# Improving Advanced LIGO sensitivity using a local readout scheme

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# **Dynamics of Single Cavity**

Equations of motion of suspended mirror



# Monitoring End-Mirror Displacement



Radiation pressure induced position fluctuations of the ETM caused by the main cavity field are measured by a reference cavity.

#### Detection strategy:

- -Output b<sup>out</sup> can be feed back to ETM
- Optimal noise spectral density can by computed form outputs a<sup>out</sup> and b<sup>out</sup>

Heidmann et. al. [quant-ph/0311167]

# **Detuned Cavity**

Detuning the cavity by  $\phi$  modifies equation of motion:



# **Detuned SR Interferometer**

- <u>Remember:</u> Detuned SR Interferometer is equivalent to single detuned cavity
- Detuning is moved to signal recycling cavity
- Additional resonances:
  - optical resonance
  - optomechanical resonance
- Gain of sensitivity at the two resonances
- Loss of sensitivity below optomechanical resonance frequency





# Signal and Noise Transfer



Mainly the rigid optical spring suppresses the response of the interferometer's differential mode to GW waves  $\rightarrow$  cf. optical bar

[Braginski, Gorodetsky & Khalili 1997; Braginski & Khalili 1999; Khalili 2002] motion x

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motion x

# Signal and Noise Transfer



Radiation pressure noise of SR interferometer is also suppressed by the optical spring

Further suppression of radiation pressure noise by a local meter is not necessary for detuned SR interferometers! But...



# Local Readout Scheme (1)

- Reading out the ITMs' motion by injection of second laser beam
- Additional laser beam should not resonate in arm cavities
- At frequencies below optomechanical resonance the local meter views bar formed by rigidly connected ITM and ETM
- Effective mass sensed by local meter is twice that of ITM or ETM (assuming equal masses)
- Recover low-frequency response
  of detuned SR interferometer
- Extension to stand-alone optical bar or SR schemes





# Local Readout Scheme (2)

| Symbol                        | Physical meaning                              | Value                    |  |
|-------------------------------|---|--------------------------|--|
| m                             | Single mirror mass                            | 40 kg                    |  |
| m <sub>BS</sub>               | BS mass                                       | 40 kg                    |  |
| ω <sub>0</sub> <sup>(1)</sup> | Light frequency 1 <sup>st</sup> laser         | 1.8x10 <sup>15</sup> 1/s |  |
| P <sup>(1)</sup>              | Circulating power 1st carrier                 | 100-800 kW               |  |
| L <sup>(1)</sup>              | Large scale ifo arm length                    | 4 km                     |  |
| $\rho_{PR}$                   | PRM reflectivity                              | (0.5) <sup>1/2</sup>     |  |
| ф                             | Detuning for 1 <sup>st</sup> carrier          | 0-π                      |  |
| ρ <sub>SR</sub>               | SRM reflectivity                              | (0.93) <sup>1/2</sup>    |  |
| γ <sub>0</sub>                | Cavity half bandwidth 1st carrier             | 2π 15 Hz                 |  |
| ζ(1)                          | Det. angle for 1 <sup>st</sup> carrier        | 0-π                      |  |
| ω <sub>0</sub> <sup>(2)</sup> | Light frequency 2 <sup>nd</sup> laser         | 1.8x10 <sup>15</sup> 1/s |  |
| P <sup>(2)</sup>              | Circulating power 2nd carrier                 | 0-16 kW                  |  |
| L <sup>(2)</sup>              | Local meter arm length                        | 15 m                     |  |
| λ <sup>(2)</sup>              | Detuning for 2 <sup>nd</sup> carrier          | 0 Hz                     |  |
| ٤ <sup>(2)</sup>              | Cavity half bandwidth 2 <sup>nd</sup> carrier | 2 π 4 kHz                |  |
| ζ(2)                          | Det. angle for 2 <sup>nd</sup> carrier        | 0                        |  |



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# **Combined Sensitivity**

The output can be written in the compact form

$$\hat{y}^{(1)} = \vec{n}_1^T \ \vec{\nu} + s_1 \ h \text{ and } \hat{y}^{(2)} = \vec{n}_2^T \ \vec{\nu} + s_2 \ h$$

and the combined output is given by

$$\hat{y} = K_1(\Omega) \; \hat{y}^{(1)} + K_2(\Omega) \; \hat{y}^{(2)}$$

with filter functions  $K_1(\Omega)$  and  $K_2(\Omega)$ . The resulting total noise spectral density

$$S_{h}(\Omega) = \frac{\begin{pmatrix} K_{1}(\Omega) & K_{2}(\Omega) \end{pmatrix} \begin{pmatrix} \vec{n}_{1}^{T}\vec{n}_{1}^{*} & \vec{n}_{1}^{T}\vec{n}_{2}^{*} \\ \vec{n}_{2}^{T}\vec{n}_{1}^{*} & \vec{n}_{2}^{T}\vec{n}_{2}^{*} \end{pmatrix} \begin{pmatrix} K_{1}^{*}(\Omega) \\ K_{2}^{*}(\Omega) \end{pmatrix}}{\begin{pmatrix} K_{1}(\Omega) & K_{2}(\Omega) \end{pmatrix} \begin{pmatrix} s_{1}s_{1}^{*} & s_{1}s_{2}^{*} \\ s_{2}s_{1}^{*} & s_{2}s_{2}^{*} \end{pmatrix} \begin{pmatrix} K_{1}^{*}(\Omega) \\ K_{2}^{*}(\Omega) \end{pmatrix}}$$

has to be minimized.

 $\vec{\nu}^T = (a_1^{(1)}, a_2^{(1)}, a_1^{(2)}, a_2^{(2)}, \hat{\xi}_{\text{ITM}}^{\text{cl}}, \hat{\xi}_{\text{ETM}}^{\text{cl}}, \hat{\xi}_{\text{BS}}^{\text{cl}})$ 

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# **Filter Functions**

- Optimal filter functions

   minimize noise spectral density
  - are close to step functions
- Signal transfer function of large scale interferometer below optomechanical resonance decreases rapidly but...
- ...signal transfer of local meter stays constant

Combination of locally sensed optical bar scheme and SR interferometer



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## **Noise Spectral Density**



-0

# Astrophysical Optimization

- Optimization with respect to binary systems with total mass M and reduced mass  $\mu$
- Observable distance for a given SNR  $\rho_0$  and averaged binary orientation has to be maximized:

$$D = \sqrt{\frac{2}{15}} \frac{G^{5/6} \mu^{1/2} M^{1/3}}{\pi^{2/3} c^{3/2} \rho_0} \sqrt{\int_{f_{\min}}^{f_{\max}} \mathrm{d}f} \ \frac{f^{-7/6}}{S_h(f)}$$

- Classical noise cutoff:  $f_{min} \sim 7 \text{ Hz}$
- Upper cutoff given by GW frequency at last stable circular orbit of the binary:  $f_{max}^{\sim}$  4400Hz (M / M)

# **Comparison of Event Rates**



### Noise Spectral Densities with Classical Noise

| M/M | opt. parameter with local meter |         |                        | opt. parameter without local meter |         |                     |         |
|-----|---------------------------------|---------|------------------------|------------------------------------|---------|---------------------|---------|
|     | P <sup>(1)</sup> [kW]           | φ [rad] | ζ <sup>(1)</sup> [rad] | P <sup>(1)</sup> [kW]              | φ [rad] | $\zeta^{(1)}$ [rad] | improv. |
| 2.8 | 800                             | 0.48 π  | 0.7 π                  | 800                                | 0.48 π  | 0.49 π              | 29%     |
| 20  | 450                             | 0.47 π  | 0.58 π                 | 500                                | 0.48 π  | 0.48 π              | 28%     |
| 40  | 150                             | 0.45 π  | 0.43 π                 | 150                                | 0.45 π  | 0.46 π              | 33%     |
| 120 | 100                             | 0.46 π  | 0.32 π                 | 100                                | 0.47 π  | 0.41 π              | 42%     |



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# Conclusion and Outlook

- Locally reading out ITMs' motion by second laser beam improves sensitivity significantly
- Maintaining or improving sensitivity of Advanced LIGO even for reduced power in arm cavities



- Combinable with other QND schemes, e.g. injection
  of squeezed vacuum
- Our proposed upgrade for Advanced LIGO should be realizable with low effort



BS motion is

- only important in the local meter
- negligible for the large scale interferometer due to arm cavities
- also driven by bright port laser input fields
   [Harms et. al. 2002]



#### **Classical noise**

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- modeled by operators ξ<sup>cl</sup><sub>i</sub>, i 5 {ITM,ETM,BS}
- contributions are uncorrelated
- each mirror is subject to fourth of the spectrum generally expected for whole differential mode



# Implementation

- RF sidebands (1% of carrier light) already probe ITM in planed Advanced LIGO
- For our scheme a second laser beam is needed with the same power as the first laser (125 W).
- Polarized light or different frequencies can be used
- Frequency of second laser must be chosen such that it does not resonate in the arm cavities
- Circumvent shot-noise-limited sensitivity of large scale interferometer since sensitivity in the detection band cannot be lower than shot-noise level of local measurement of the ITMs in the control bandwidth



# **Control Filter**

- Instability induced by optical spring requires feedback control
- In general local meter and large scale interferometer could be detuned and therefore show instabilities
- It can be shown that an appropriate control feedback leaves noise spectral density unchanged

