





Adv LIGO and retrofit seismic isolation research update

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LIGO





LIGO-I Seismic isolation Stack

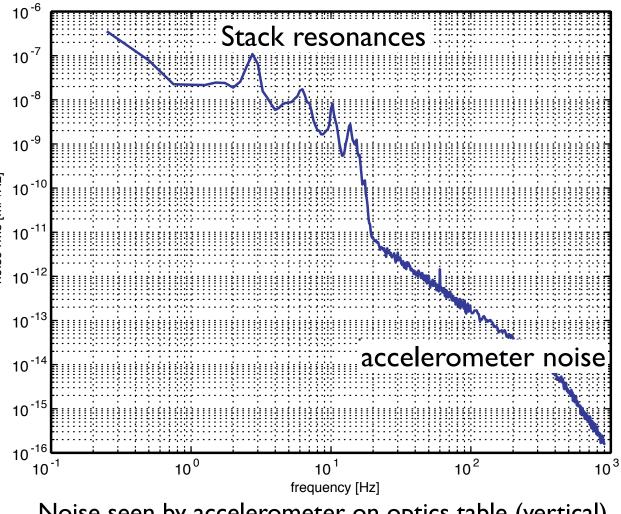
- 4 cascaded mass-spring layers support integral down-tube/ optics table
- novel internally-damped coil springs bring Q's of normal modes down to ≈10-30.





Stack performance

- Stack isolates very well at high frequencies,
- meeting requirements. But, there are several troublesome resonances in the I-I2 Hz band that affect the interferometer when excited by ground noise.



Noise seen by accelerometer on optics table (vertical)

Ground noise studies.



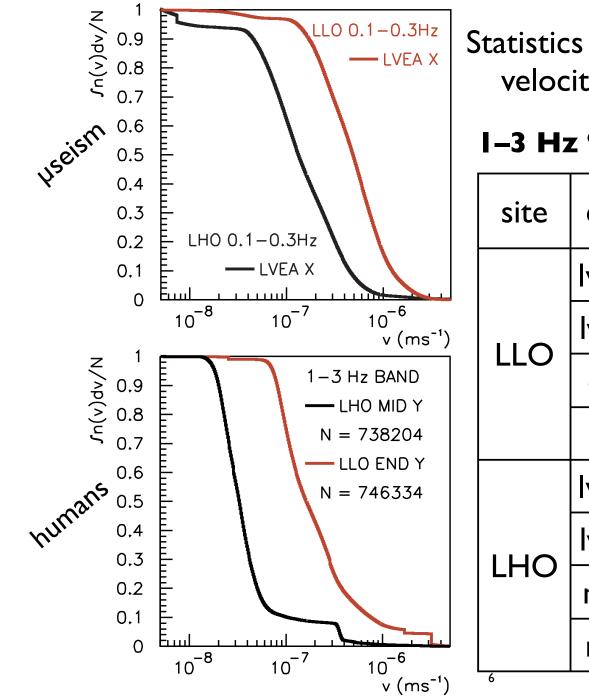
Louisiana ground noise



- Timber harvesting adds noise in I-3 Hz band
- Storms and waves in the Gulf of Mexico add noise in sub-Hz bands.
- Trucks, cars and trains...



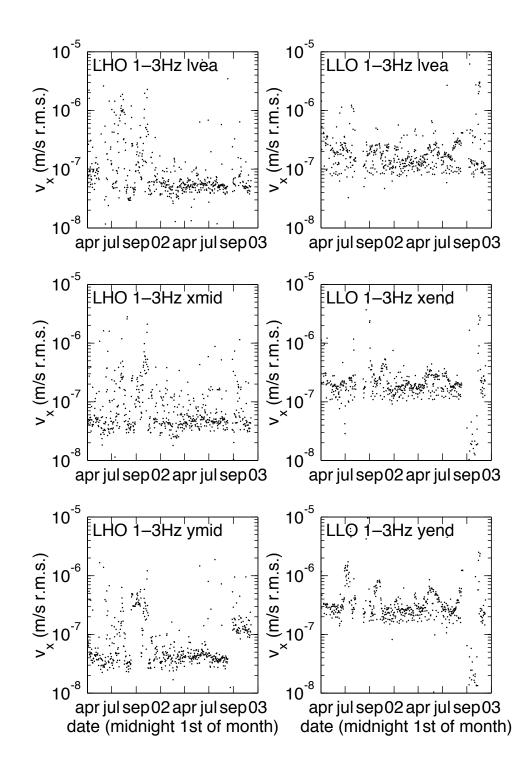
80 60 40 20 0 -20 -40 -60 -80 -100 -130 F Cloud 30 20 10 0 -10 -20 -30 -40 -50 -60 -70 -80 -90 C Temperature



Statistics of band-limited rms velocities over 613 days

I-3 Hz 90th percentile values

		000/	
site	chan	90%,	llo/
		µm/s	lho
LLO	lvea x	0.31	4.0
	lvea y	0.29	3.6
	ex x	0.34	4.5
	ey y	0.75	7.3
LHO	lvea x	0.078	
	lvea y	0.083	
	mx x	0.077	
	my y	0.10	



Long-term ground noise trends

- 600+ day study of bandlimited RMS of seismometer signals at both sites.
- no long-term trend is evident.
- large excursions seen in high frequencies due to human activity
- large seasonal excursions seen in microseism due to large-scale weather.

Torture test: 1500 s segments during 'interesting' times.

- Quantities listed are for the greatest arm length peak-to-peak excursion, and for the differential rms arm length deviation.
- Displacement integrated down to 30 mHz, acceleration up to 16 Hz.

data file	Displacement	Velocity	Acceleration
Enormous µseism	63 µm p-p	35 µm/s p-p	180 µm/s² p-p
	11 µm rms	4.8 µm/s rms	17 µm/s² rms
Day Train	13 µm p-p	13 µm/s p-p	150 µm/s² p-p
	1.7 µm rms	1.6 µm/s rms	17 µm/s² rms
Borderline day	30 µm p-p	18 µm/s p-p	150 µm/s² p-p
	4.6 µm rms	2.5 µm/s rms	17 µm/s² rms

Active noise reduction

$y = (I + GK)^{-1}GKr$ command tracking $+ (I + GK)^{-1}G_{\rm d} d$ disturbance suppression $-(I+GK)^{-1}GKn.$ noise environmental environment disturbance Feedforward sensor noise $d(\omega)$ $n_d(\omega)$ $K_{\rm ff}G_{\rm ff}G = G_{\rm d} \Rightarrow$ noise cancellation feed-forward measured K_{ff}(s) controller environment Sensor Correction G_d(s) M corrects error signal within servo loop system G_{ff}(s) dynamics feedback command "real" controller input output ► y(ω) K(s) G(s) $r(\omega)$ y_m(ω) M(s) measured + sensor output other sensor $\ln(\omega)$ noise correction ^Imeasurements

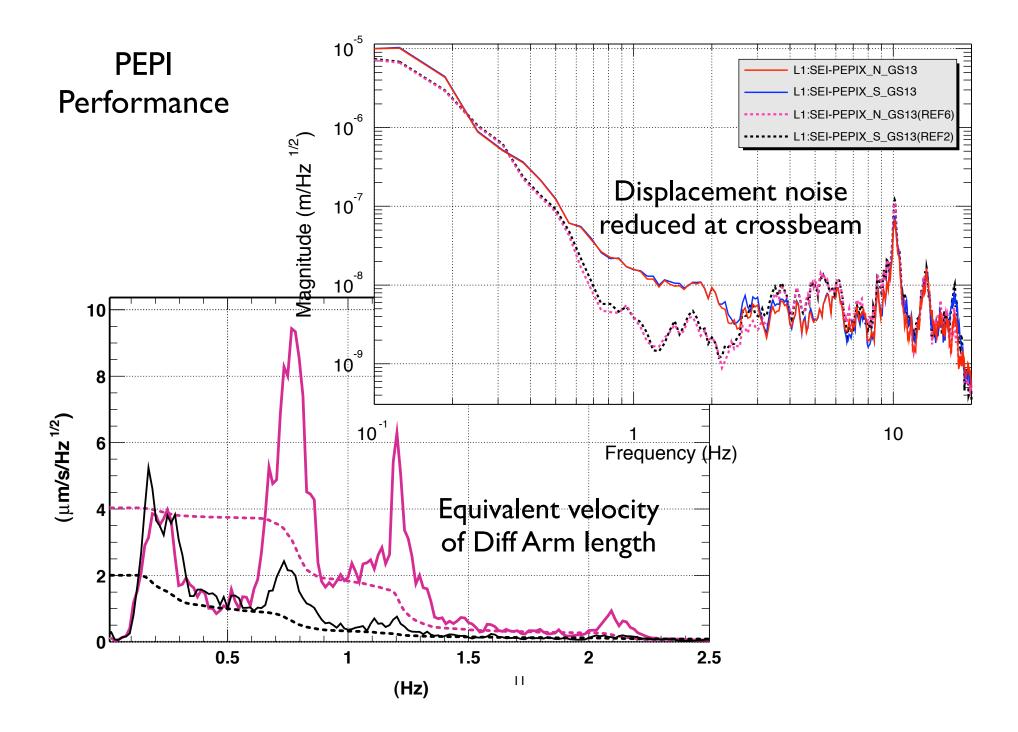
Feedback

PEPI: Piezoelectric pre-isolation

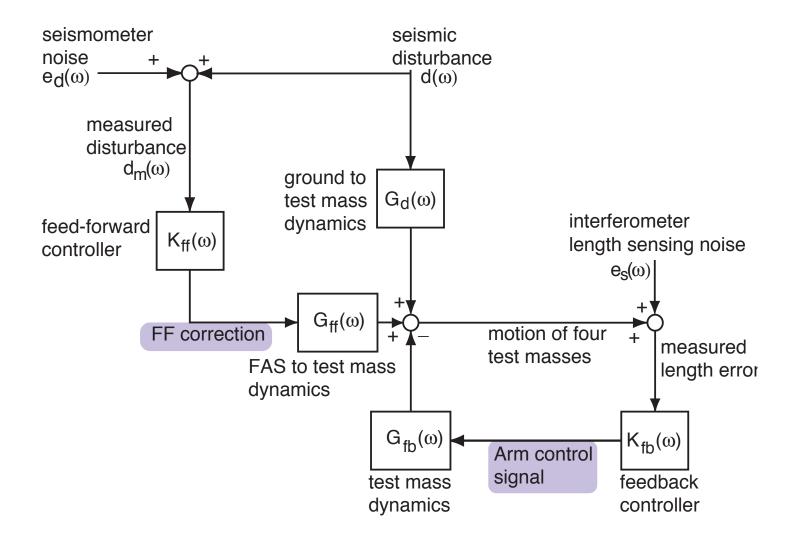


SISO controller, East and West

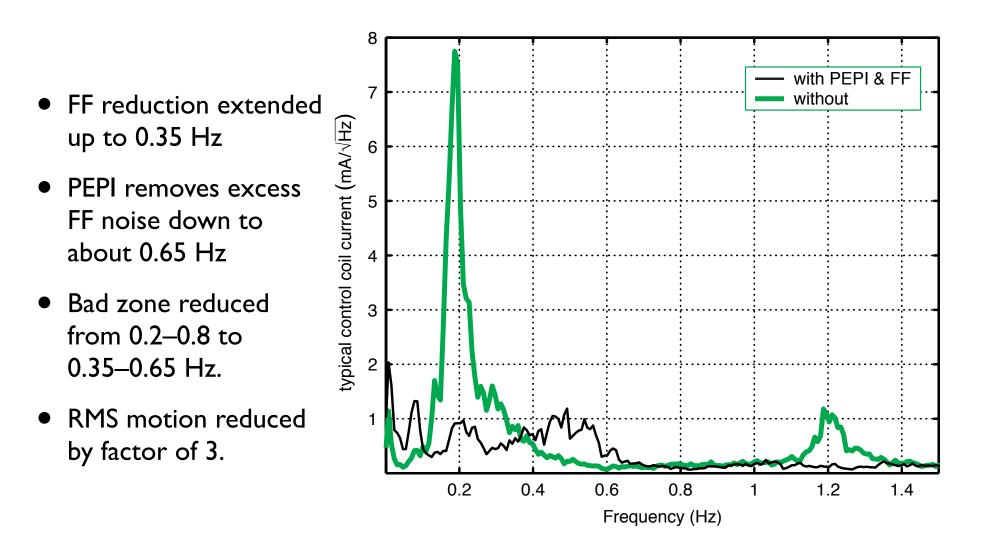
- Feedback to piezoelectric 180 µm range external actuator from local geophones placed on test mass chamber crossbeams.
- Goal is to reduce beam-direction disturbance to stack in the 0.6–3 Hz band.



Microseism Feedforward



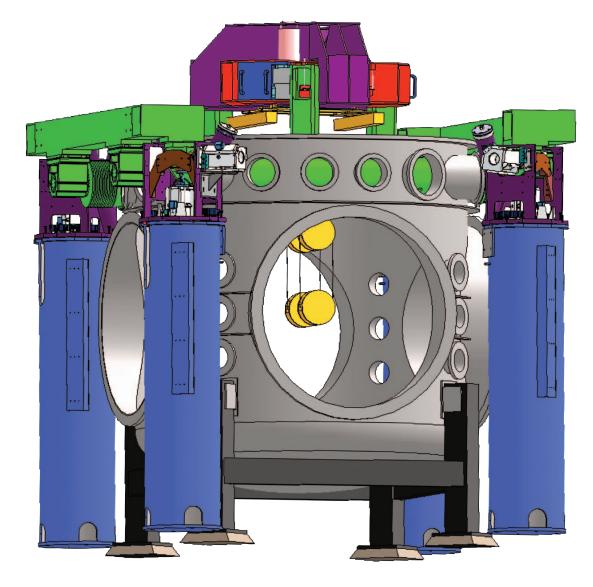
Combined PEPI/FF performance.



Seismic isolation for Advanced LIGO

Seismic isolation takes place in three places:

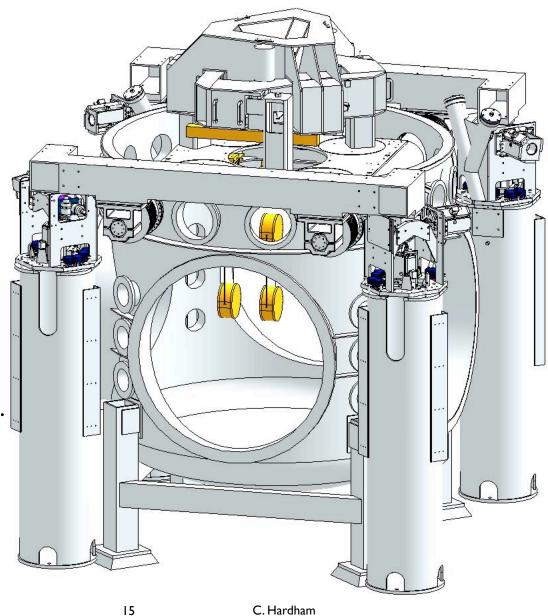
- Test mass suspension.
- 2-stage in-vacuum active (inertialfeedback) platform.
- External preisolation stage.



C. Hardham

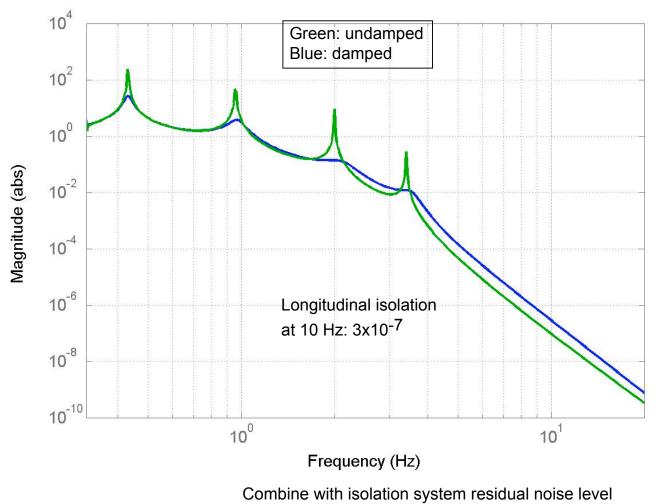
Quad Pendulum

- cascade of 4 pendulum stages
- isolates as 1/f⁸ above pendulum resonances
- I0⁻¹⁴ m_{rms} after global control
- $10^{-19} \text{ m}/\sqrt{\text{Hz}}$ at 10 Hz.



Quadruple Pendulum: Isolation Prediction

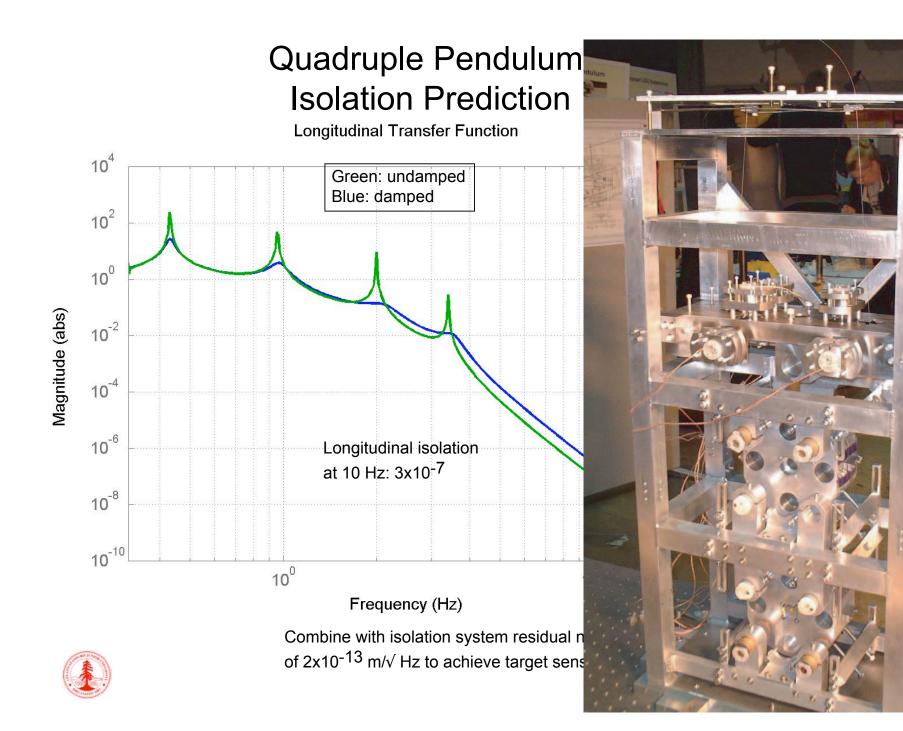
Longitudinal Transfer Function



of $2x10^{-13}$ m/ \sqrt{Hz} to achieve target sensitivity





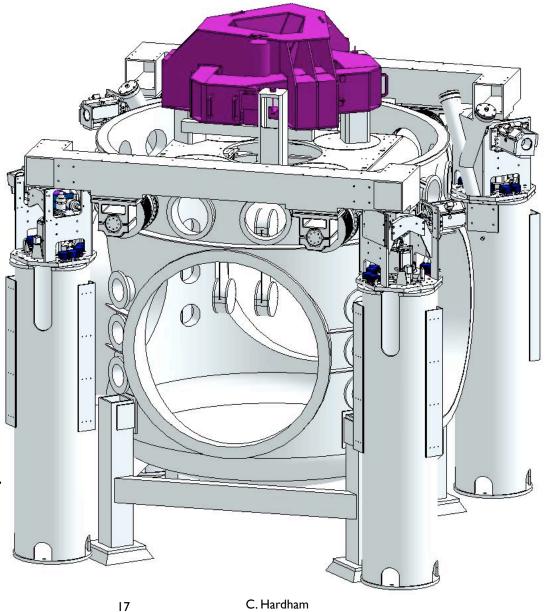


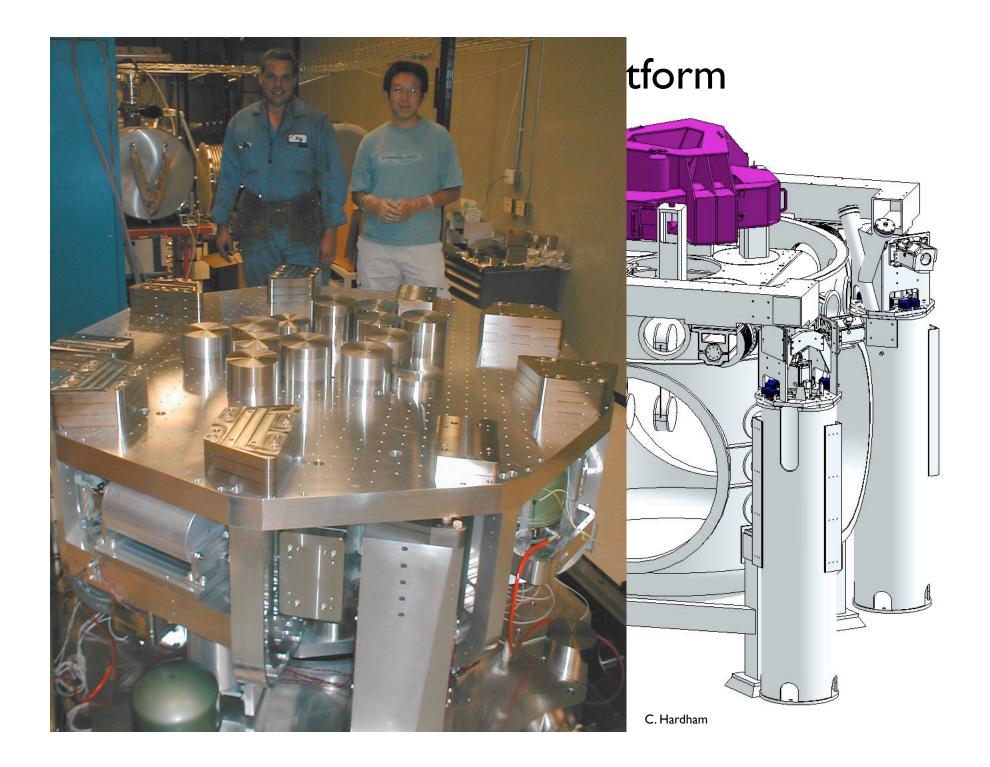
2 Stage active platform

- Local feedback in 6 DOFs per stage to (inertial) seismometer and (relative) displacement sensors
- Also, local sensor correction based on local seismometers.
- Should reduce the noise to:

 $10^{-11} \text{ m}/\sqrt{\text{Hz}}$ at 1 Hz.

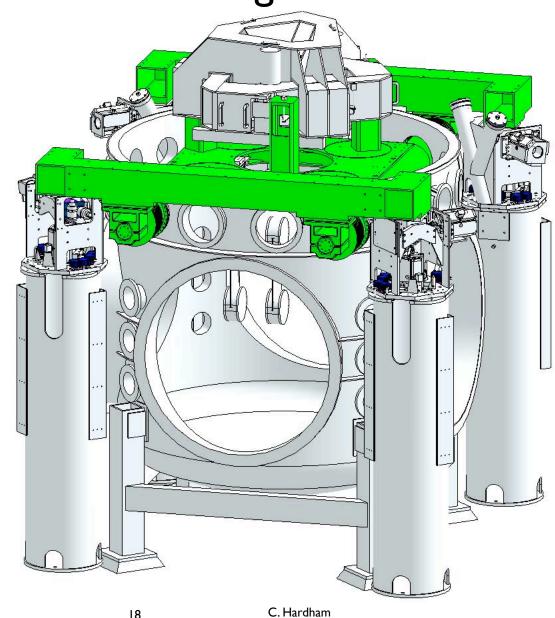
$$2 \times 10^{-13} \text{ m}/\sqrt{\text{Hz}}$$
 at 10 Hz.





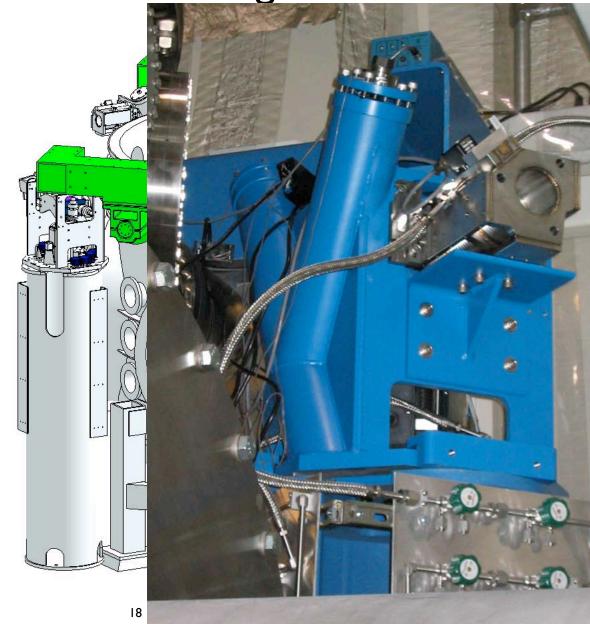
Pre-Isolator Stage

- Outside-of-vacuum stage, actuated by hydraulic bridge devices: I mm range and 6 DOFs
- Noise reduction largely due to local feedforward and sensor correction.
- Microseism through several hertz noise reduced by approx 10.



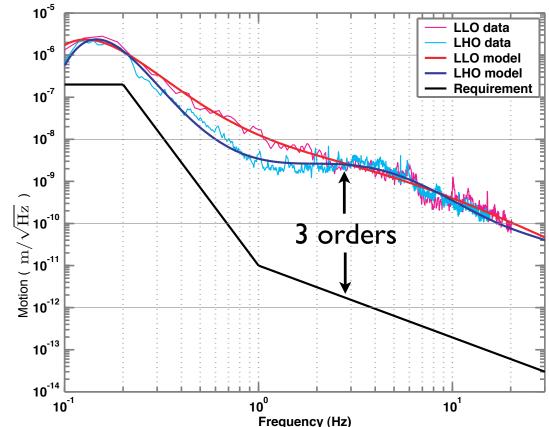
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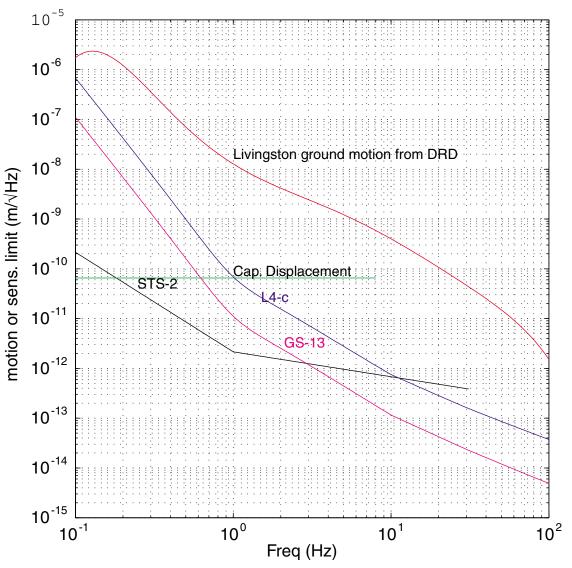
Adv. LIGO seismic isolation requirements.

- Design requirements are based on Adv LIGO 'system' design, to avoid seismic noise's ever adding to detector noise floor.
- two-stage active platform could meet the requirements at LHO and the quiet times at LLO.
- The external hydraulic stage will bring LLO into compliance as well.
- Seismic team spending most of its time on the retrofit at LLO; BTL will talk on this.

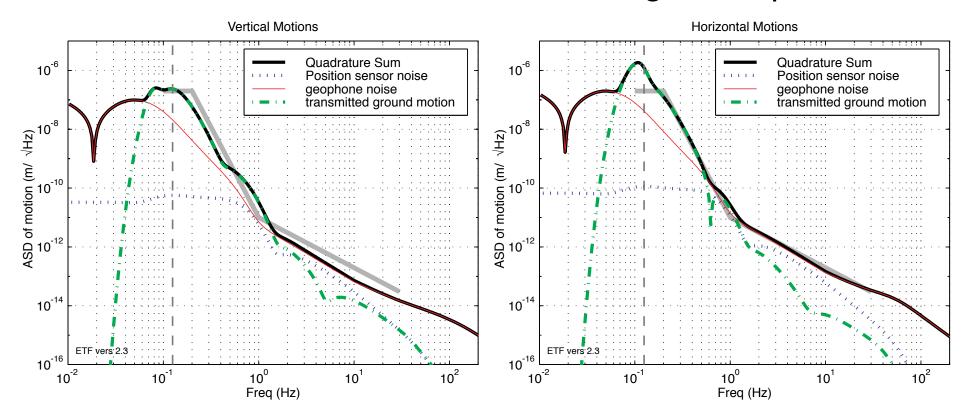


Sensor blending

- Servo error signal derived from 'Super-sensor,' a blended combination of displacement and inertial sensors, constructed for each controlled DOF, to minimize noise and artifacts.
- At very low frequencies locally follow displacement sensors, corrected by ground noise measurements and global interferometer signals.
- Mid frequency noise reduced by sensor correction and local inertial feedback.
- High frequencies get local inertial feedback.



Noise/ isolation model results for two-stage active platform

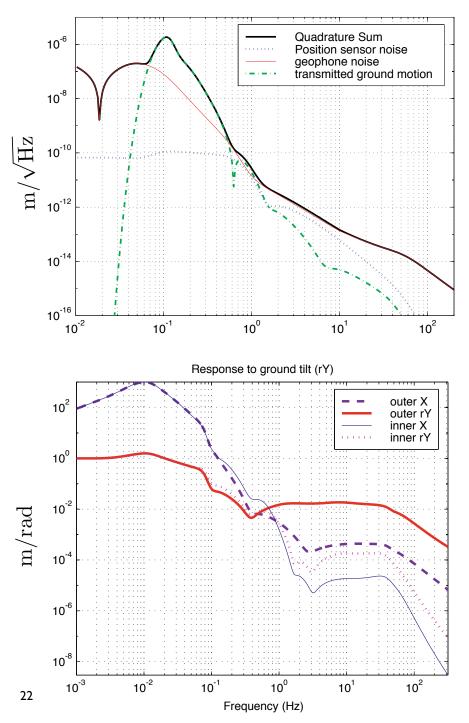


Performance estimates from dynamic model

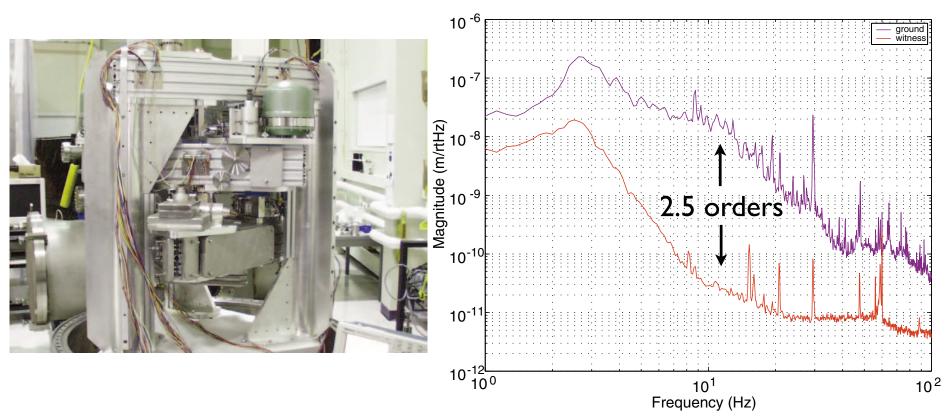
	displacement	pitch	yaw
ASD at 10 Hz	$2 \times 10^{-13} \text{ m}/\sqrt{\text{Hz}}$	$4 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$	$4 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$
RMS deviation	$1 \times 10^{-11} \mathrm{m}$	3×10^{-11} rad	2×10^{-11} rad
RMS velocity	$1 \times 10^{-10} \text{ m/s}$		

Tilt-horizontal study

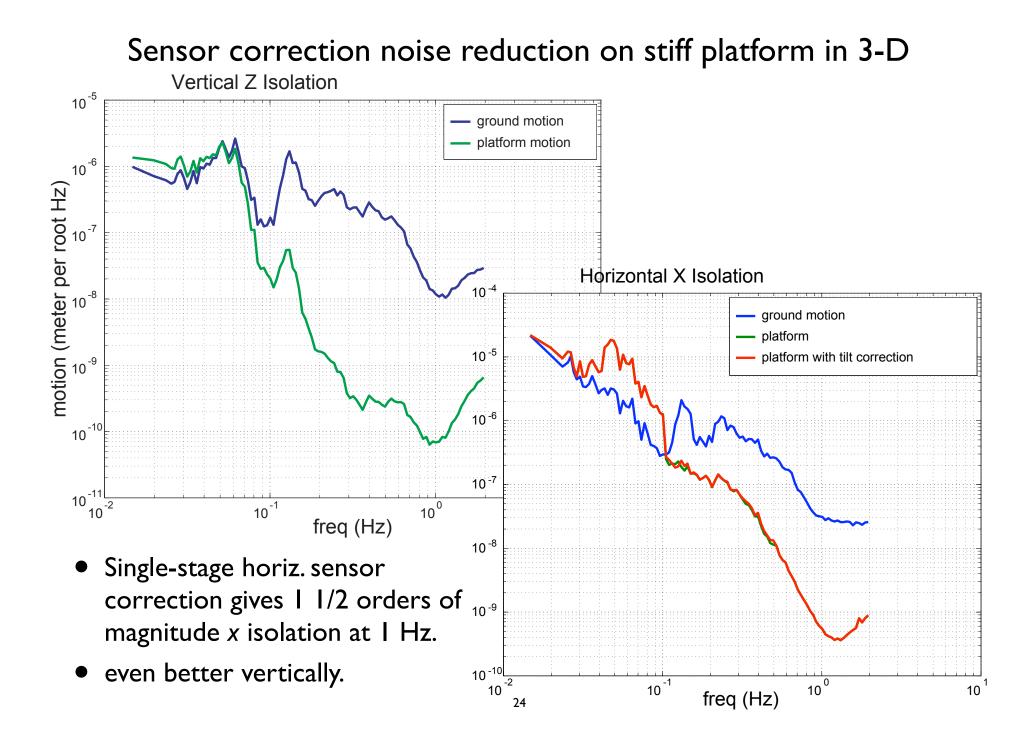
- 6 DOF dynamic model used to study our sensitivity to the tilthorizontal coupling inherent in low-frequency feedback to inertial sensors.
- A slab tilt step function causes highly-damped horizontal excursion.
- 5 tons of equipment moved across VEA slab causes *slow* 0.5 mm excursion.
- Thanks to the LIGO-1 slab designers!
- $1 \times 10^{-8} \text{ rad}/\sqrt{\text{Hz}}$ expected ground tilt causes insignificant horizontal motions at microseism.



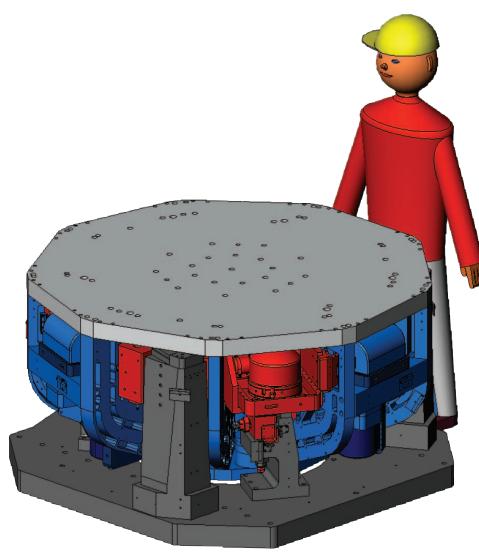
Proof-of-concept test of active platform



- Technique: feedback from inertial sensors (seismometers).
- Two stages give 2 1/2 orders of magnitude noise reduction at 10 Hz.
- Designed to test sub-hertz noise reduction and robust two-stage (12 DOF) controller.

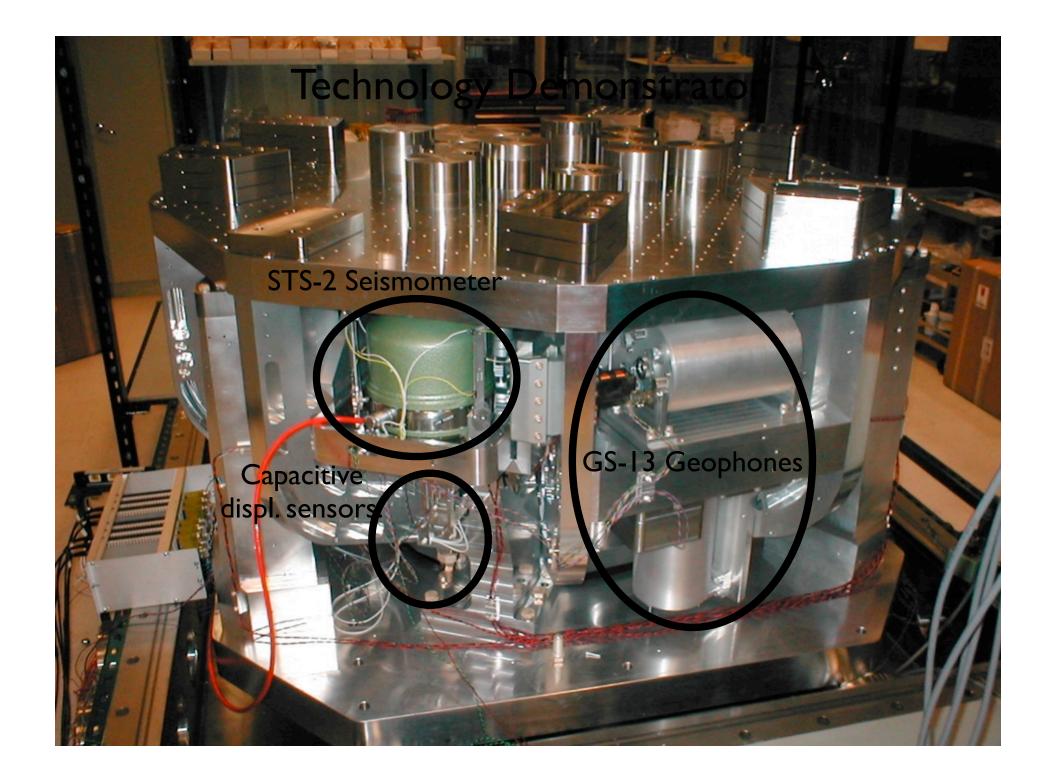


Technology Demonstrator at Stanford's ETF

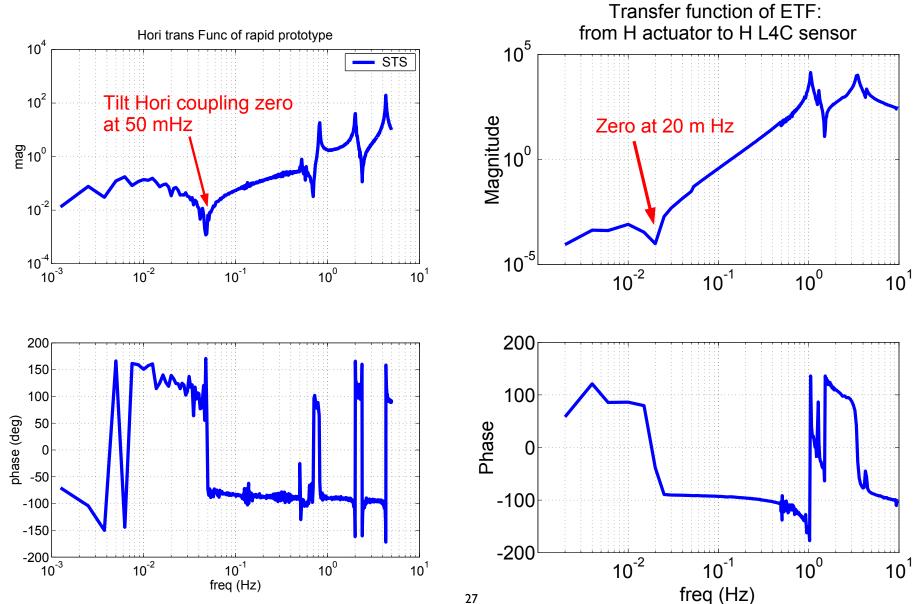


- Intended to test Adv LIGO SEI in-vacuum platform technology
- Dynamic tests underway, isolation servo design underway.
- Uses the same topology, instrumentation and materials as we expect to use in Adv LIGO's HAM chamber, except:
 - Payload about half.
 - actuator materials and cleaning appropriate for HV, not UHV.
 - Fits in slightly smaller ETF chamber.
 - Smaller area (higher noise) displacement sensors.



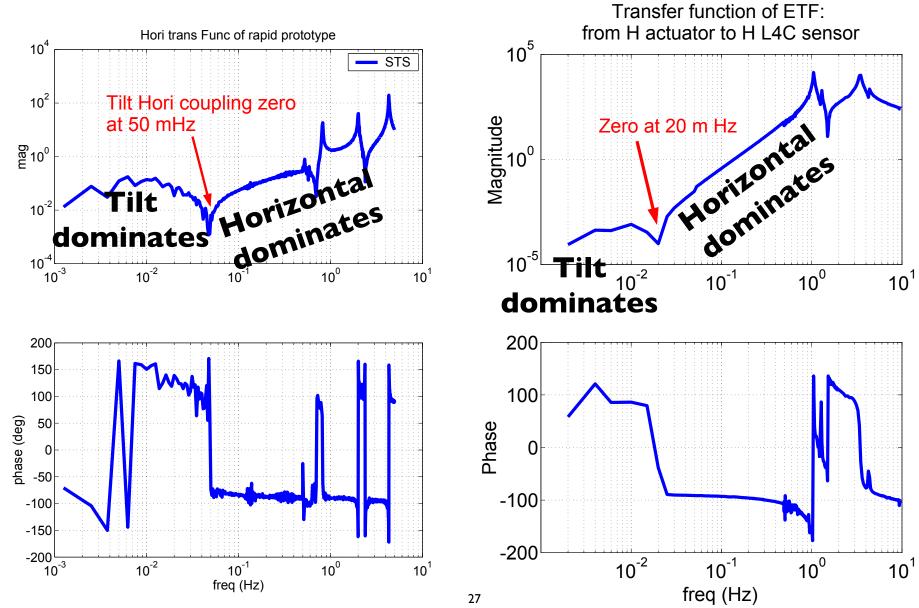


Reduced mechanical tilt-horizontal coupling

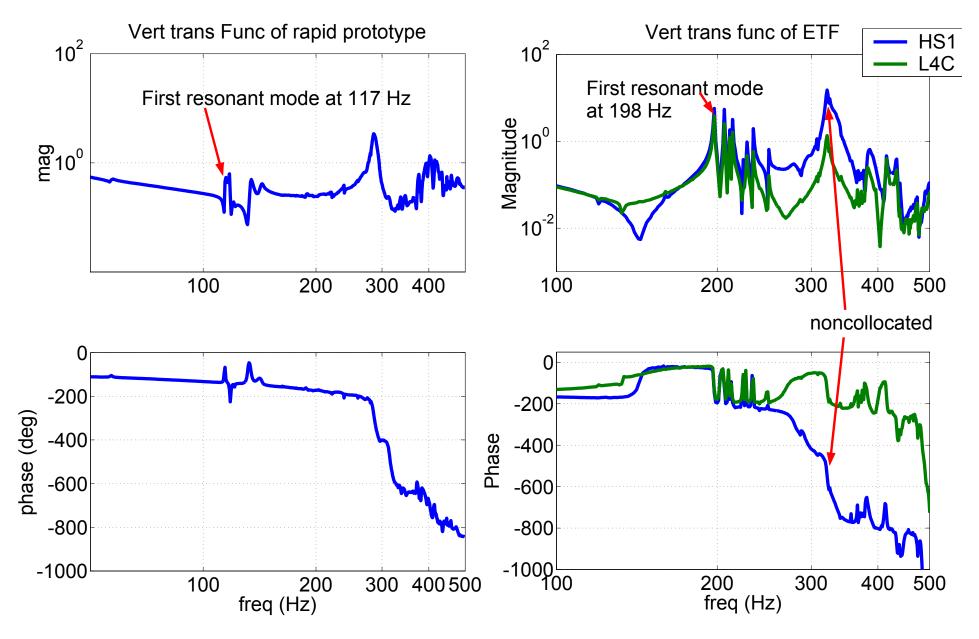


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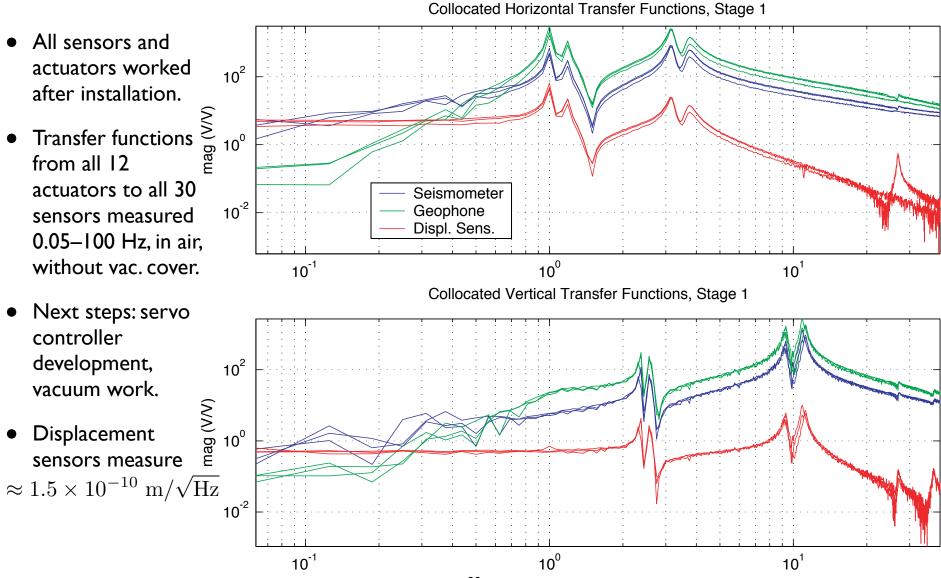
Reduced mechanical tilt-horizontal coupling



Increased structural resonance frequencies



Tech. Demo. Characterization



Development schedule & challenges

- LASTI Prototype 2-stage platforms:
 - Mechanical design should begin 9/'03; LIGO contracting with 1 or 2 design/fab firms to produce the HAM and BSC platforms. LIGO/LSC effort will be focussed on control systems.
 - Sensor & actuator specification and electronics design in parallel with mech. design.
 - Hardware ought to be ready by end of '04. Then follows commissioning, sys-id, controller design, and testing at LASTI.
- Adv LIGO SEI design reviews in 4/'05 (PDR) and 11/'05 (FDR), if things go well.
- Challenges, to be addressed during LASTI phase:
 - ≈30 systems in LIGO, each with 12 DOFs, can't easily be hand-tuned, and so sys-id and tuning of baseline controller should be automated.
 - Control-room supervision of these servos needs to be easier to use than systems of similar complexity in LIGO-1.