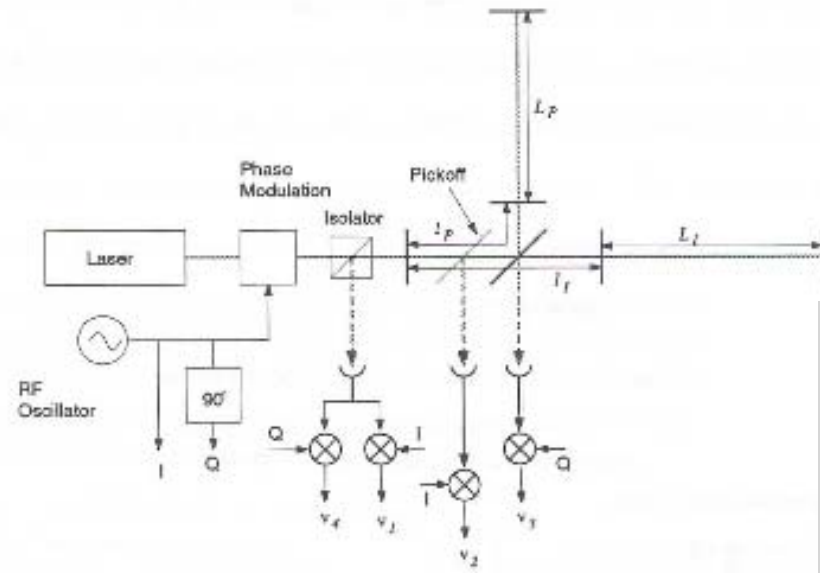




Next to lowest order approximation of LIGO I

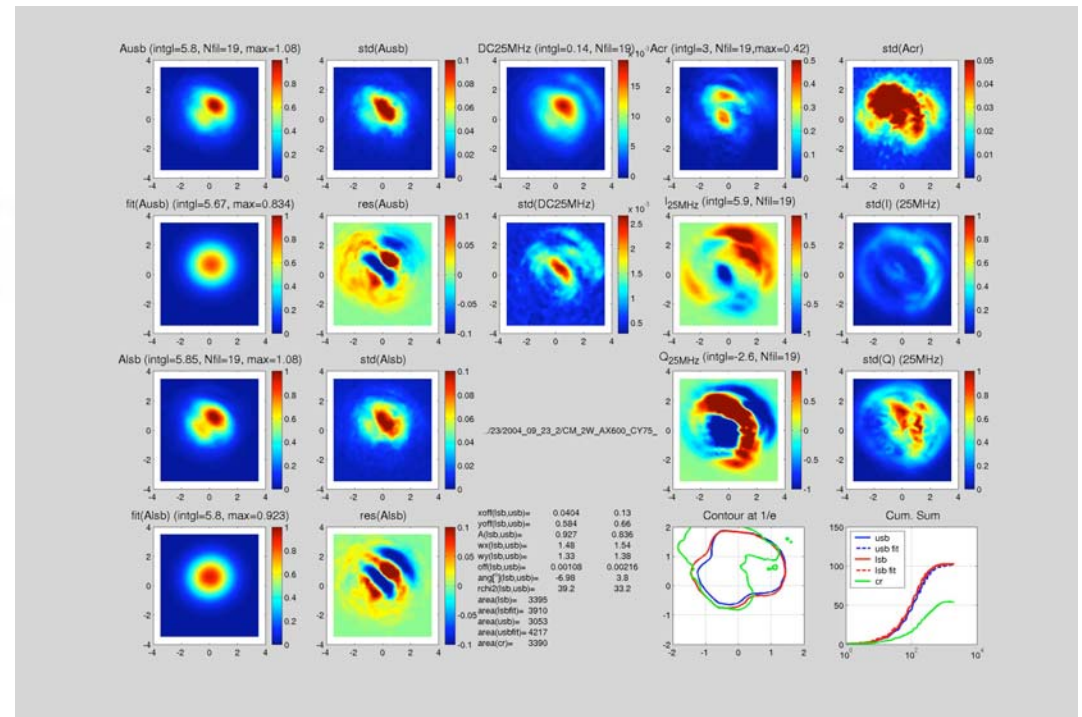
Figure 1.6 Signal extraction scheme.



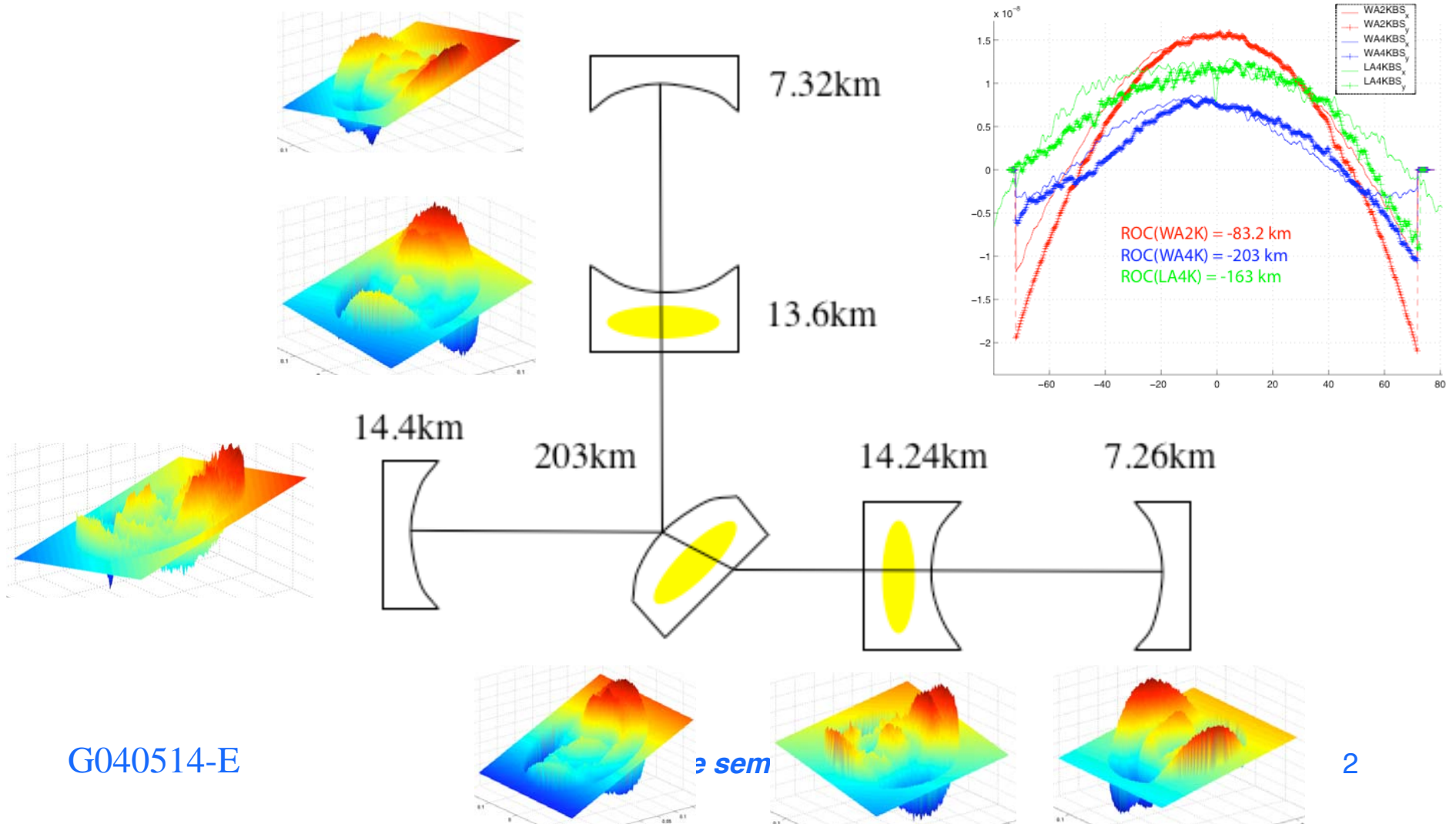
LIGO 1994

Hiro Yamamoto

LIGO 2004



With a little bit of reality





A simplified picture of

- ❑ “What’s going on ?”
- ❑ Thermal lensing
- ❑ Sideband imbalance
- ❑ Effect of locking
- ❑ Output Mode Cleaner
- ❑ Optical gain, Spob, contrast defect, etc, etc
- ❑ Correlation between DC-pitch/yaw and WFS signal



Tools

Tool	Pros	Cons
Analytic calculation	<input type="checkbox"/> Underlying mechanism can be understood	<input type="checkbox"/> Only simplified case can be analyzed
e2e	<input type="checkbox"/> Time evolution can be traced <input type="checkbox"/> Semi-realistic sensing and controls can be included	<input type="checkbox"/> Limited spatial profile <input type="checkbox"/> No details of optics
FFT	<input type="checkbox"/> Details of optics can be included (Phase map, Thermal lens)	<input type="checkbox"/> Only static

Modal Model, not so bad

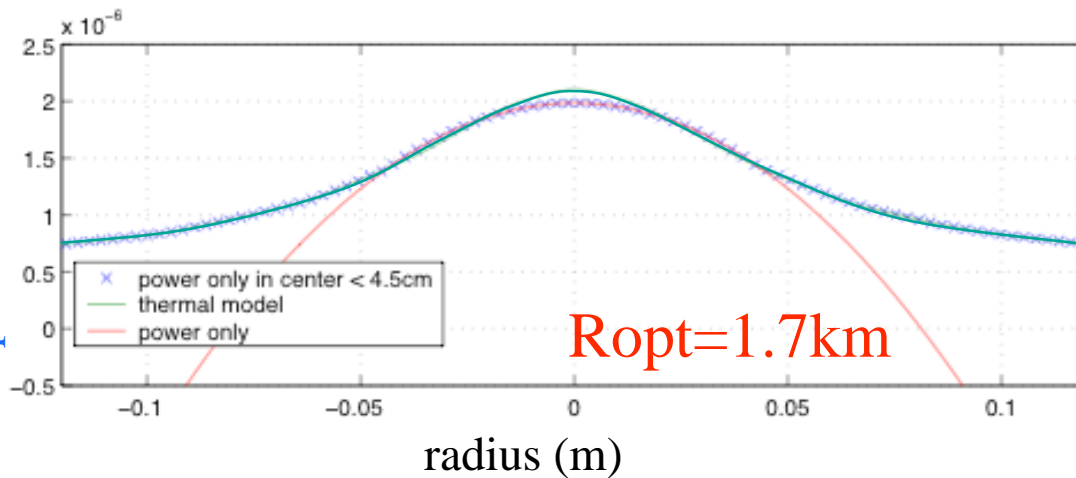
- » Modal Model can be used to study degenerate and/or unstable cavity
- » Valid only when perturbation is small
- » Field source mode is more important than cavity eigenstates



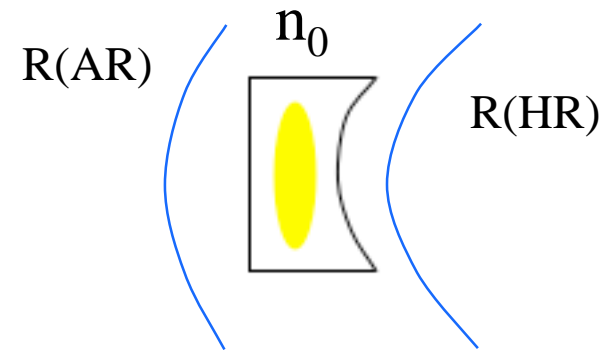
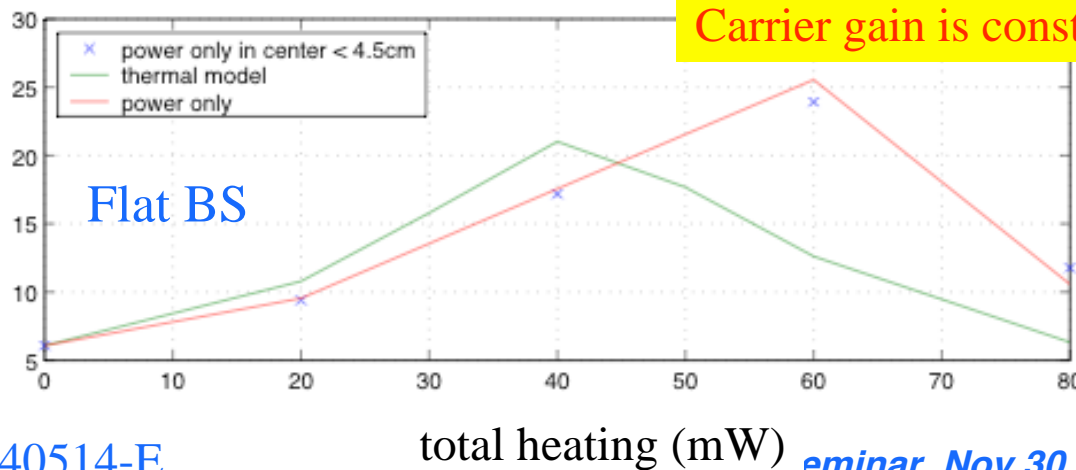
Thermal lensing and $n_{\text{effective}}$

- P. Willems calculated based on MIT model -

Optical thickness @ 1w



Sideband recycling gain



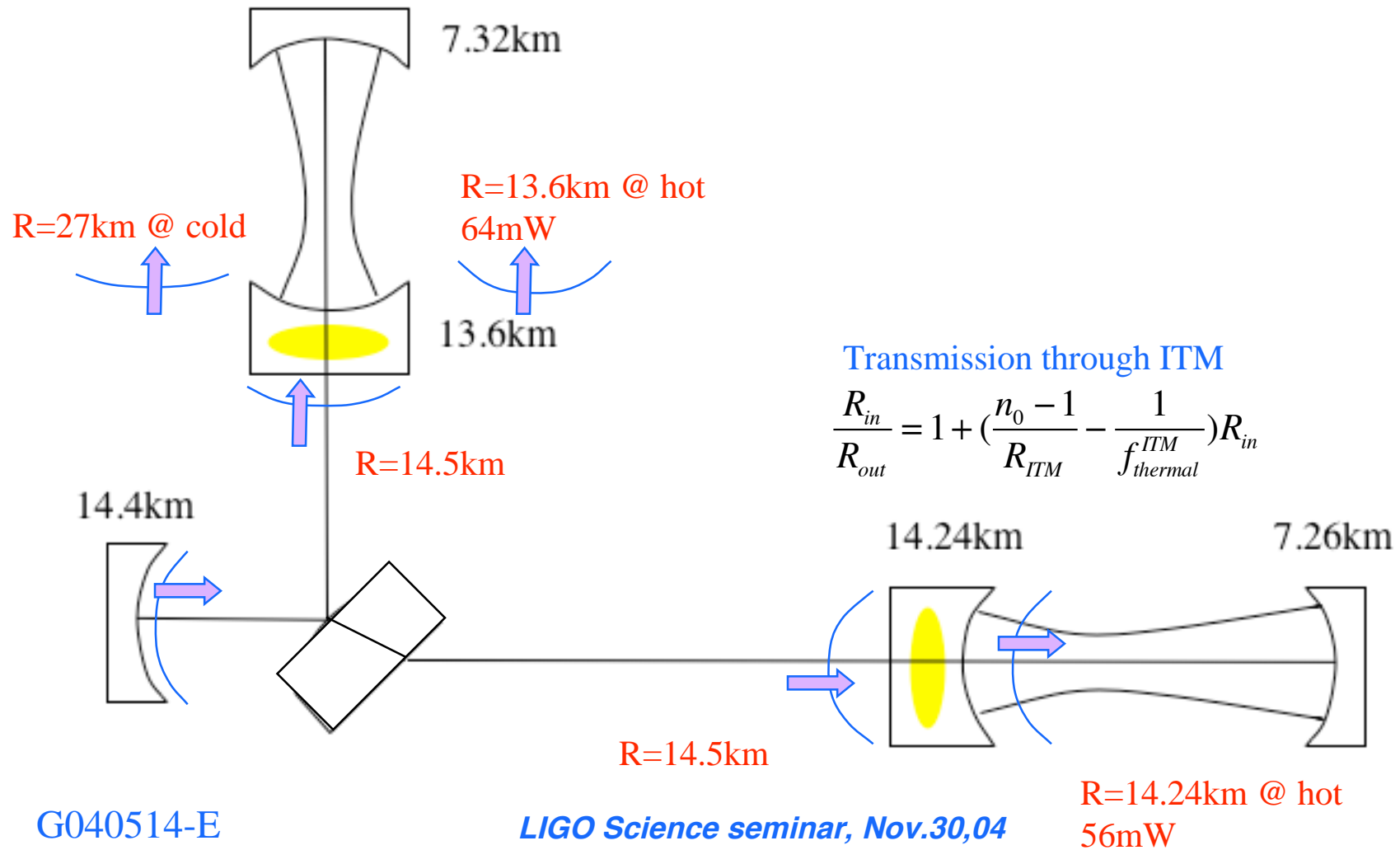
$$\frac{1}{f} = -\frac{n_0 - 1}{Rm} + \frac{Power}{Ropt}$$

$$= -\frac{n_{\text{effective}} - 1}{Rm}$$

$$\frac{1}{R_f(HR)} = \frac{1}{R_f(AR)} - \frac{1}{f}$$

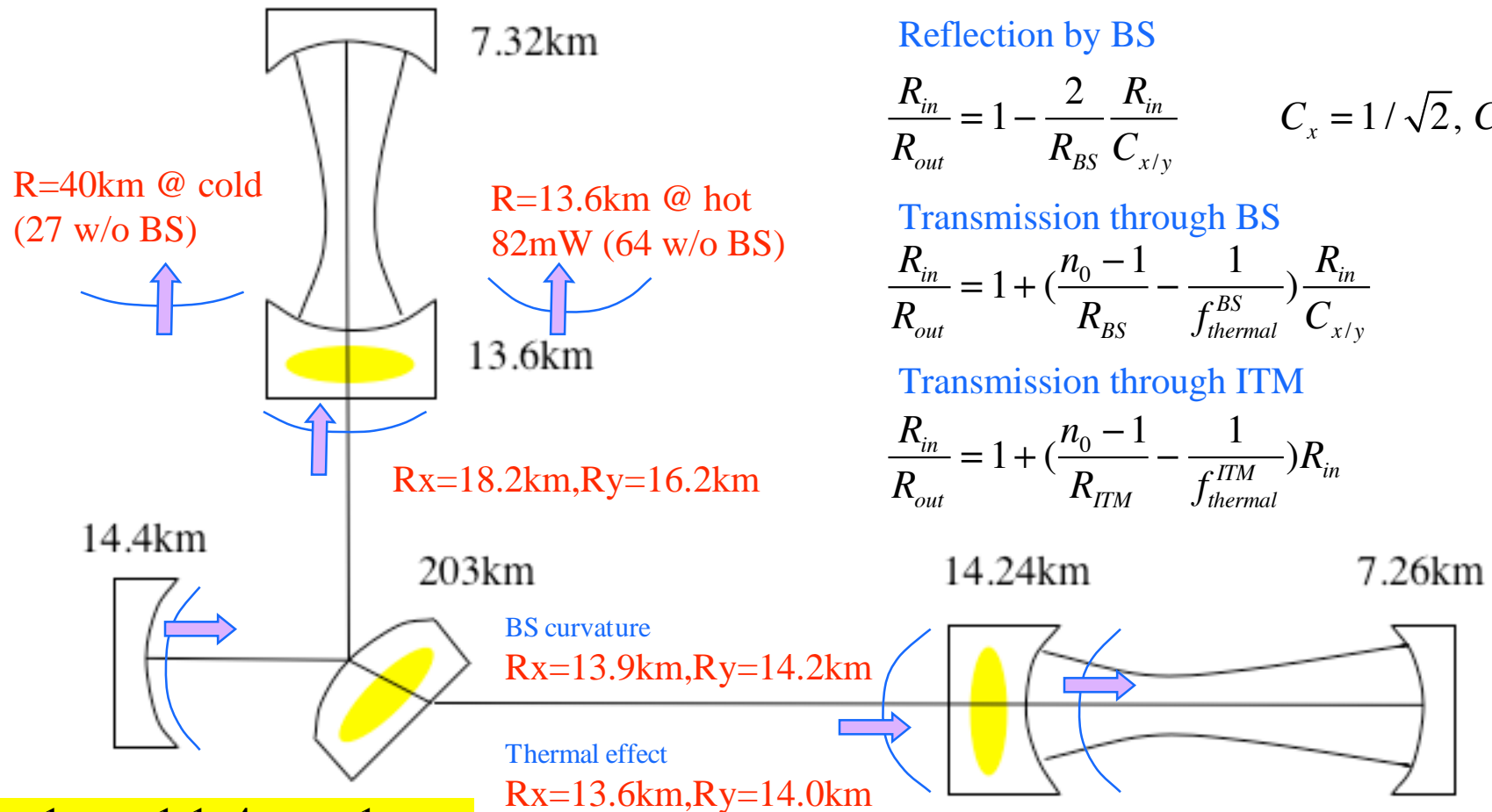
Power = 58mW

Mode matching





Mode matching with BS



Reflection by BS

$$\frac{R_{in}}{R_{out}} = 1 - \frac{2}{R_{BS}} \frac{R_{in}}{C_{x/y}} \quad C_x = 1/\sqrt{2}, C_y = \sqrt{2}$$

Transmission through BS

$$\frac{R_{in}}{R_{out}} = 1 + \left(\frac{n_0 - 1}{R_{BS}} - \frac{1}{f_{thermal}^{BS}} \right) \frac{R_{in}}{C_{x/y}}$$

Transmission through ITM

$$\frac{R_{in}}{R_{out}} = 1 + \left(\frac{n_0 - 1}{R_{ITM}} - \frac{1}{f_{thermal}^{ITM}} \right) R_{in}$$

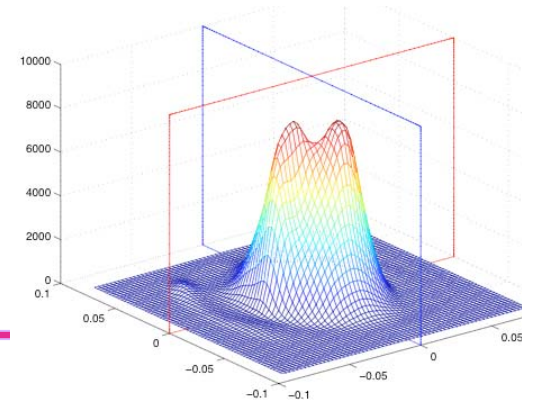
$$\frac{1}{f_{thermal}^{BS}} = \frac{1}{2} \frac{1}{2} \frac{4}{10} \frac{1}{f_{thermal}^{ITM} (hot)}$$

LIGO Science seminar, Nov.30,04

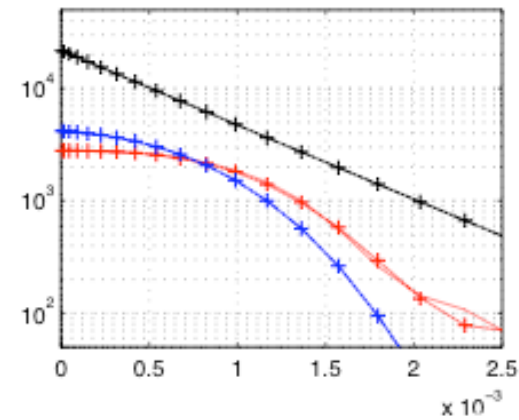
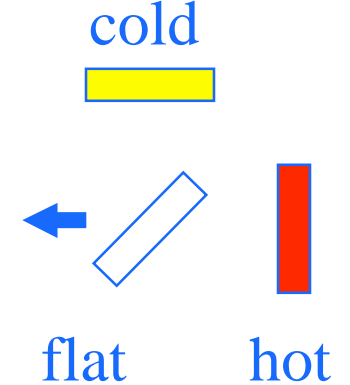
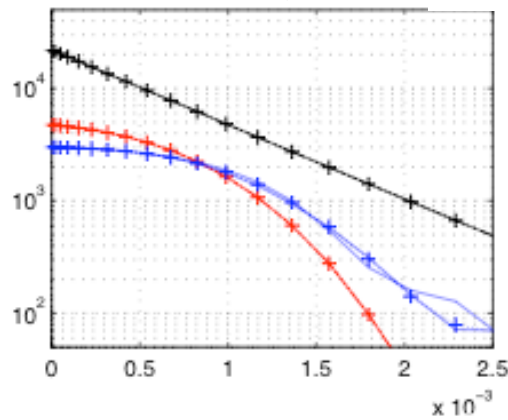
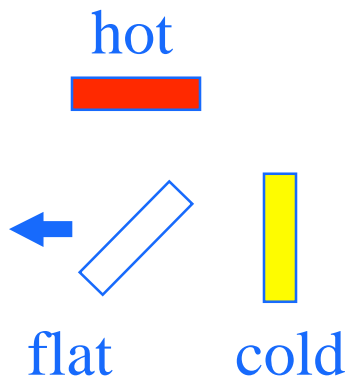
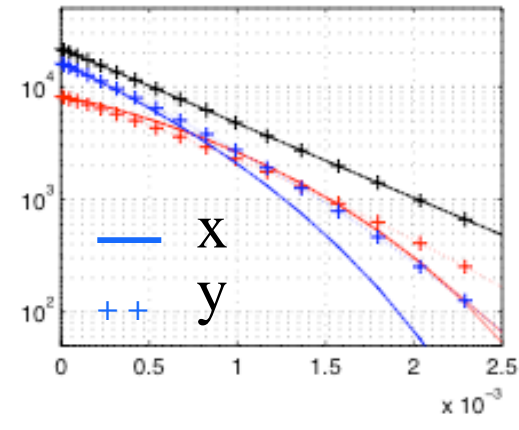
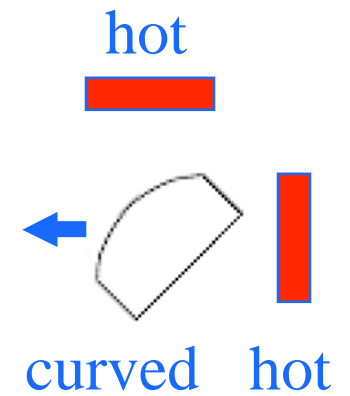
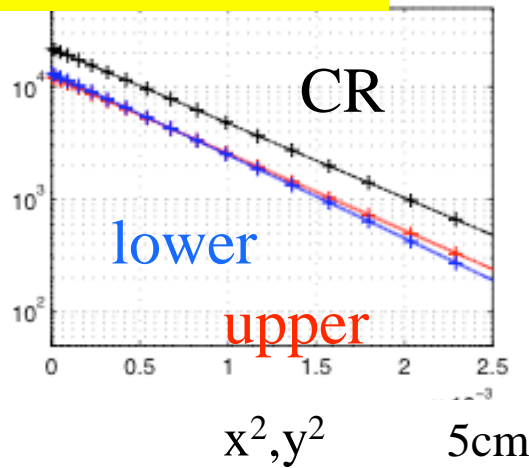
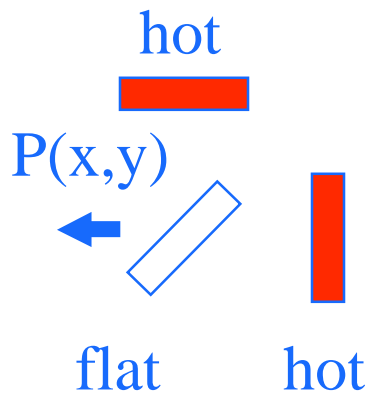
$R=14.24\text{km}$ @ hot
52mW (54 w/o BS)
only BS effect



LIGO ITM differential heating and beam splitter curvature



- Linear line : gaussian
- Blue vs red : sideband imbalance
- --- vs + + + : astigmatism





Effects of mode matching in PRM

- Carrier field is insensitive to thermal state of ITMs and BS curvature
 - » CR reflected by arm does not have higher mode excited
 - » SB reflected has higher order mode excited due to curvature mismatch
- Michelson cavity can induce imbalance of upper and lower sidebands
 - » Oscillation phase part change sign, but Gouy phase and terms due to mode mixing are SB sign independent.
 - » Sideband imbalance in PRM is observable when two cavities in PRM are different

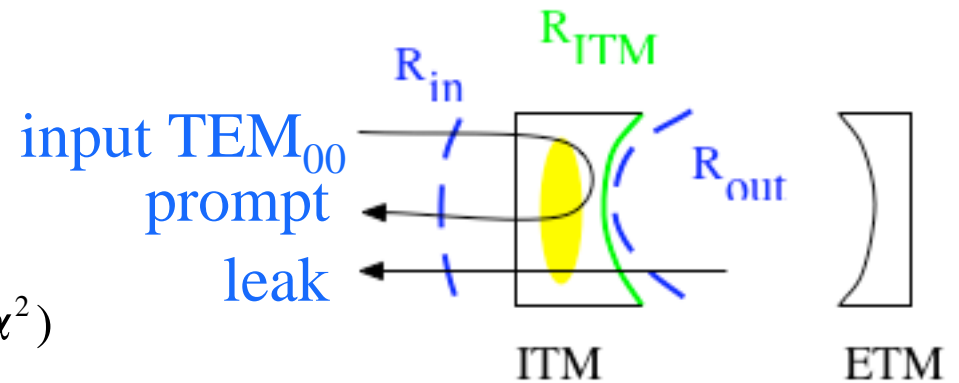
$$\text{Propagator} = 1 - r_{RM} \cdot r_{ITM} \cdot \exp(-i\phi)$$

$$\phi = k_{SB} \cdot d\ell_{snp} - c_1 \cdot \eta - c_2 \cdot \alpha^2$$

Reflection by arm cavity with curvature mismatch

$$\alpha = \frac{z}{z_0} \left(1 - \frac{R_{ITM}}{R_{out}} \right)$$

E_{mn} is the mode in PRC which couples to the arm when $\alpha=0$

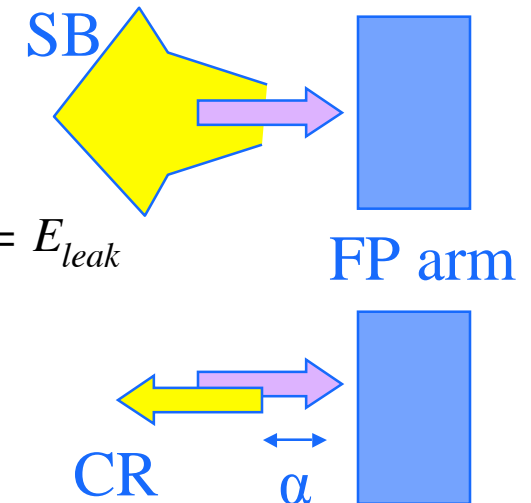


$$E_{SB} = \frac{1}{1+i\alpha} E_{00} - \frac{i\alpha / \sqrt{2}}{(1+i\alpha)^3} (E_{02} + E_{20}) + O(\alpha^2)$$

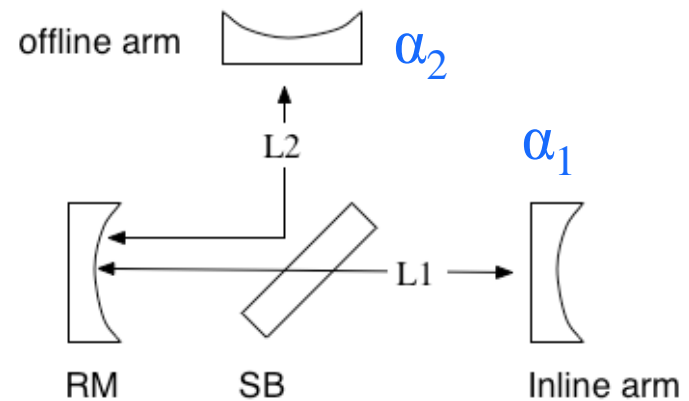
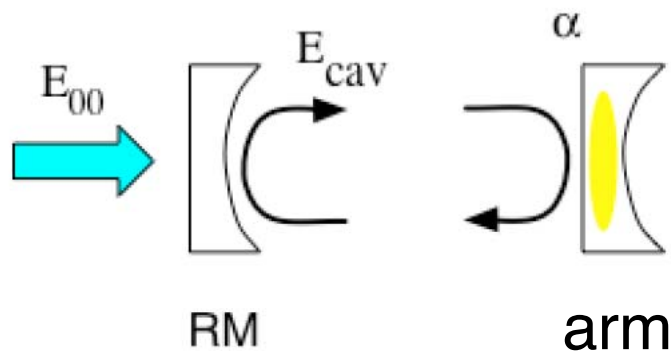
$$E_{CR} = \frac{1}{1+i\alpha} E_{00} - \frac{i\alpha / \sqrt{2}}{(1+i\alpha)^3} (E_{02} + E_{20}) + O(\alpha^2) \Leftarrow E_{prompt}$$

$$-2 \frac{1}{1+i\alpha/2} \left(\frac{1}{1+i\alpha/2} E_{00} - \frac{i\alpha/2 / \sqrt{2}}{(1+i\alpha/2)^3} (E_{02} + E_{20}) + O(\alpha^2) \right) \Leftarrow E_{leak}$$

$$= -\frac{1}{1+i\alpha} E_{00} + O(\alpha^2)$$



Sideband imbalance in curvature mismatched FPs



$$E_{cav} = \sum_{m,n} \frac{C_{mn}(\alpha) \cdot HG_{mn}}{1 - r_{RM} \cdot \exp(i\phi)}$$

$$\phi_{CR,00} = -2k_{CR}L + 2\eta_{00} - \arctan(\alpha)$$

$$\phi_{SB}(k_{SB}L) = \phi_{CR,00} - 2k_{SB}L + \delta\phi(\alpha, \eta)$$

$$\phi_{SB}(k_{SB}L, \alpha) \neq \phi_{SB}(-k_{SB}L, \alpha)$$

$$P(k_{SB}L, \alpha) \neq P(-k_{SB}L, \alpha)$$

$$k_{SB}L_1 = -k_{SB}L_2 = \frac{\pi \cdot \delta L_{syn}}{\lambda_{SB}}$$

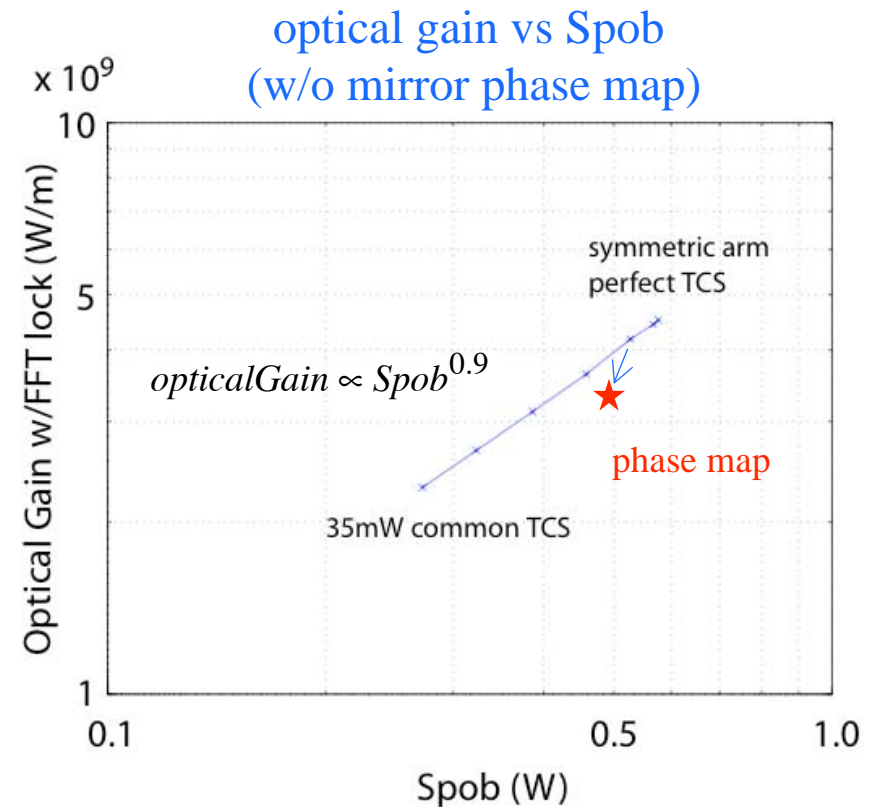
$$P(k_{SB}L_1, \alpha_1) = P(-k_{SB}L_2, \alpha_1)$$

$$\begin{aligned} &P(k_{SB}L_1, \alpha_1) + P(k_{SB}L_2, \alpha_2) \\ &= P(-k_{SB}L_1, \alpha_2) + P(-k_{SB}L_2, \alpha_1) \end{aligned}$$



I/O performance

	Lock	CR gain	Upper SB gain	Lower SB gain	Contrast Defect $\times 10^{-6}$
symmetric arm, best TCS	FFT	46	23.7	23.7	58
As built arm, best TCS	FFT	46	21.7	25.3	220
As built arm, com.TCS	FFT	46	19.6	24.6	233
	LSC	46	22.3	22.3	244
As built arm, com.TCS w/ phase map	FFT	36	18.3	23.3	429
	LSC	36	21.5	20.2	439



SB imbalance comes from R_{ITM} and R_{BS}

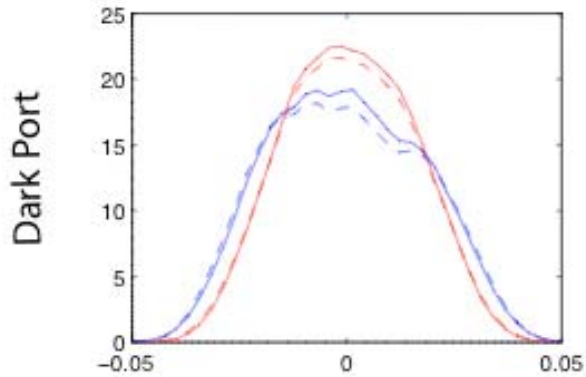


FFT vs LSC lock

$n(\text{ITM}_x) - n(\text{ITM}_y)$

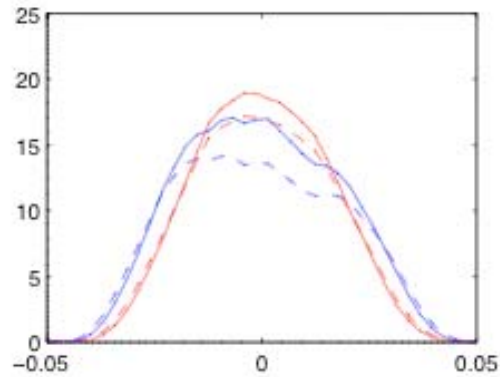
0.96-0.96

Symmetric Heating



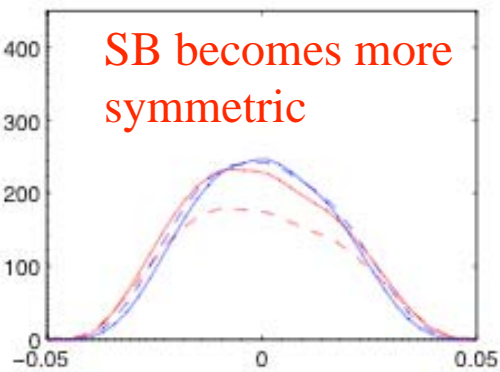
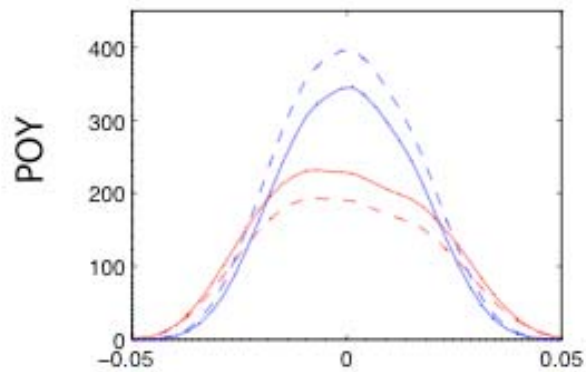
1.10-0.96

Differential Heating
ITMx cooler than ITMy



— lower SB — upper SB

- - - FFT lock — LSC lock

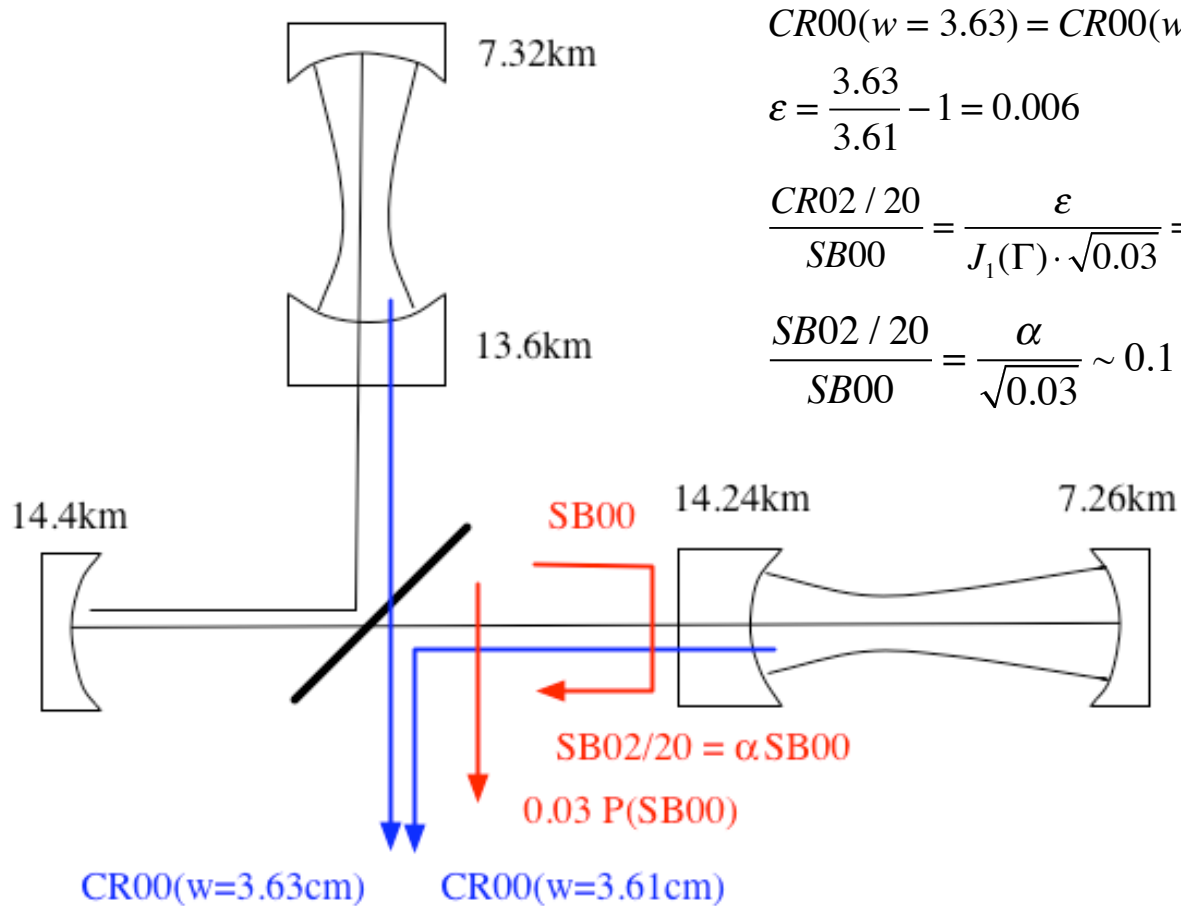


symmetric
differential

	FFT	LSC
θ_{CR}	0.3	-1.9
θ_{SB+}	-0.6	-2.3
θ_{SB-}	7.2	5.1
Spob	-0.57i	-0.57i
θ_{CR}	0.2	-8
θ_{SB+}	4.9	-1.2
θ_{SB-}	11.8	5.1
Spob	-0.48i	-0.50i



modes in the dark port - back on the envelope -



$$CR00(w = 3.63) = CR00(w = 3.61) + \varepsilon \cdot CR02 / 20(w = 3.63)$$

$$\varepsilon = \frac{3.63}{3.61} - 1 = 0.006$$

$$\frac{CR02 / 20}{SB00} = \frac{\varepsilon}{J_1(\Gamma) \cdot \sqrt{0.03}} = 0.15$$

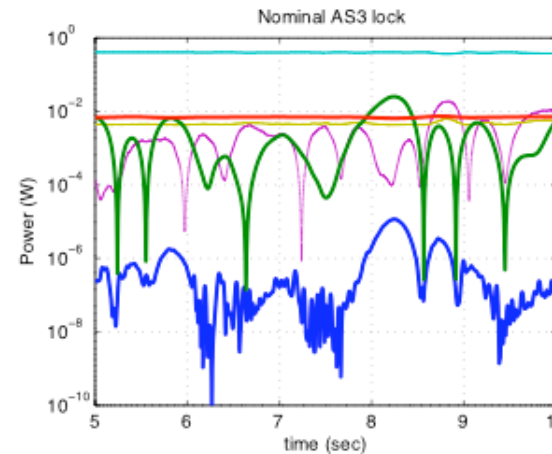
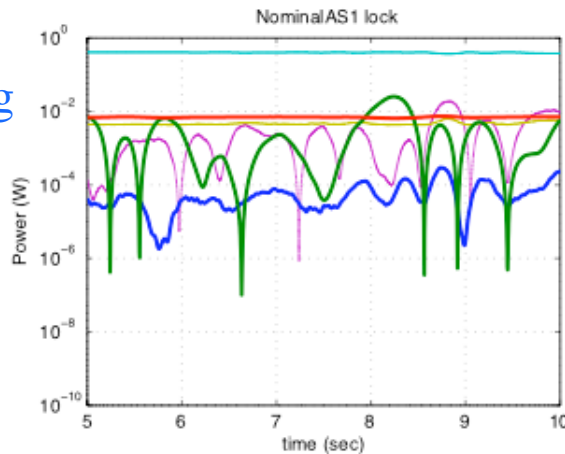
$$\frac{SB02 / 20}{SB00} = \frac{\alpha}{\sqrt{0.03}} \sim 0.1$$



modes in the dark port

- e2e simulation -

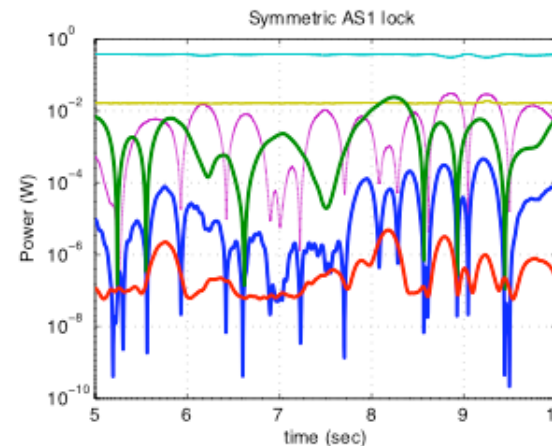
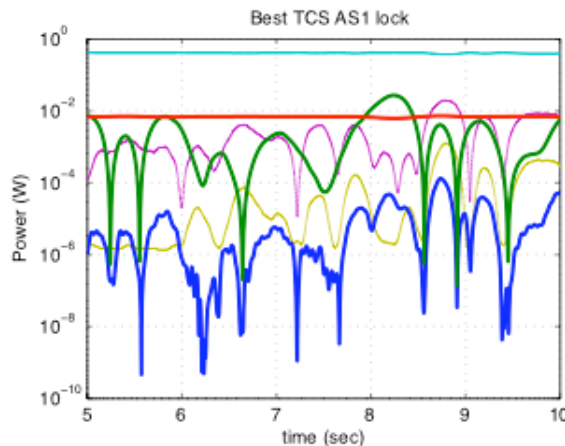
common heating
 $\alpha \sim 0.01$
use dark port
signal to lock



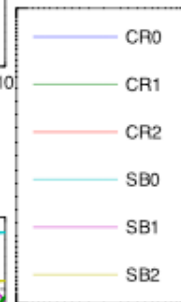
common heating
 $\alpha \sim 0.01$
use OMC output
signal to lock

time evolution of powers of various modes

differential
heating
 $\alpha \sim 0$
use dark port
signal to lock



Symmetric arm
common heating
 $\alpha \sim 0.01$
dark port signal

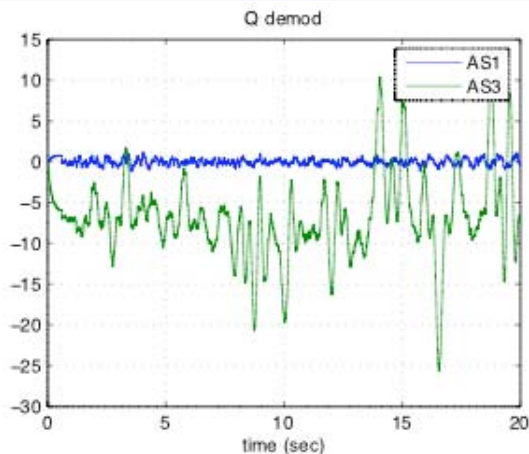




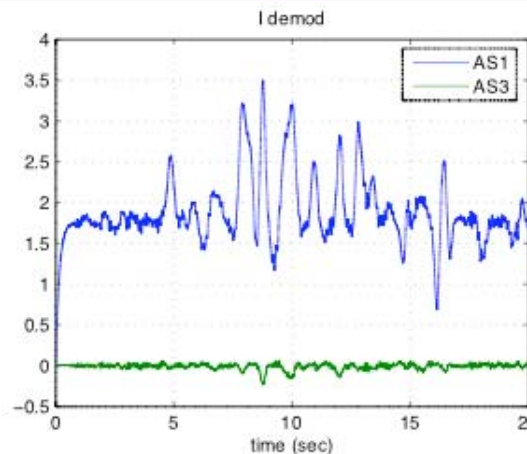
OMC and ASQ and ASI

(1) nominal matching

use dark port
signal to lock
common heating
 $\alpha \sim 0.01$



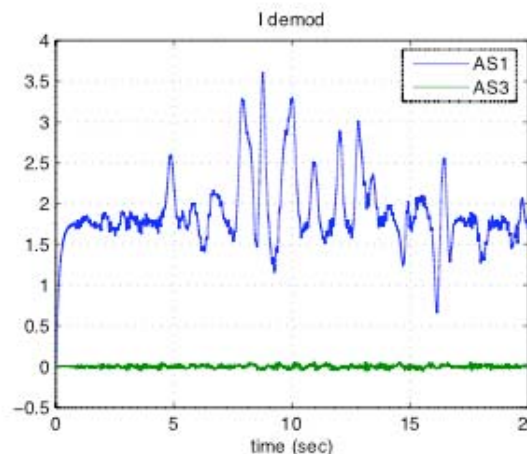
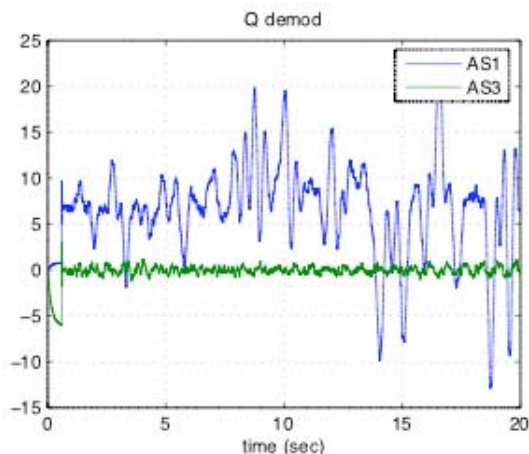
Q-demod



I-demod

AS1:
dark port
AS3:
OMC output

use OMC output
signal to lock
common heating
 $\alpha \sim 0.01$

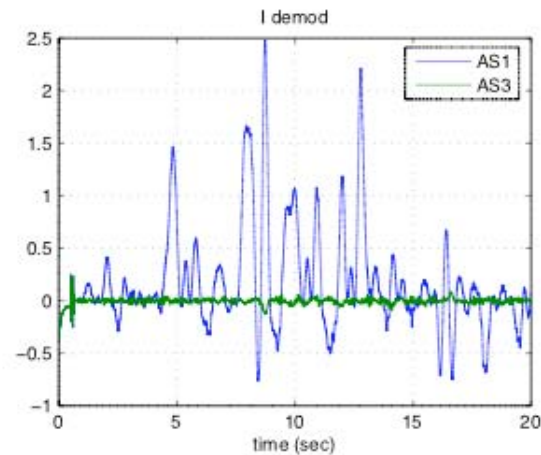
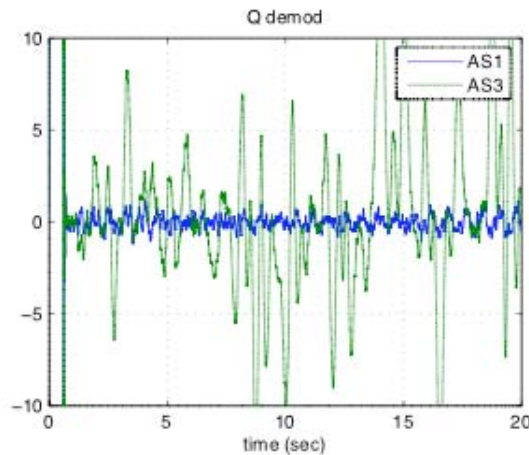




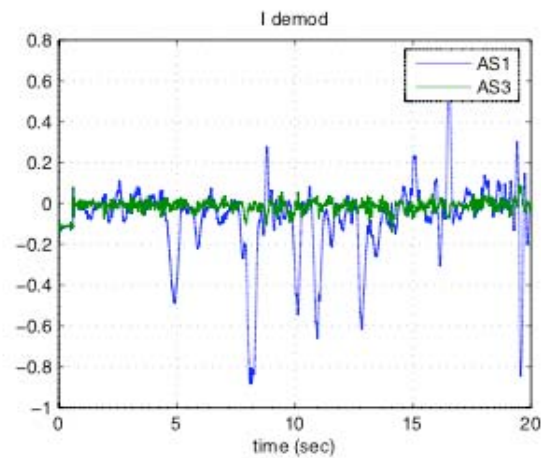
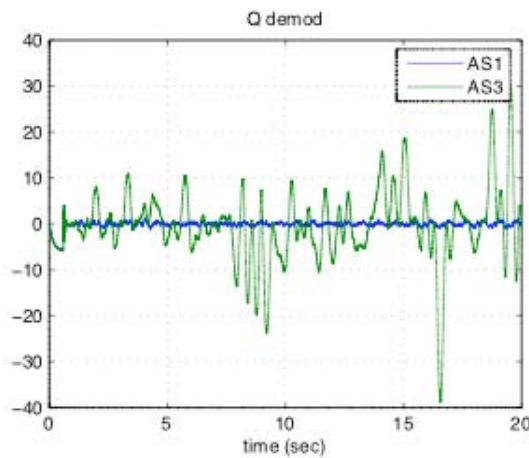
OMC and ASQ and ASI

(2) better matching

differential heating
 $\alpha \sim 0$
use dark port signal to lock



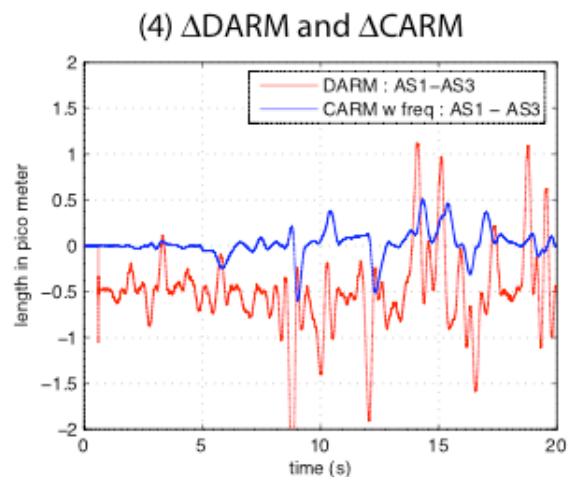
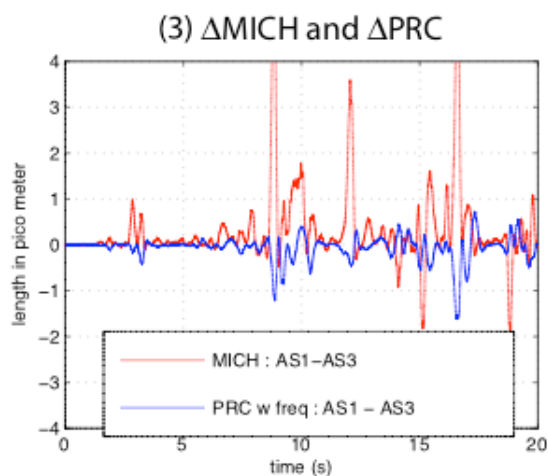
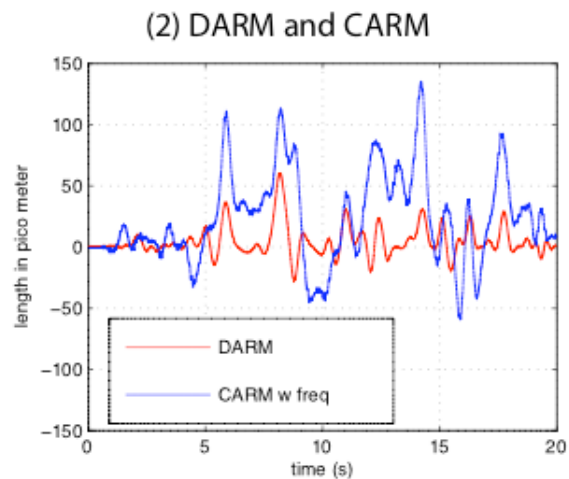
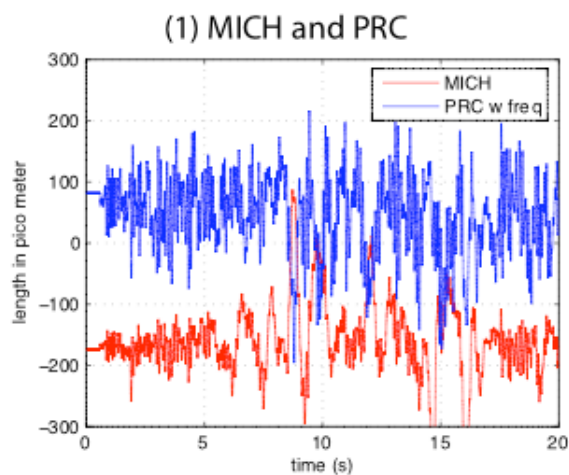
Symmetric arm
common heating
 $\alpha \sim 0.01$
dark port signal



G040514-E



Effect on length DOF





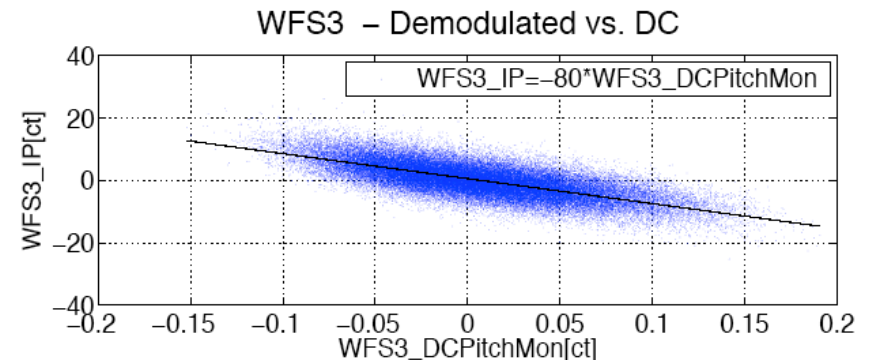
Beam positioning on WFS head

T030290(Luca,etc), eLog(Keita on Nov.18,04)

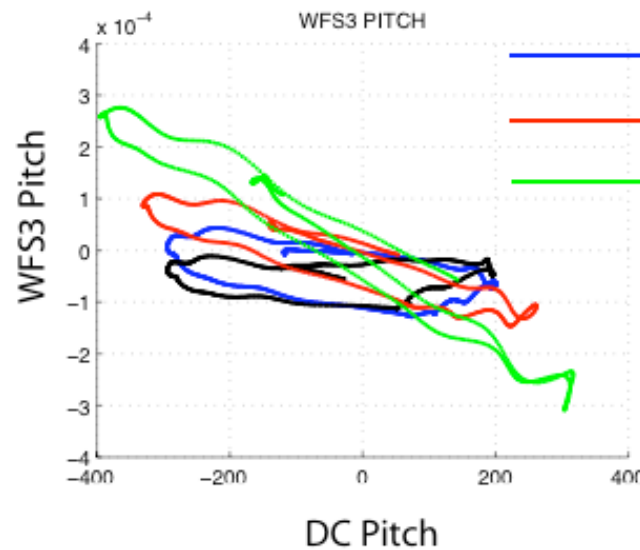
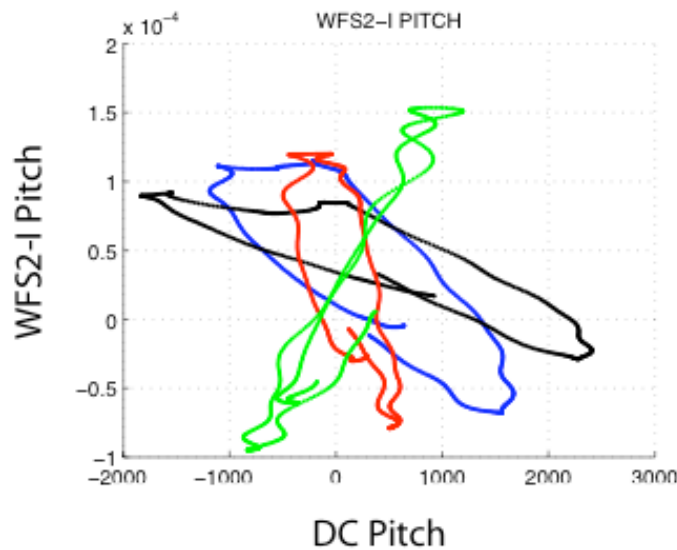


$$\text{DCpitch} = \text{DC}(\text{N}) - \text{DC}(\text{S})$$

$$\text{WFS} = \text{Q/I}(\text{N}) - \text{Q/I}(\text{S})$$



e2e simulation for 1.45 seconds at different thermal states



- Diff.TCS Best
- Com.TCS 98%
- Com.TCS 90%
- Com.TCS 80%

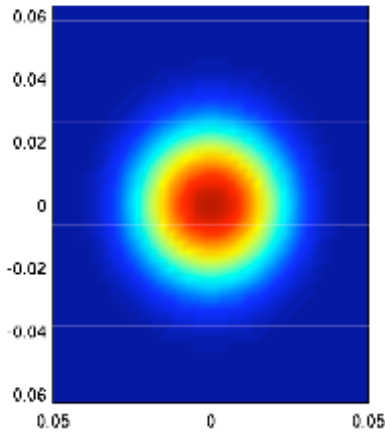
GO.



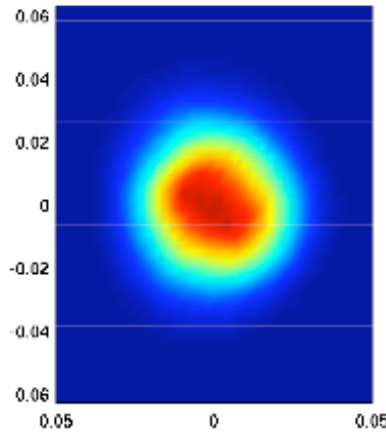
Dark Port beam profile by FFT

- ideal vs reality-prime -

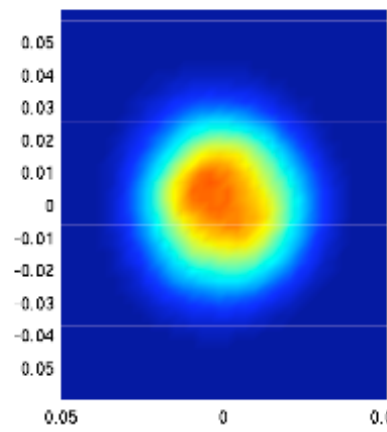
upper SB



No phase map
Symmetric heating

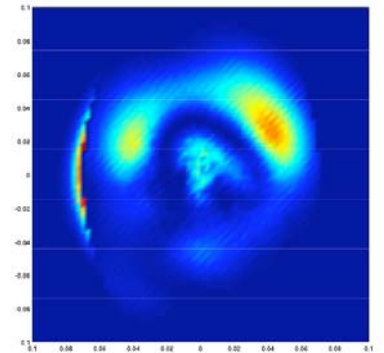


With phase map
Symmetric heating



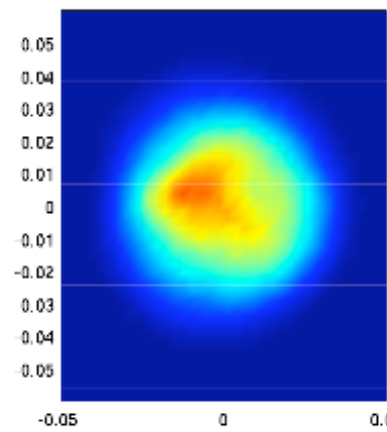
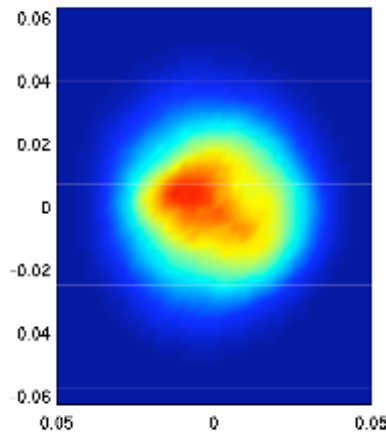
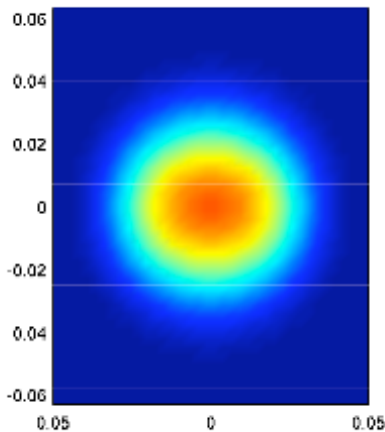
With phase map
Differential heating

and CR



200k BS
curvature

lower SB



G040514