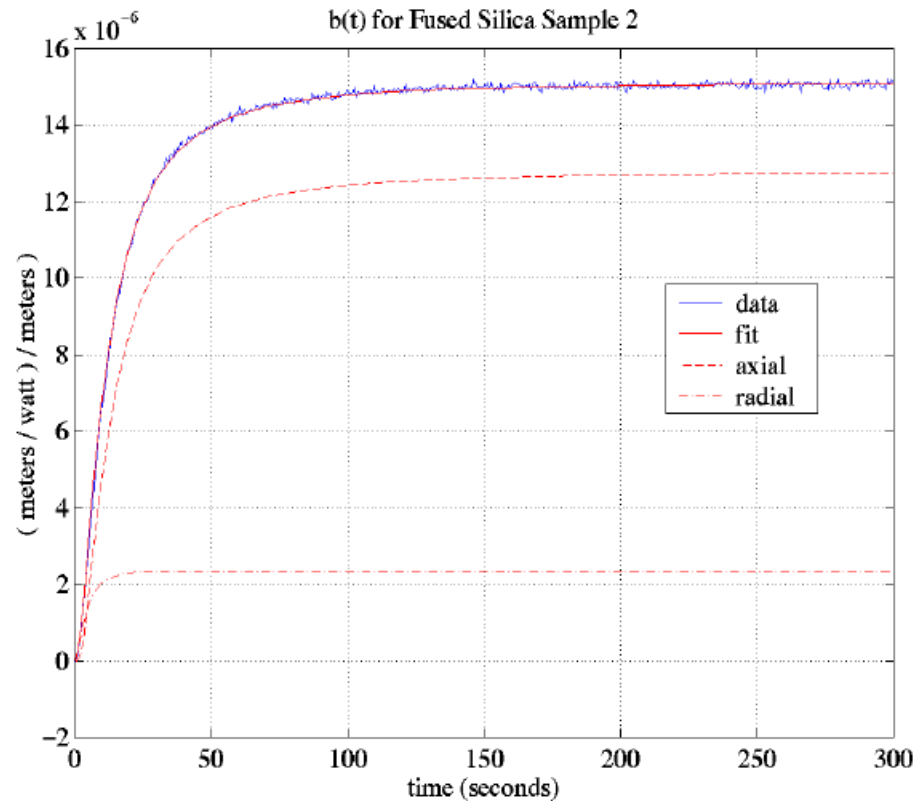
Thermophysical Constants

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- Radial OPD gradient vs. time in “impulse response” (space & time) will project k_{th} and α independently
 - Prior attempts to also include dn/dT were not so easy
 - Results sensitive to systematics from SH sensors, “wavefront reconstruction” errors
 - Now have anisotropic formalism for influence kernel, use only wavefront gradients
 - Waiting for “good” C-axis sapphire, but initial silica test looks consistent with model



Fused Silica Constants

@ 60C temperature



Measure:

$$d\phi/dr = a(t) r + b(t)$$

Isotropic Fit:

$$k_{th} = 1.47(\pm 0.03) \text{ W/m/K}$$

$$\alpha = 6.39(\pm 0.13) \times 10^{-7} / \text{K}$$

Anisotropic Fit:

$$k_{th_r} = 1.48(\pm 0.08) \text{ W/m/K}$$

$$k_{th_z} = 1.13(\pm 0.24) \text{ W/m/K}$$

$$\alpha_r = 5.07(\pm 1.04) \times 10^{-7} / \text{K}$$

$$\alpha_z = 6.83(\pm 0.40) \times 10^{-7} / \text{K}$$

Published Values:

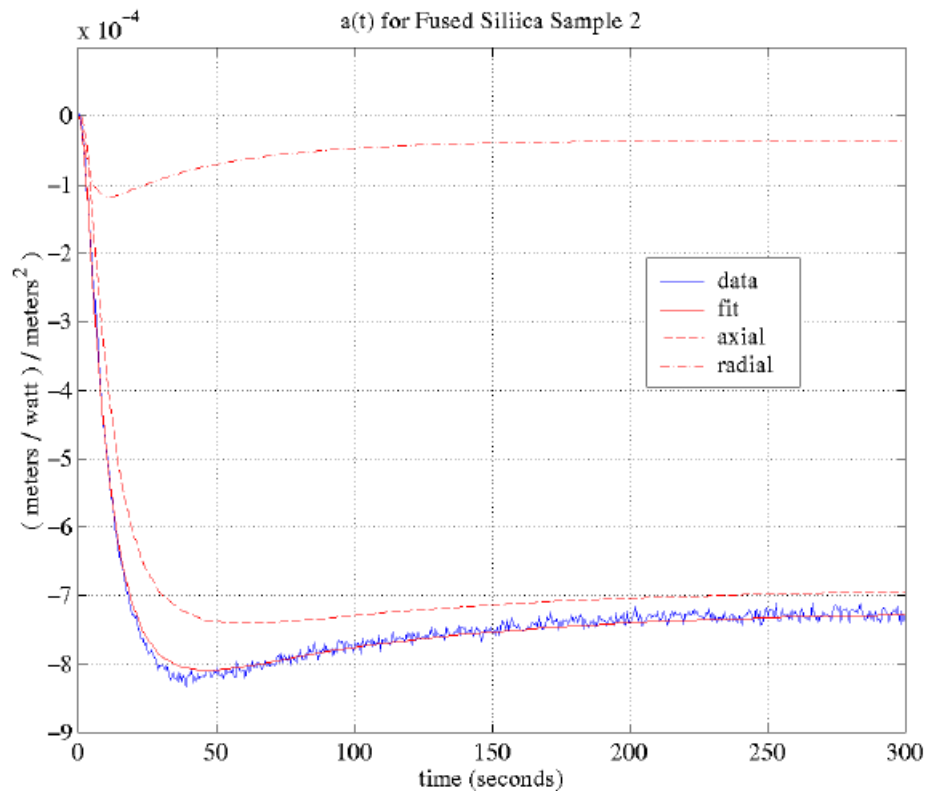
$$k_{th} = 1.42 \text{ W/m/K (CRC)}$$

$$\alpha = 5.5 \times 10^{-7} / \text{K (??)}$$



Fused Silica Constants (cont'd)

@ 60C temperature



Measure:

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Future Track

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- Now: Second pass at sapphire k_{th} , α
 - Next: Retest toaster, beam actuators on silica
 - ◇ Significantly enhanced models
 - ◇ Better control of systematics in SH sensing
 - ◇ With more IFO performance modeling -> RCL Ph.D. thesis
 - Transitioning work to other team members
 - ◇ Dave Ottaway + student + part-time optomech engineer
 - 4Q'02: deliver “toaster” design to Gingin
 - 2Q'03: deliver prototype dual-actuator system to Gingin