

Low temperature dissipation in coating materials

S. Reid¹, I. Martin¹, H. Armandula³, R. Bassiri¹, E. Chalkley¹, C. Comtet⁴, M.M. Fejer⁵, A. Gretarsson⁶, G. Harry⁷, J. Hough¹, P. Lu⁵, I. McLaren¹, J-M.M. Mackowski⁴, N. Morgado⁴, R. Nawrodt², S. Penn⁸, A. Remillieux⁴, S. Rowan¹, R. Route⁵, A. Schroeter², C. Schwarz², P. Seidel², K. Vijayraghavan⁵, W. Vodel², A. Woodcraft¹

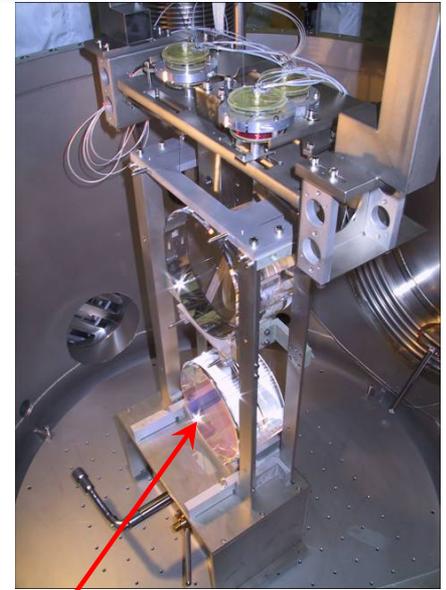
¹SUPA, University of Glasgow, Scotland. ²Friedrich-Schiller University, Jena, Germany. ³LIGO Laboratory, California Institute of Technology, USA. ⁴LMA, Lyon, France. ⁵Stanford University, USA. ⁶Embry-Riddle Aeronautical University, USA. ⁷LIGO Laboratory, Massachusetts Institute of Technology, USA. ⁸Hobart and William Smith Colleges, USA.

Overview

- Introduction and experimental details
- Measurements of the low temperature dissipation peak in Ta_2O_5 coatings
 - Possible dissipation mechanism in ion beam sputtered Ta_2O_5
 - Effect of TiO_2 doping on the loss in Ta_2O_5 coatings
 - Effect of annealing on the loss in Ta_2O_5 coatings
- Comparison of dissipation in Ta_2O_5 and SiO_2 films as a function of temperature
- Magnetron sputtered SiO_2 results from Jena University (slides courtesy of Ronny Nawrodt)
- Preliminary results of Hafnia.

Introduction

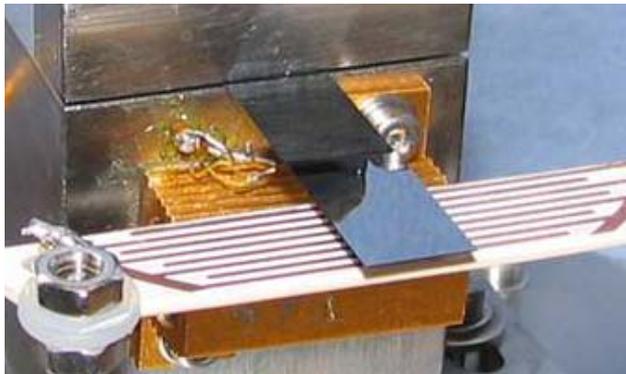
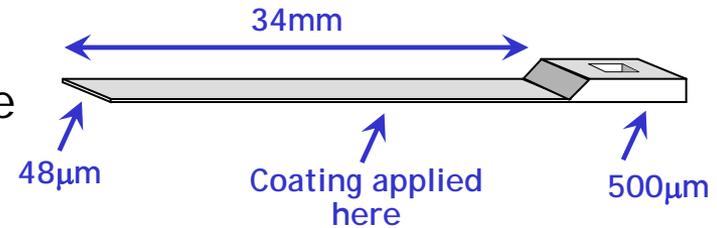
- **Mechanical dissipation** from dielectric mirror coatings is predicted to be a significant source of **thermal noise** for advanced detectors.
- Experiments suggest
 - Ta_2O_5 is the dominant source of dissipation in current $\text{SiO}_2/\text{Ta}_2\text{O}_5$ coatings
 - **Doping** the Ta_2O_5 with TiO_2 can reduce the mechanical dissipation
- Mechanism responsible for the observed mechanical loss in Ta_2O_5 as yet not clearly identified
- Studying dissipation as a function of temperature of interest to:
 - Determine dissipation mechanisms in the coatings, possibly allowing dissipation to be reduced
 - Evaluate coating for possible use in proposed cryogenic gravitational wave detectors



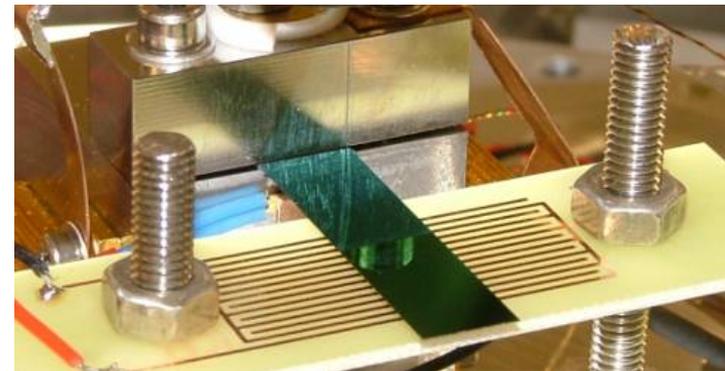
GEO600 mirror suspension, with HR coating on front face.

Single layer coating samples for low temperature studies

- Thin silicon substrates used for coating
 - Loss of silicon decreases at low temperature
 - Coating will dominate the loss



uncoated silicon cantilever in clamp

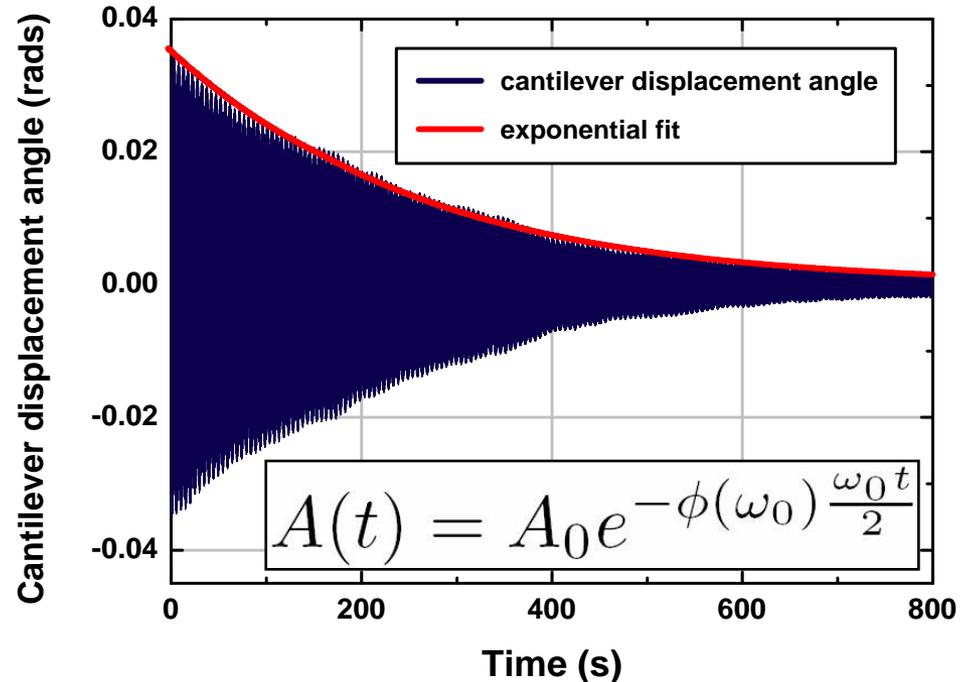


Titania doped tantalum coated silicon cantilever in clamp

- Samples etched from silicon wafers, with thicker clamping block to isolate cantilever from clamp
- 0.5 µm thick films deposited by ion beam sputtering, including (a) Ta₂O₅ doped with (14.5 ± 1)% TiO₂ (b) un-doped Ta₂O₅ (c) SiO₂ and (d) hafnia

Measuring coating loss

- **Bending modes** of cantilever excited electrostatically, loss $\phi(\omega)$ obtained from exponential amplitude ringdown
- Loss of coating material calculated from losses of **coated** and **un-coated** cantilevers
- Loss of coating material is given by:



Typical amplitude of ring-down

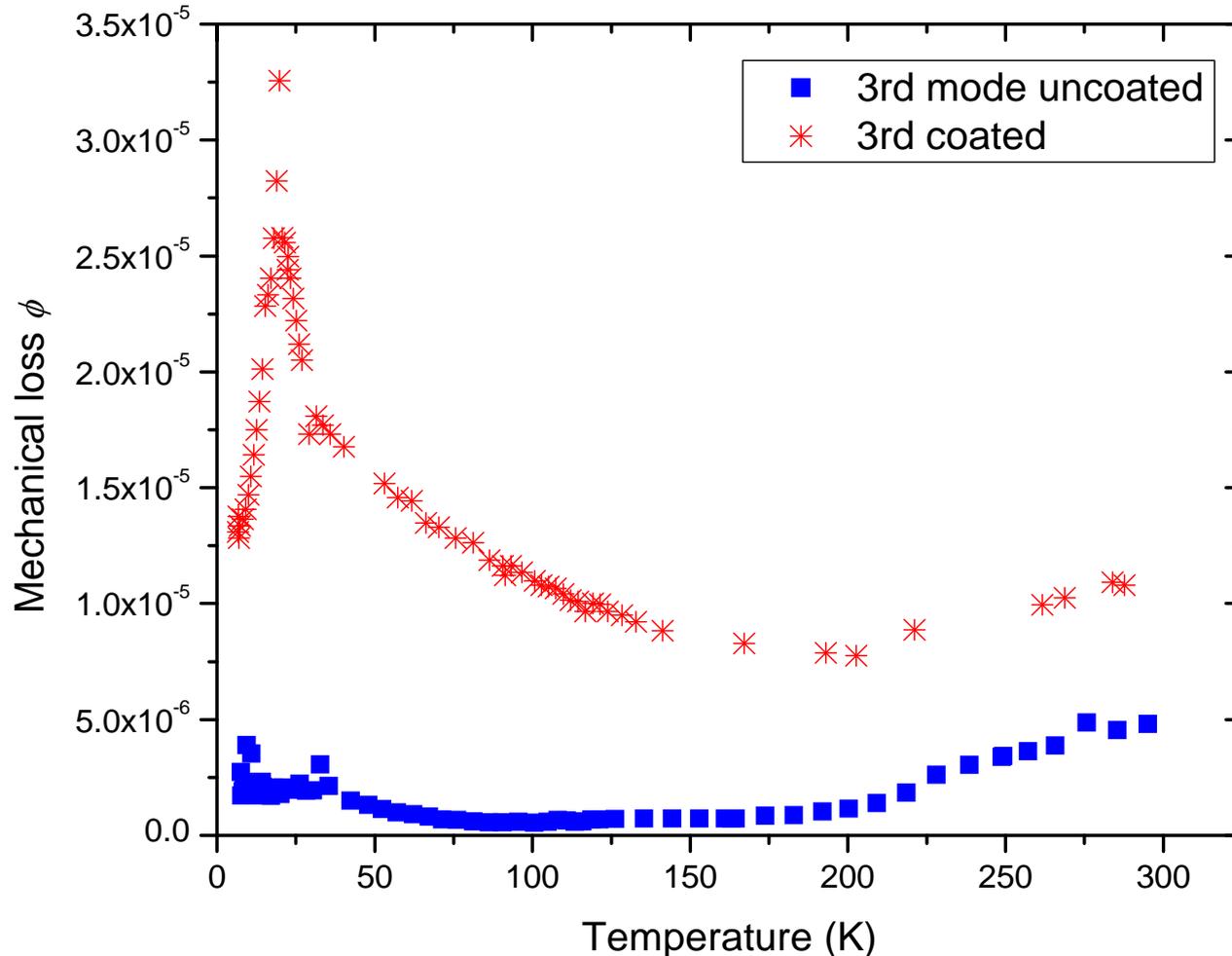
$$\phi_{\text{coating}} = \frac{E_{\text{coated-sample}}}{E_{\text{coating}}} (\phi_{\text{coated sample}} - \phi_{\text{uncoated sample}})$$

ratio of energy stored in cantilever to energy stored in coating

difference in loss between coated and un-coated cantilevers

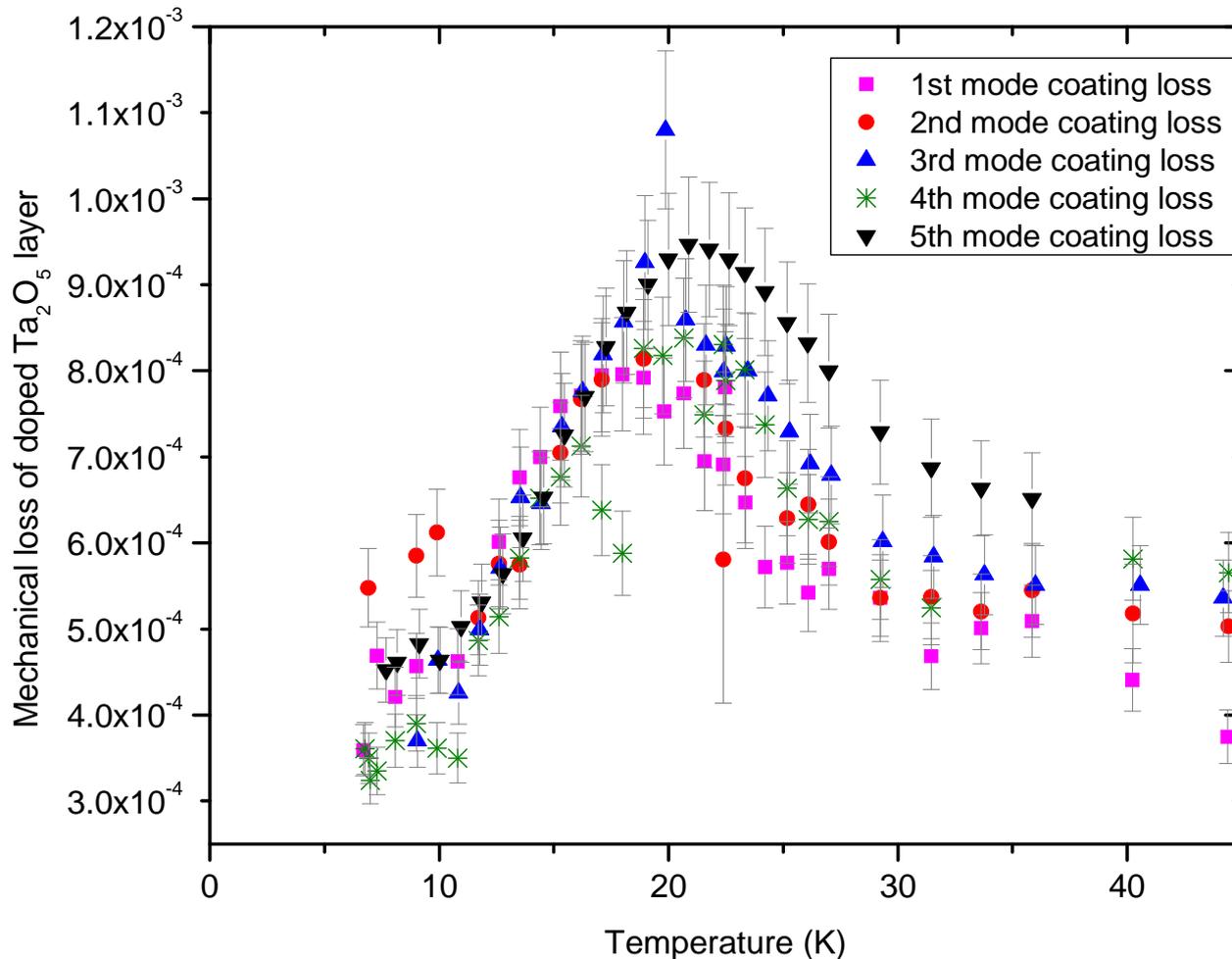
Mechanical loss measurements

- Comparison of the mechanical loss of the third bending mode (~1000 Hz) for a cantilever coated with Ta₂O₅ with 14.5 % TiO₂, and an identical uncoated cantilever (in collaboration with Jena University)



Low temperature coating loss peak

- A **dissipation peak** at ~18-20 K observed in both TiO₂-doped Ta₂O₅ (see figure) and pure Ta₂O₅



Interpretation and analysis

- Most internal friction mechanisms may be thought of as relaxation processes associated with transitions between equilibrium states, and typically:

$$\phi(\omega) = \Delta \frac{\omega\tau}{1 + (\omega\tau)^2} \quad \text{where } \tau \text{ is the relaxation time}$$

Δ is a constant related to height of peak

- Thermally activated processes follow Arrhenius equation:

$$\tau^{-1} = \tau_0^{-1} e^{-\frac{E_a}{K_B T}}$$

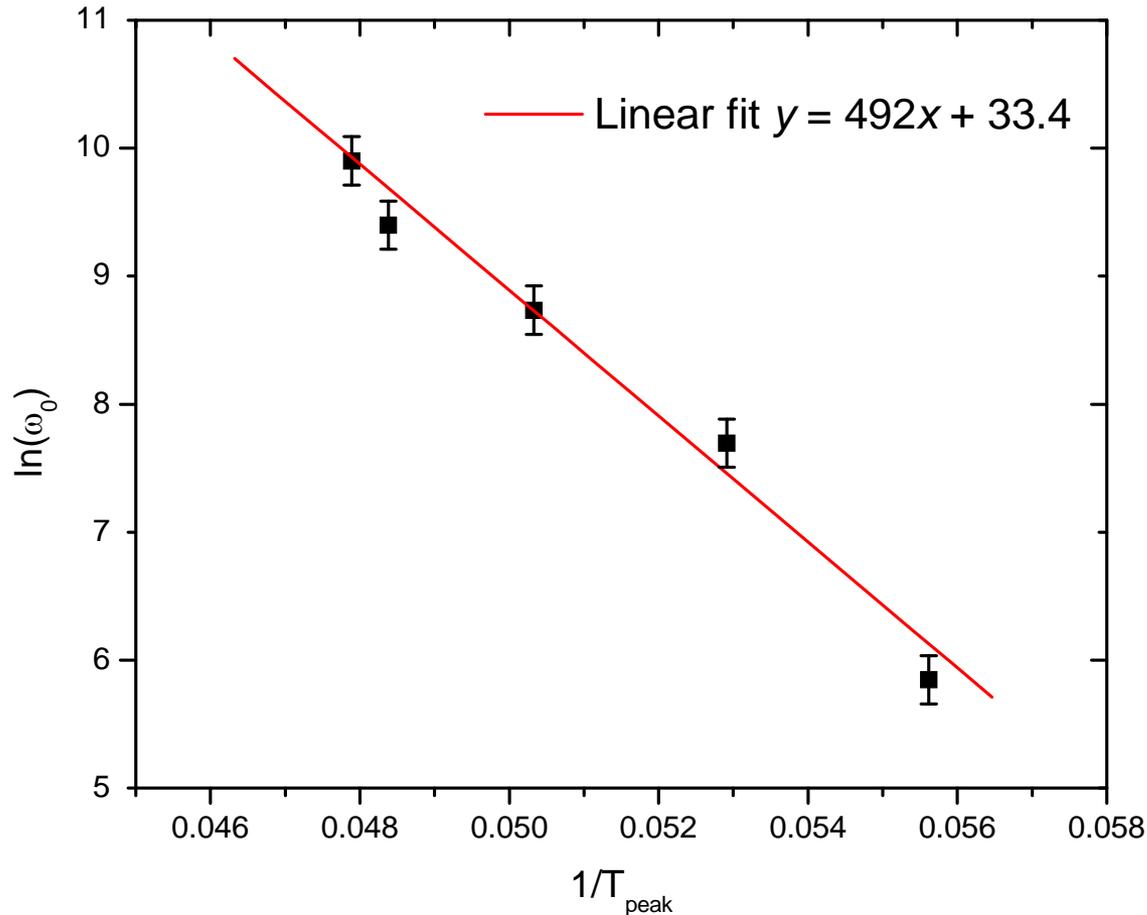
where τ_0^{-1} is the rate factor and E_a is the **activation energy** for the process

- At the dissipation peak, $\omega\tau = 1$ and $\omega = \tau_0^{-1} e^{-\frac{E_a}{K_B T_{peak}}}$

hence

$$\ln \omega = \ln \tau_0^{-1} - \frac{E_a}{K_B T_{peak}}$$

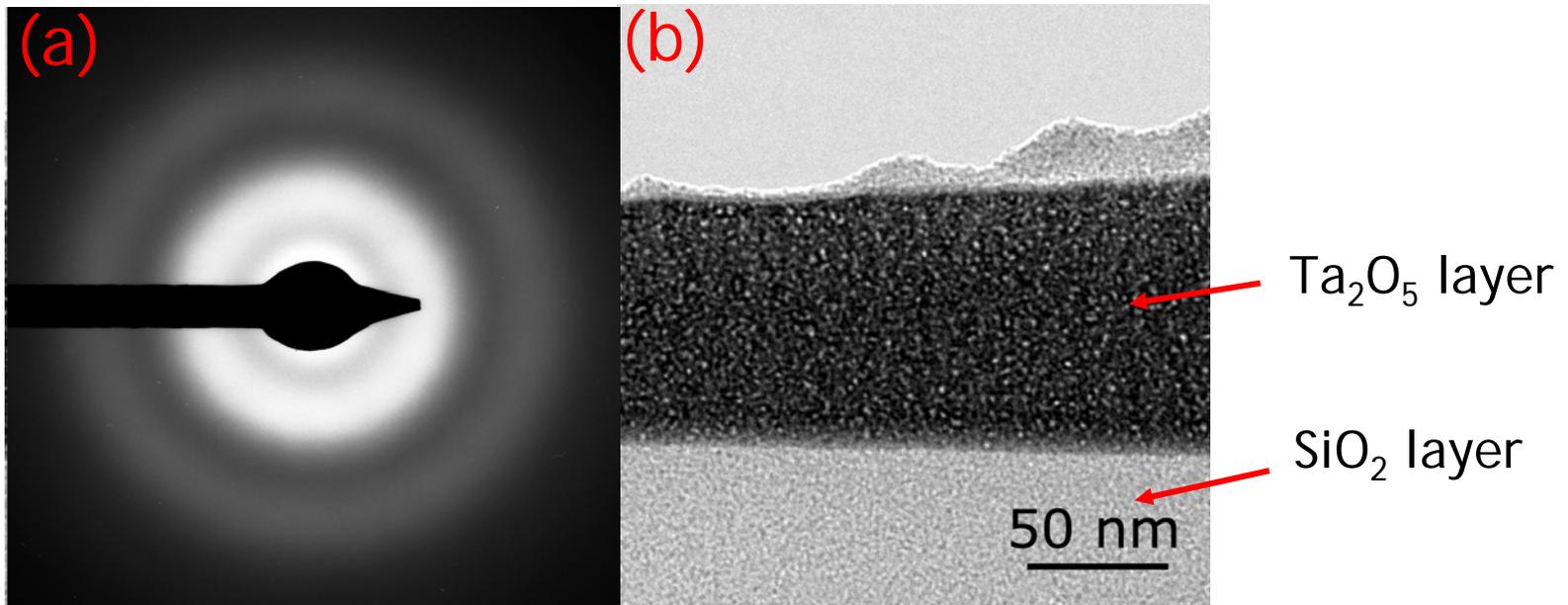
Fitting to Arrhenius equation



- This gives an **activation energy** associated with the dissipation peak in doped tantala of (42 ± 2) meV, and a rate factor of 3.3×10^{14} Hz.

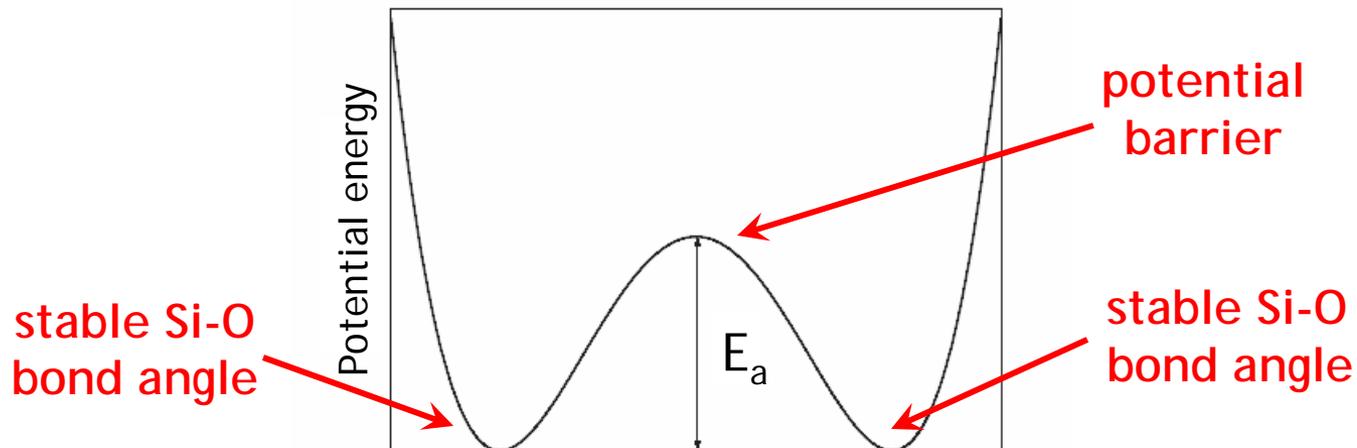
Coating Structure

- Convergent beam **electron diffraction** measurements (a) of a pure ion-beam sputtered Ta_2O_5 layer (see TEM image, (b)) shown only diffuse rings of intensity, confirming that the layer is **amorphous**.

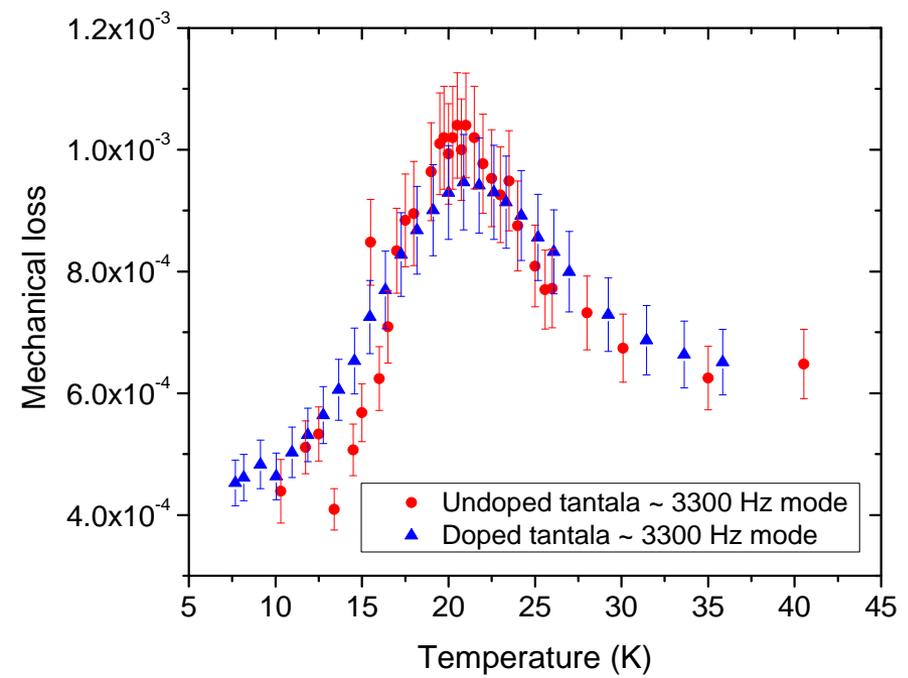
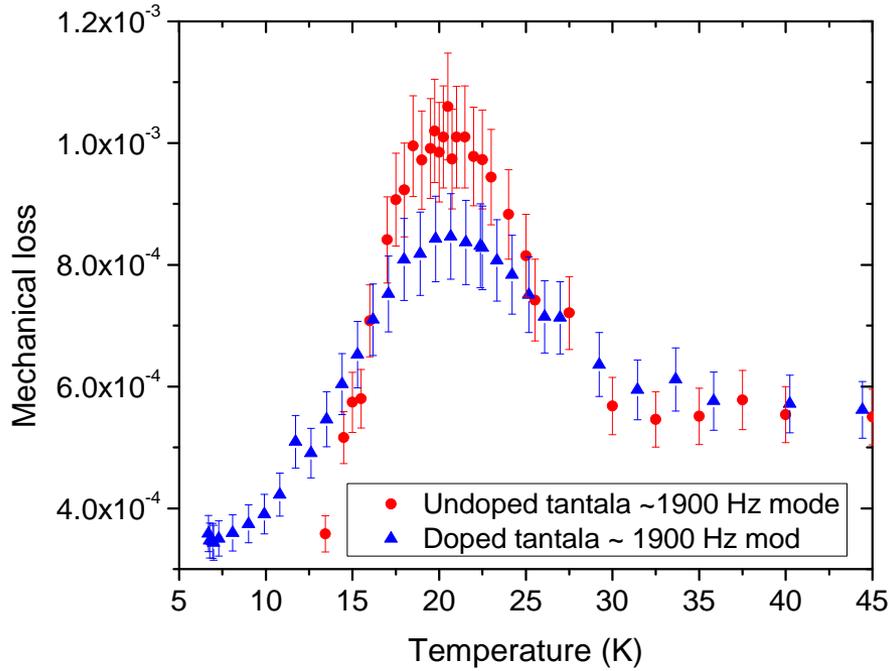


Interpretation - double well potential

- Low temperature dissipation peak in **fused silica** has similar activation energy (44 meV)
 - Oxygen atoms can undergo thermally activated transitions between two possible energy states in a double well potential
 - Width of the dissipation peak thought to be related to the distribution of Si-O bond angles in the sample
 - The dissipation mechanism in doped Ta_2O_5 may be similar, but requires further study



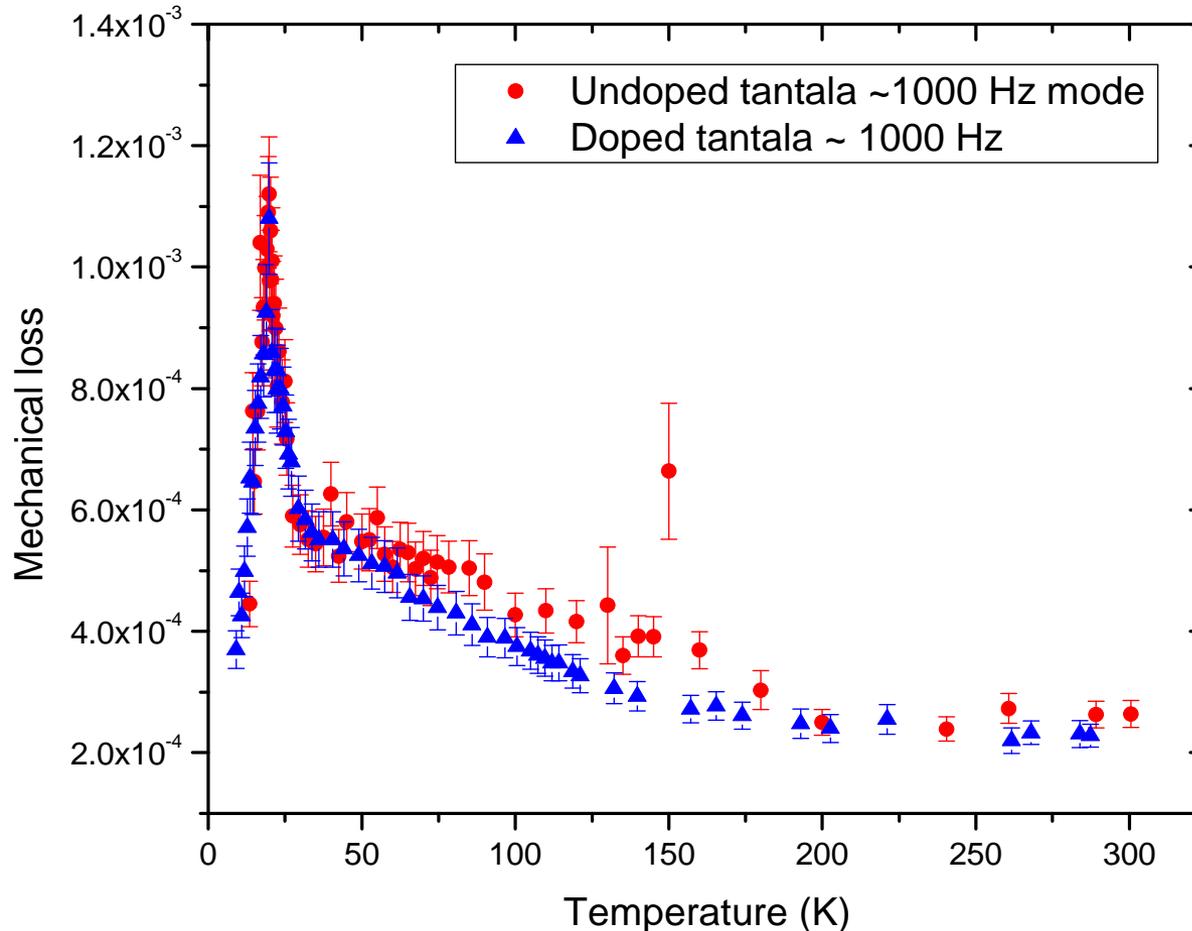
Effect of doping Ta_2O_5 with 14.5 % TiO_2



Comparison of dissipation peak in **doped** and **un-doped** Ta_2O_5 for 4th (left) and 5th bending modes (right).

- Doping appears to reduce the height of the peak and slightly reduce the width of the peak

Effect of doping Ta_2O_5 with 14.5 % TiO_2



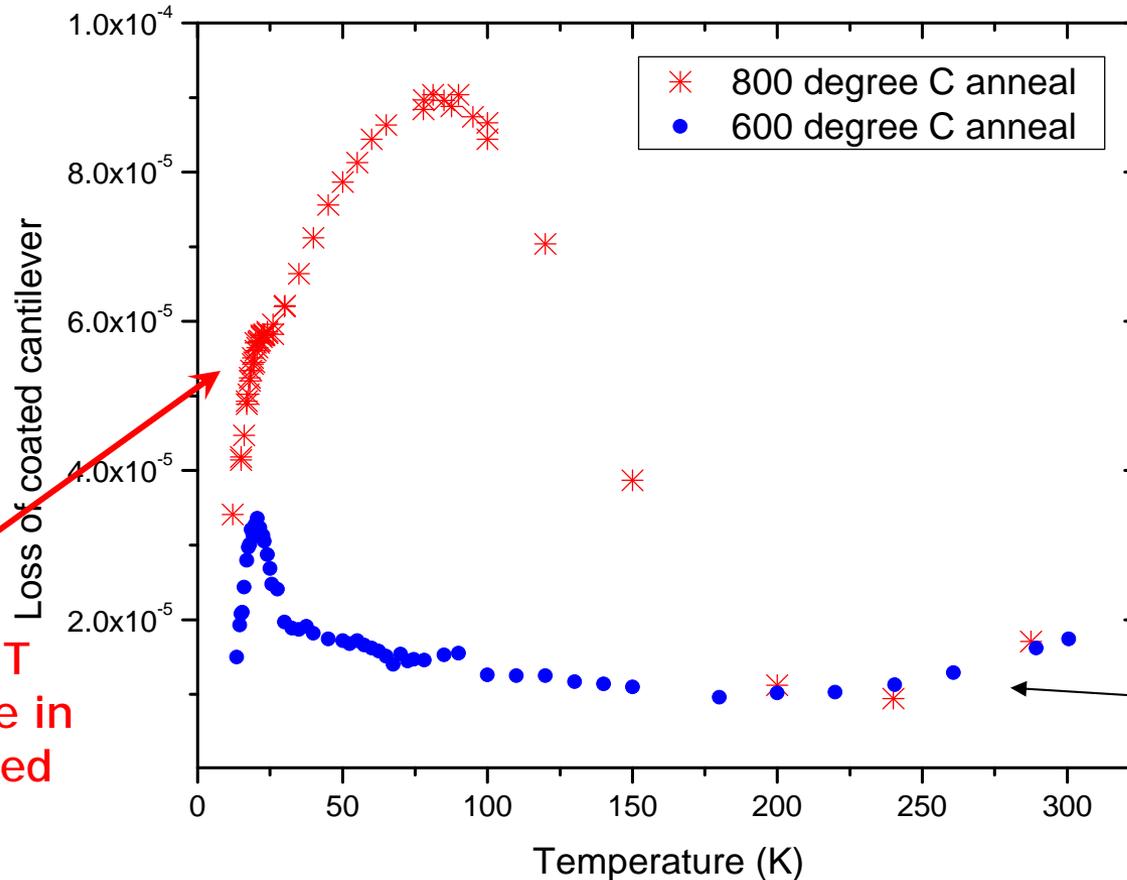
Comparison of the dissipation of TiO_2 -doped and un-doped Ta_2O_5

- Doping reduces loss of Ta_2O_5 throughout temperature range

Effect of annealing

- **Heat treatment** can reduce the dissipation in SiO_2 possibly by changing distribution of bond angles
 - If dissipation mechanism in Ta_2O_5 is indeed similar to SiO_2 it may be possible to modify characteristics of the dissipation peak by heat treatment
 - Ta_2O_5 known to **crystallise** above $\sim 650^\circ\text{C}$
- Experiment currently underway to measure un-doped Ta_2O_5 coatings annealed at 300, 400, 600 and 800°C
- Initial results for 800°C anneal

Effect of annealing temperature



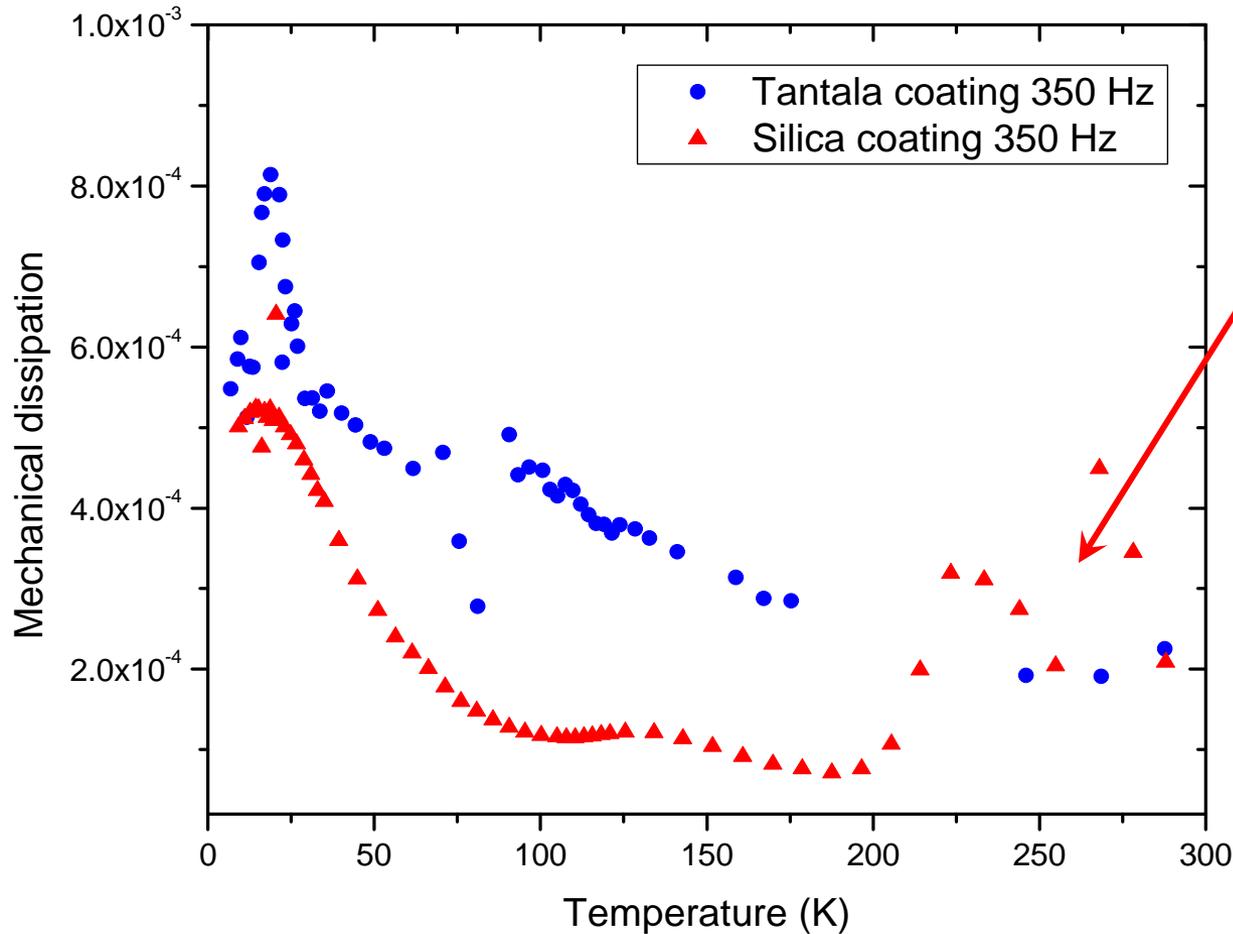
effect of low T peak still visible in sample annealed to 800 °C

Losses similar close to room temperature

Loss at 1900 Hz of Ta₂O₅ annealed at 800 °C and 600 °C

- Large peak at ~ 80 to 90 K in coating annealed at 800 °C, perhaps due to onset of polycrystalline structure?

Comparison of SiO_2 and Ta_2O_5



scatter at higher temperatures possibly due to loss into clamp.

Recent data suggests SiO_2 loss of $\sim 4 \times 10^{-5}$ at room temperature.

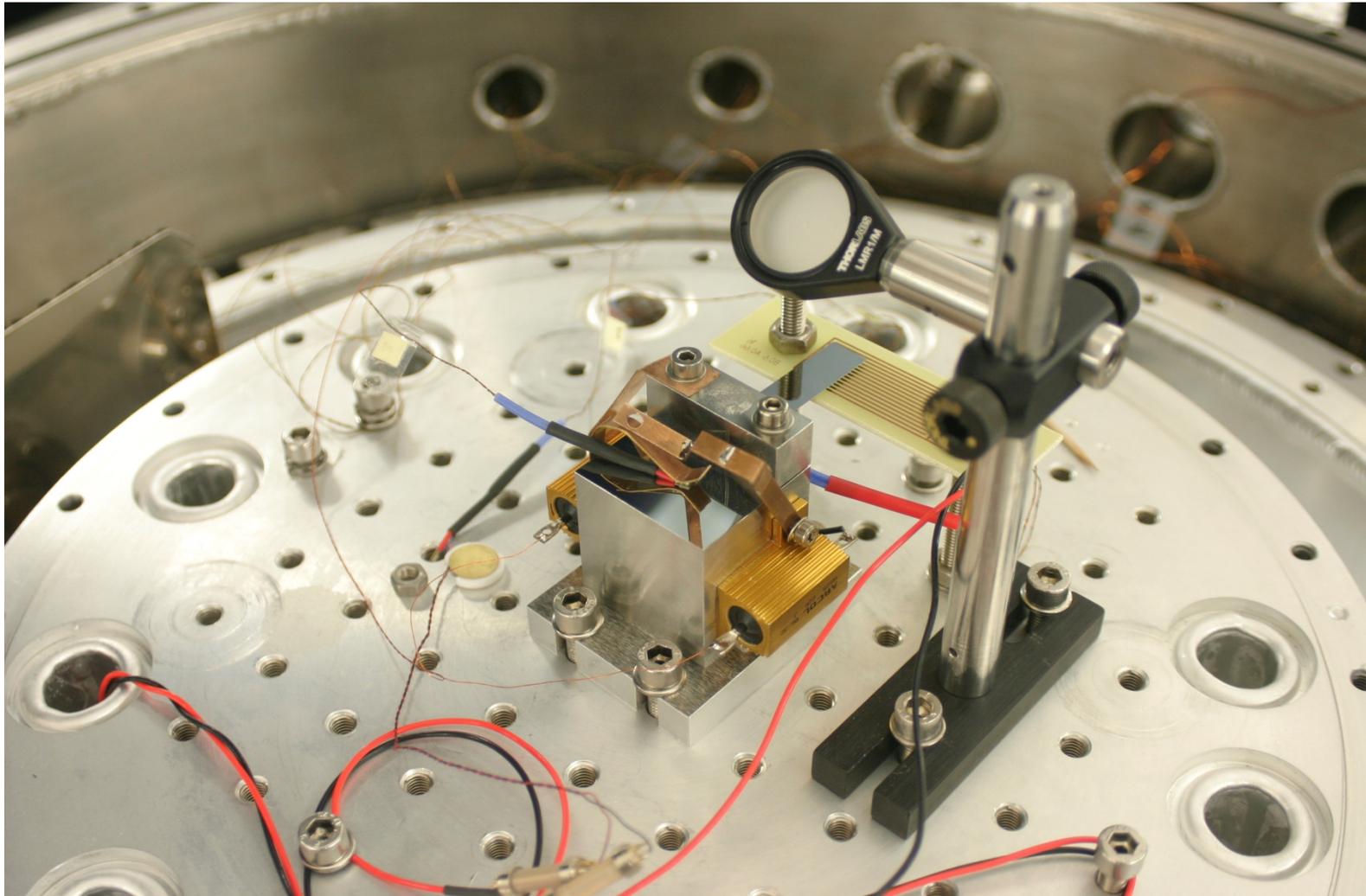
- Loss of ion beam sputtered SiO_2 is significantly lower than loss of Ta_2O_5 between 10 and 300 K.

Conclusions - Ta₂O₅

- Dissipation peak observed at ~ 20 K in both pure Ta₂O₅ and in Ta₂O₅ doped with 14.5 % TiO₂
- **Activation energy** of dissipation process calculated to be 42 ± 2 meV (for doped coating). Possible dissipation mechanism is thermally activated transitions of the oxygen atoms, similar to that in fused silica
- Some evidence that **TiO₂ doping reduces the height** of the dissipation peak in Ta₂O₅, in addition to reducing the loss at room temperature.
- Ta₂O₅ coatings annealed at 800 °C display a **large dissipation peak at ~90 K.**
- A full understanding of the dissipation mechanism may allow
 - Mechanical loss at room temperature to be further reduced
 - Reduction of loss at particular temperatures of interest for future cryogenic detectors
- Ta₂O₅ has higher loss than SiO₂ between 10 and 300 K

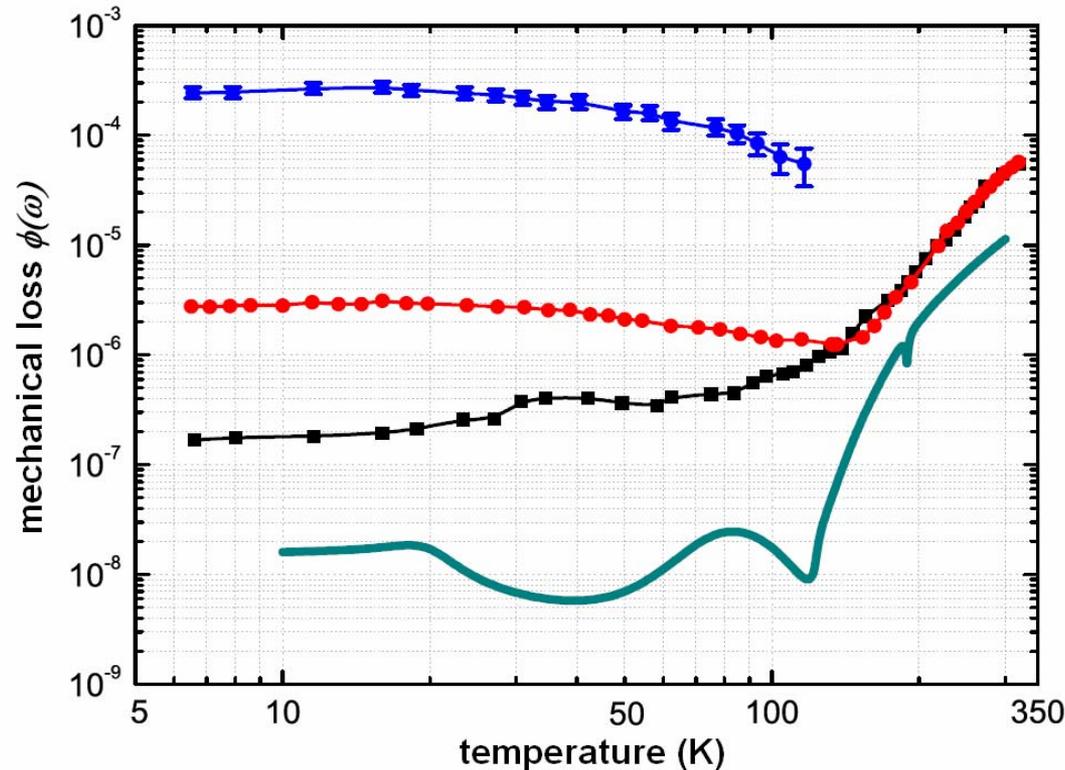


Magnetron Sputtered Silica (400 nm) - Jena





Magnetron Sputtered Silica (400 nm) - Jena



- coating loss
- coated cantilever
- uncoated cantilever
- thermoelastic + residual gas loss

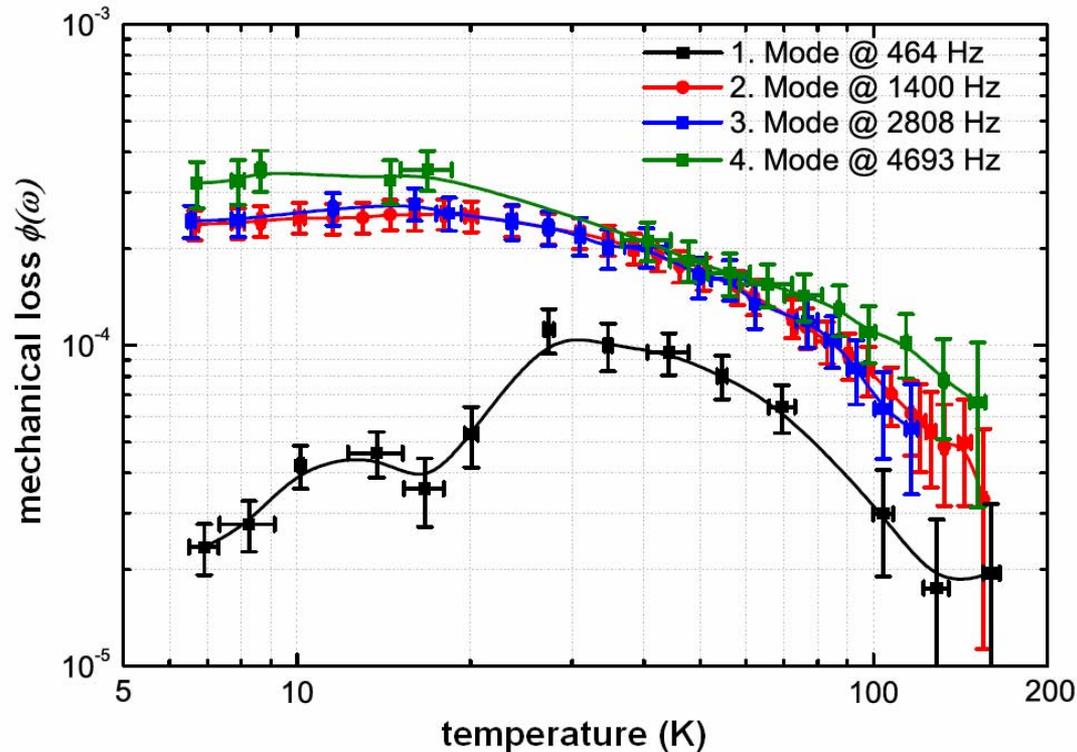
frequency: 2.8 kHz

geometry: 50 mm × 8 mm × 70 μm

- Comparable level of observed loss associated with the magnetron sputtered silica coating at ~100 K to ion-beam sputtered silica.
- However, below 100 K no dissipation peak observed in magnetron sputtered silica



Magnetron Sputtered Silica (400 nm) - Jena



- 464 Hz mode - resonance with clamping structure
- Loss increases for all modes at low temperatures

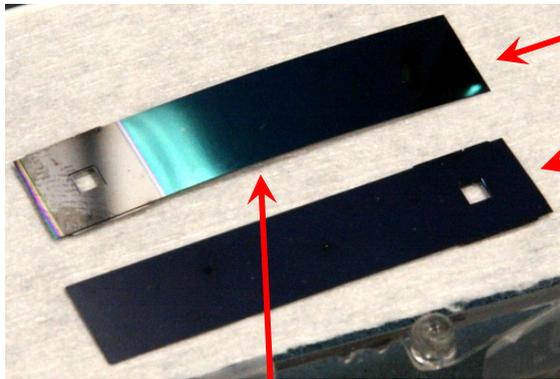
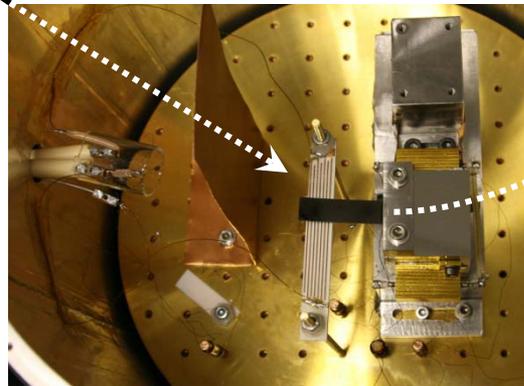
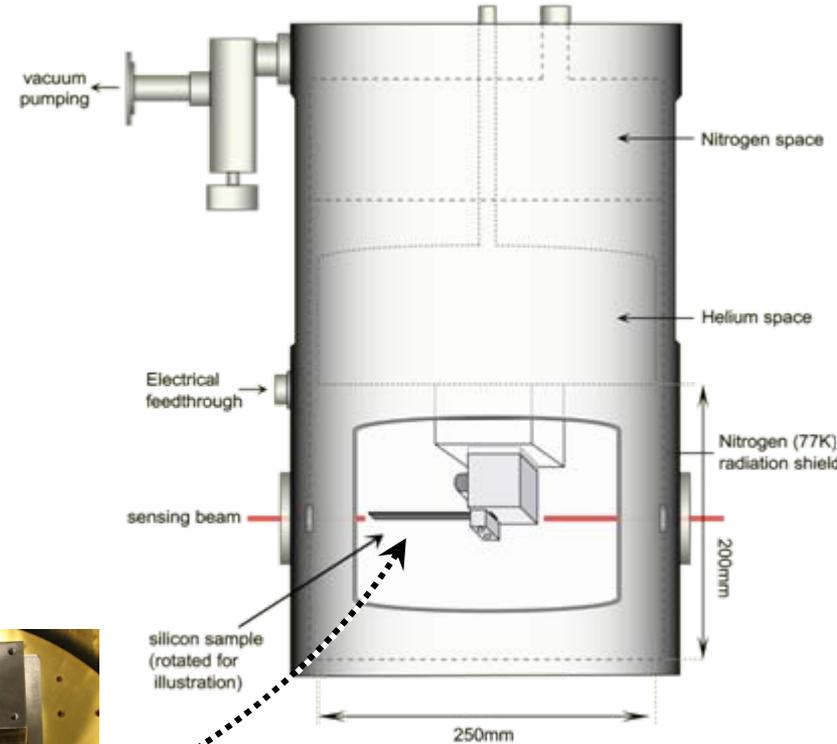
Preliminary studies on HfO₂

- New cryogenic setup in Glasgow:

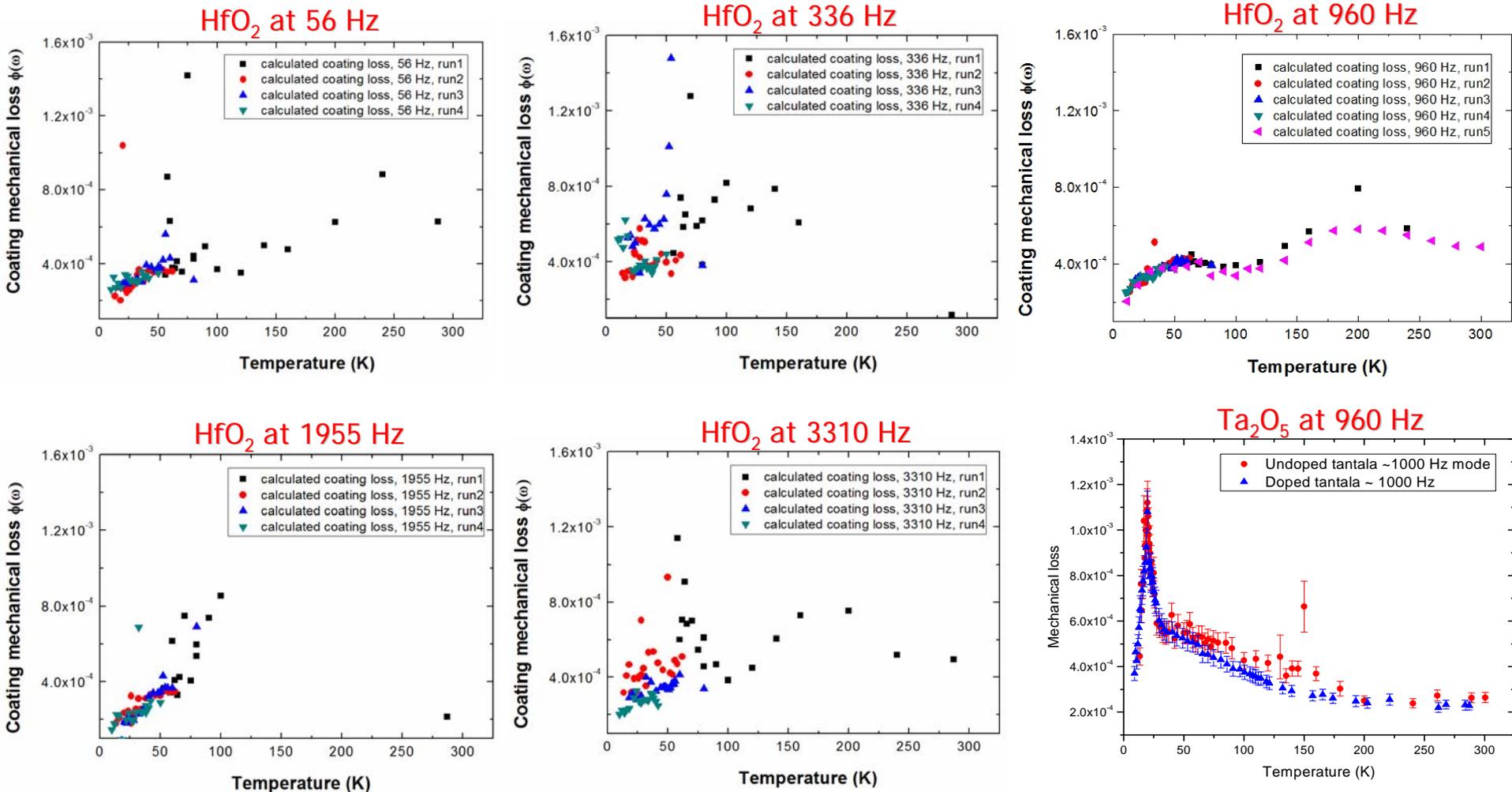
500nm HfO₂ coating on a silicon cantilever

uncoated silicon cantilever

thermal stresses in coating clearly observed in the bending of the silicon substrate

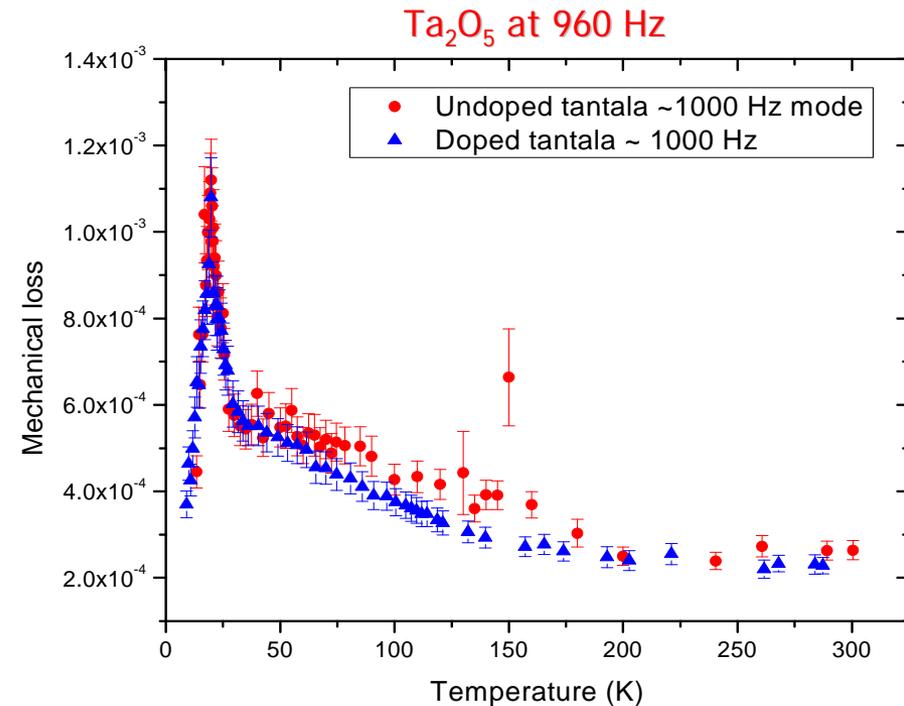
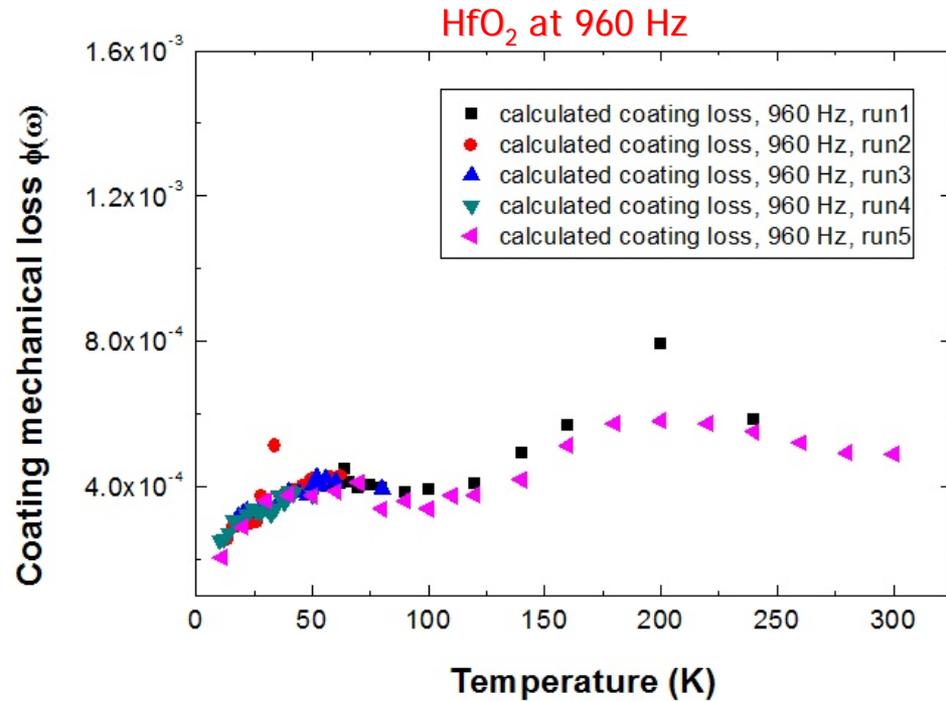


Preliminary studies on HfO_2 and compared to Ta_2O_5



- Observed scatter in initial mechanical losses suggest energy coupling to clamp resonances for several of the resonant modes studied.

Preliminary HfO₂ compared to Ta₂O₅



- At 100 K, the level of mechanical loss associated with both doped tantalum and hafnia appear at a level $\phi(\omega)_{\text{coating}} \sim 4 \times 10^{-4}$.
- Below 100 K, the loss of tantalum is observed to rise to a dissipation peak, whereas the loss of hafnia appears to decrease to below 3×10^{-4} at ~ 15 K.

Preliminary HfO_2 compared to Ta_2O_5

- Preliminary results of the mechanical loss of Hafnia does not show a large dissipation peak at low T.
- Note: the higher Young's modulus of Hafnia should lead to lower thermal noise for the same $\phi \cdot d$ (loss-thickness product) - in the case of silicon optics (not true for other materials *e.g.* fused silica).
- Initial room temperature studies on a multi-layer silica-hafnia coating on a fused silica substrate were found to be $\phi_{\text{hafnia}} = (5.7 \pm 0.3) \times 10^{-4}$.
- However **material properties** for thin-film Hafnia are **not well studied** and any changes over bulk properties will change the results presented here.
- The optical properties also require further investigation, where initial recent absorption studies of a multilayer silica-hafnia coating by Markosyan et al. (Stanford University) lie in the range 60-80ppm, which is considerably higher than required.