



# Frequency dependent loss in coated silica substrates

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## Introduction

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- Recent studies suggest loss of silica substrates improve at lower frequencies [Numata et al. LIGO Doc G010365-00.pdf, Penn et al. Rev Sci Inst 72(9) 3670]
- We have measurements of the losses of silica substrates and of dielectric coatings from  $\sim 2.8$  kHz to  $\sim 73$  kHz
- Have enough information to consider frequency dependence of coating losses



## Overview

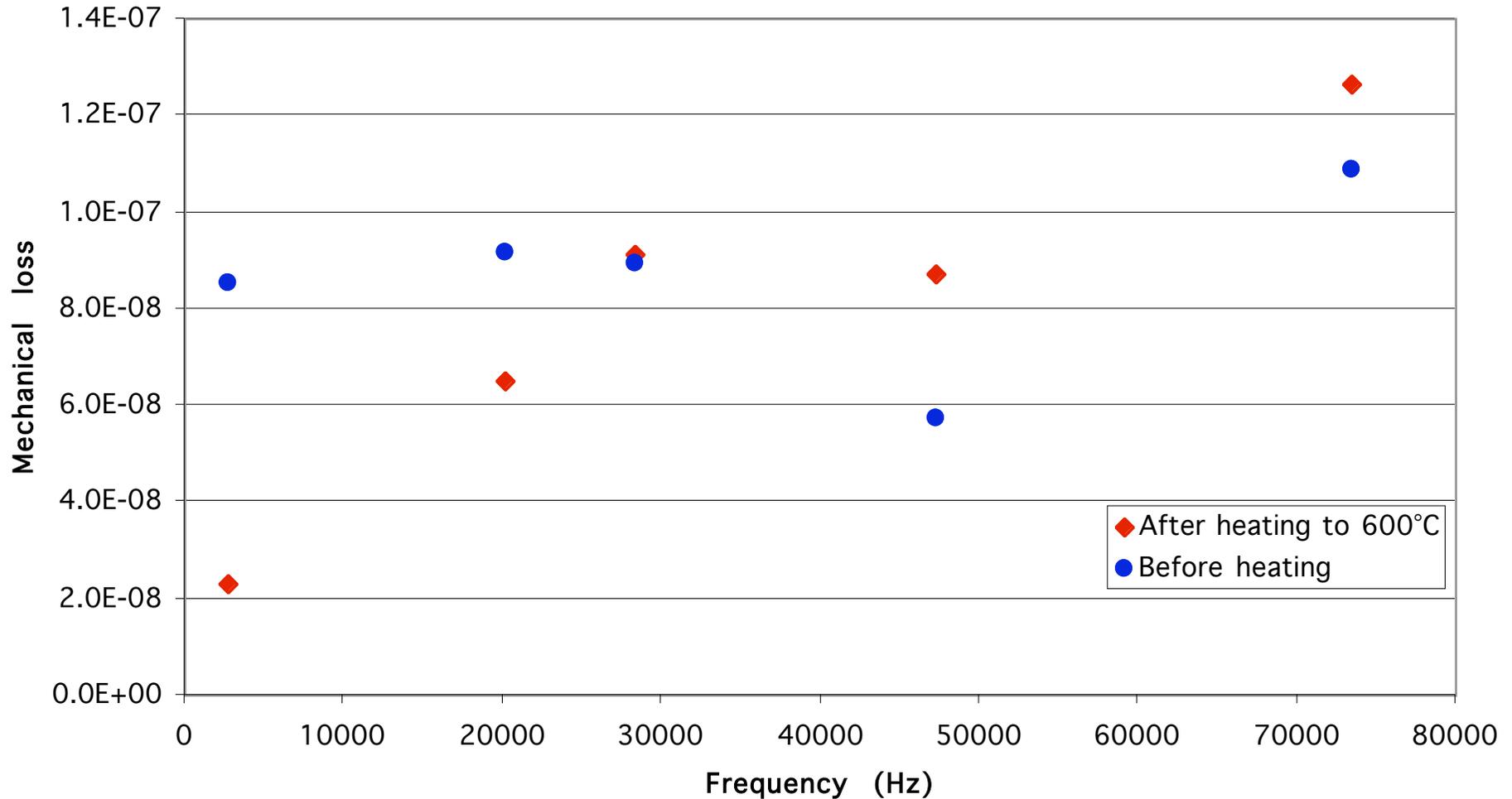
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1. Substrate loss frequency dependence (Corning 7980 silica, grade 0A, sub-Angstrom polish; samples as in talk by P. Sneddon)
2. Frequency dependent mechanical loss of dielectric coatings ( $\text{SiO}_2:\text{Ta}_2\text{O}_5$  coating)
3. Frequency dependent loss of individual coating materials



# Frequency dependence of substrate loss on heating temperature

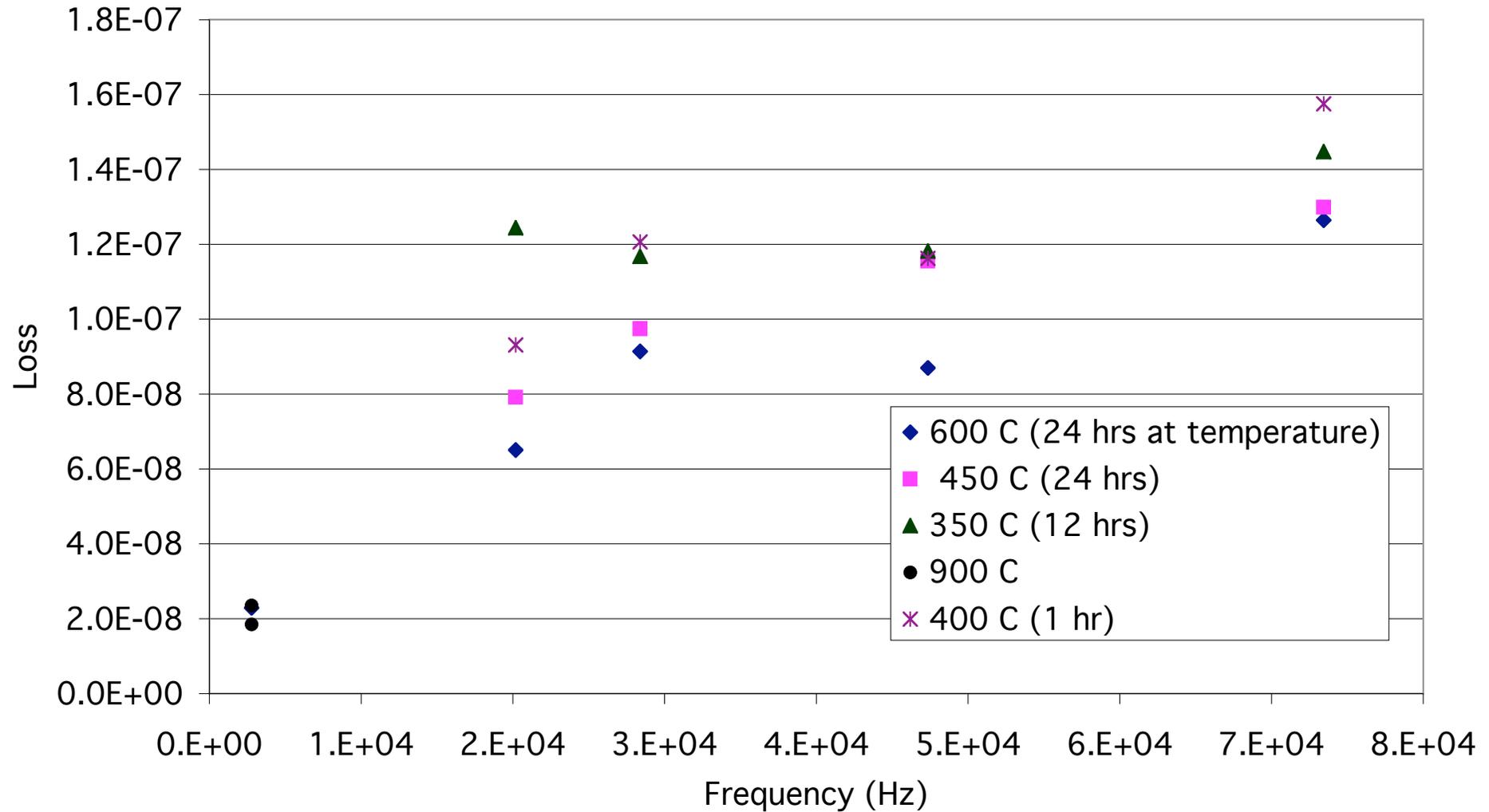
Measured loss as a function of frequency before and after heating





# Frequency dependence at various temperatures

Measured loss as a function of frequency for annealed samples





## Frequency dependence of coating losses

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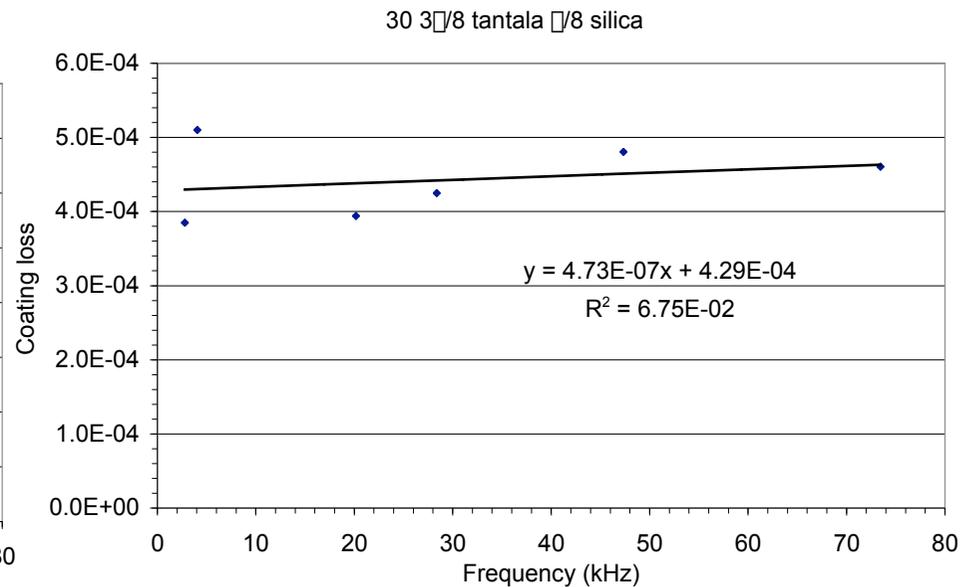
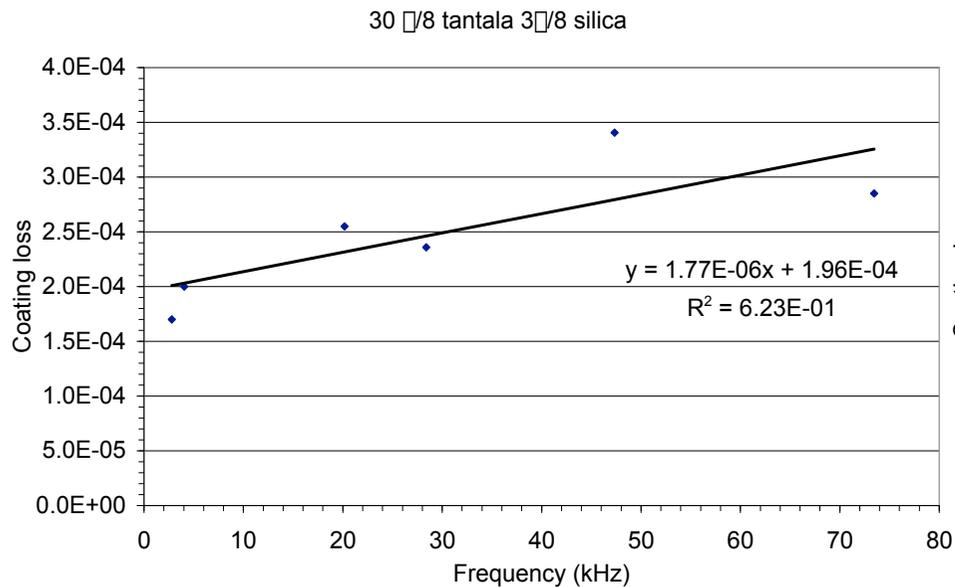
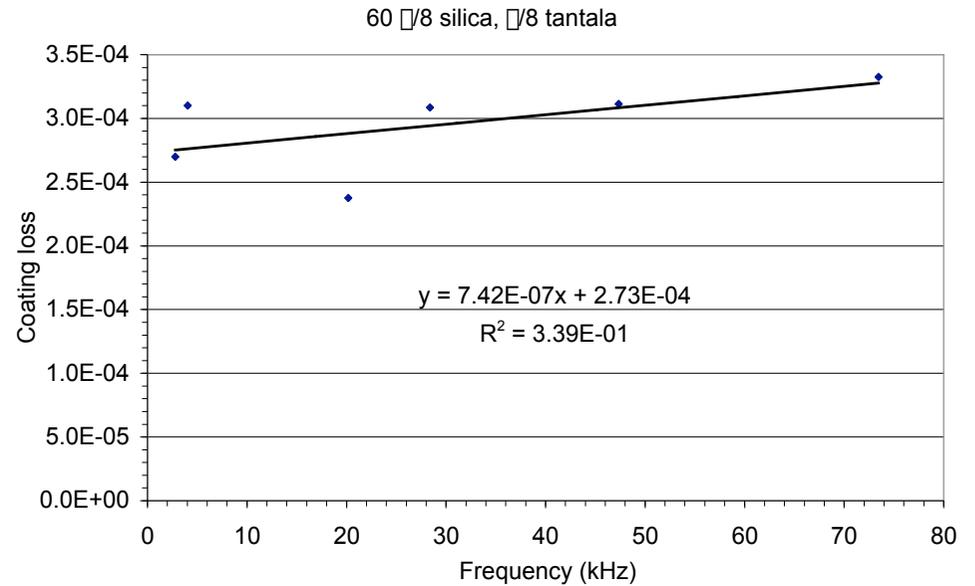
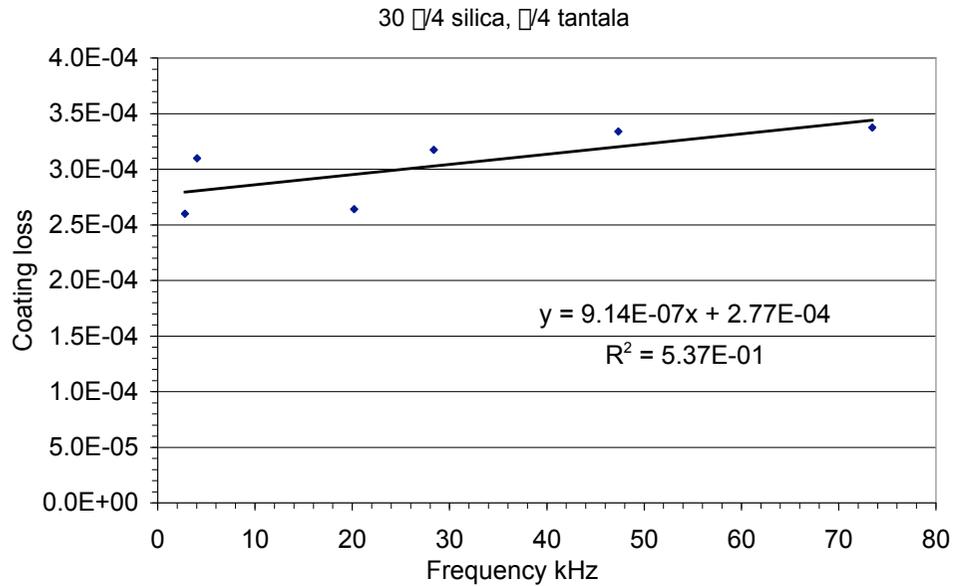
- Recall loss parameterisation (as in talk by P. Sneddon)

$$\phi_{coated}(\omega_0) = \phi_s(\omega_0) + \frac{E_{coating}}{E_{substrate}} \phi_c(\omega_0)$$

- Can use this to work out individual losses for each mode
- Obtain different frequency dependences for each coating formulation



# Frequency dependence of losses for different coating formulations





## Coating split

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- These graphs suggest the level of frequency dependence depends on the relative amounts of each coating material
- The contribution of the loss of each coating material to the total measured loss of a  $\text{SiO}_2:\text{Ta}_2\text{O}_5$  coating is scaled by the energy stored therein.  $\phi_{Sc}$  represents the loss of the  $\text{SiO}_2$  component of the coating and  $\phi_{Tc}$  represents the loss of the  $\text{Ta}_2\text{O}_5$  component

$$\phi_c(\omega) = \phi_{Sc}(\omega) \left[ \frac{Y_{Sc}t_{Sc}}{Y_{Sc}t_{Sc} + Y_{Tc}t_{Tc}} \right] + \phi_{Tc}(\omega) \left[ \frac{Y_{Tc}t_{Tc}}{Y_{Sc}t_{Sc} + Y_{Tc}t_{Tc}} \right]$$

where Y is the Young's modulus and t the total thickness of each coating material

Note this neglects the effects of Poisson's ratio (expected to be small)



## Coating split

- Model each material loss as having both a frequency linearly dependent and frequency independent term:

$$\phi_{Sc}(\omega) = \phi_{Sc_0} + \omega\phi_{Sc_1} \quad \phi_{Tc}(\omega) = \phi_{Tc_0} + \omega\phi_{Tc_1}$$

then

$$\phi_c(\omega) = (\phi_{Sc_0}A_i + \phi_{Tc_0}B_i) + \omega(\phi_{Sc_1}A_i + \phi_{Tc_1}B_i)$$

$y = c + mx$

where

$$A_i = \left[ \frac{Y_{Sc}t_{Sc}}{Y_{Sc}t_{Sc} + Y_{Tc}t_{Tc}} \right] \quad B_i = \left[ \frac{Y_{Tc}t_{Tc}}{Y_{Sc}t_{Sc} + Y_{Tc}t_{Tc}} \right]$$

- Use multiple regression to fit for  $c$ , the frequency independent loss and  $m$ , the frequency dependent loss.



## Coating split continued

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- Using this model observe a slight frequency dependence

- This gives:

- Frequency independent loss:

- »  $\square_{Sc0} = (2.7 \pm 5.7) \times 10^{-5}$

- »  $\square_{Tc0} = (4.9 \pm 0.4) \times 10^{-4}$

- Frequency dependent loss

- »  $\square_{Sc1} = (2.5 \pm 0.3) \times 10^{-9}$

- »  $\square_{Tc1} = (-1.8 \pm 2.5) \times 10^{-10}$



## Conclusions

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- There appears to be a frequency dependence not only in the annealed substrates but also in the coating itself
- Substrate loss frequency dependence appears to be associated with heating temperature
- Coating loss for each material appears to be divisible into frequency dependent and independent terms
  - Tantalum frequency independent loss larger than that of silica
  - Silica frequency dependent loss larger than that of tantalum



## Conclusions 2

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- Frequency dependence does not effect thermal noise level in sub kHz frequency band for silica tantala coatings
- Analysis of these results is preliminary and needs to be extended in light of new thermoelastic damping theory (Fejer et al.)