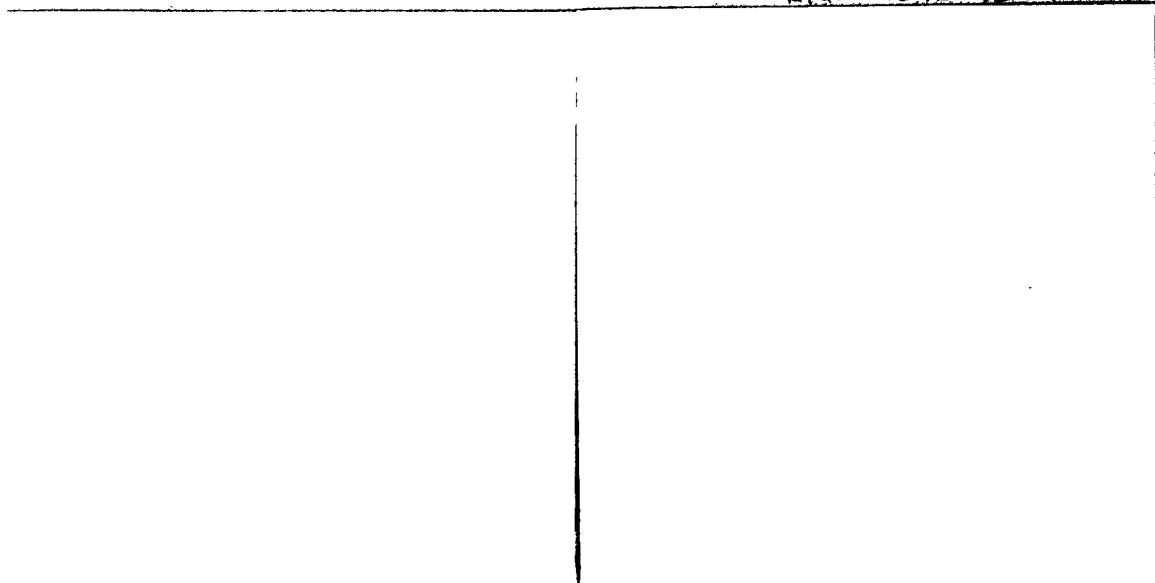


# Optical Absorption Characterization Using Thermal Waves

**Zhouling Wu**

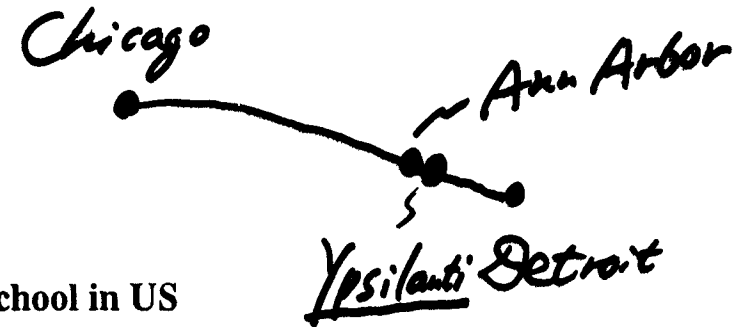
**Experimental Laser Physics Laboratory  
Department of Physics and Astronomy  
Eastern Michigan University, Ypsilanti, MI 48197**

LIGO-G970016-00-R



# Eastern Michigan University

- **Where?** Ypsilanti, Michigan  
neighbor of University of Michigan
- **When?** Founded in 1849  
as one of the first teacher training school in US
- **What?** #1 producer of school teachers in US  
about 25000 students (80% undergraduates)
- **Responsibility:** Educate future educator



## Responsible for future!

# New Challenges

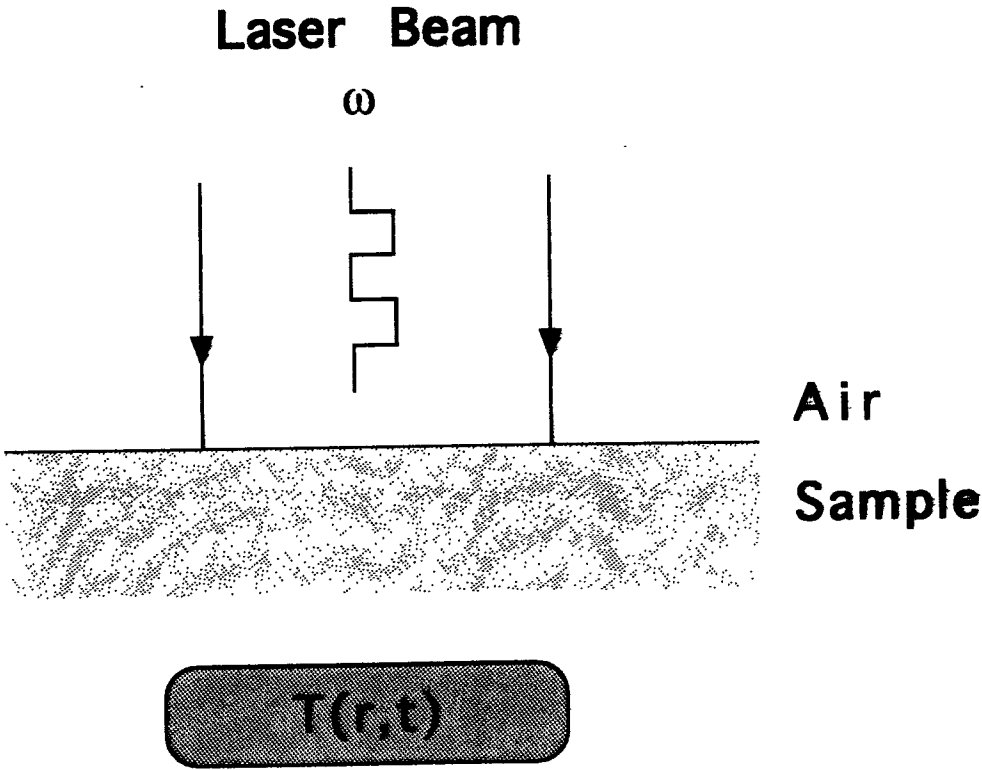
<b>Ultra-low level:</b>	sub-ppm (e.g. LIGO) <b>⇒ High sensitivity</b> ~ a few ppb
<b>Contamination:</b>	manufacturing application characterization <b>⇒ Non-contact</b> <b>Non-invasive</b> <b>In-situ</b>
<b>Nonuniformity:</b>	lateral (e.g. defects) vertical (e.g. interface) <b>⇒ Spatial resolution</b>
<b>Instability:</b>	<b>In-situ</b>
<b>Nonlinearity:</b>	<b>Power dependence</b>

Low Cost / Fast / Portable

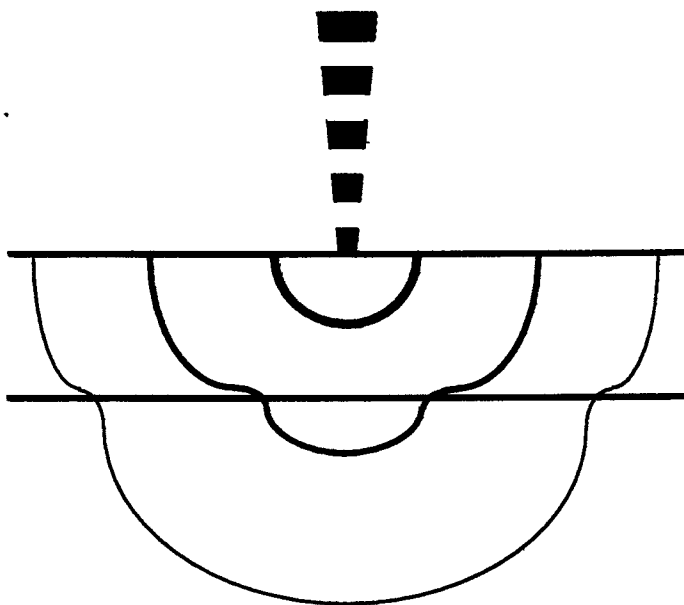
*easy to use*

*Large Aperture !*

# What is a Thermal Wave?

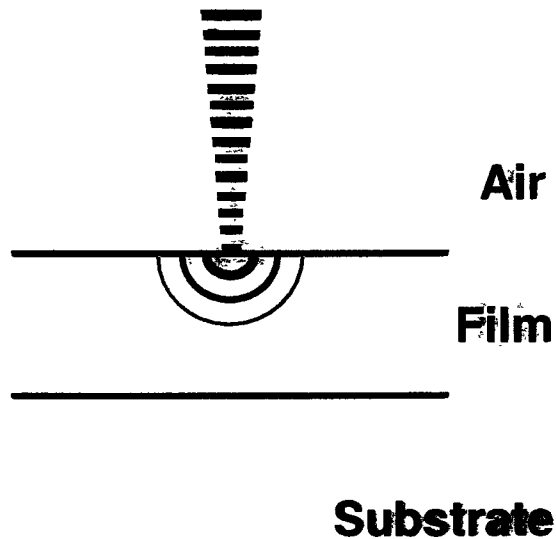


**Laser Beam**



**Long Wavelength  
(Low  $\omega$ )**

**Laser Beam**



**Short Wavelength  
(High  $\omega$ )**

**Heat diffusion Equation:**

$$\nabla^2 T = \frac{1}{\alpha} \frac{\Delta T}{\Delta t}$$

$\alpha$ : thermal diffusivity       $\alpha = \frac{\kappa}{\rho c}$   
 $\kappa$ : thermal conductivity  
 $\rho$ : mass density  
 $c$ : specific heat

**Solution in one dimension ----> Plane wave**

$$T(x,t) = T_0 e^{i(qx - \omega t)}$$

**Where the thermal wave number,  $q$ , is given by**

$$q = (1 + i) (\omega / 2 \alpha)^{1/2}$$

Real part ----> Physical temperature rise:

$$T(x, t) = T_0 e^{-x/\mu} \cos\left(\frac{2\pi x}{\lambda} - \omega t\right)$$

Diffusing length:  $\mu = (2\alpha / \omega)^{1/2}$

Wavelength:  $\lambda = 2\pi\mu$

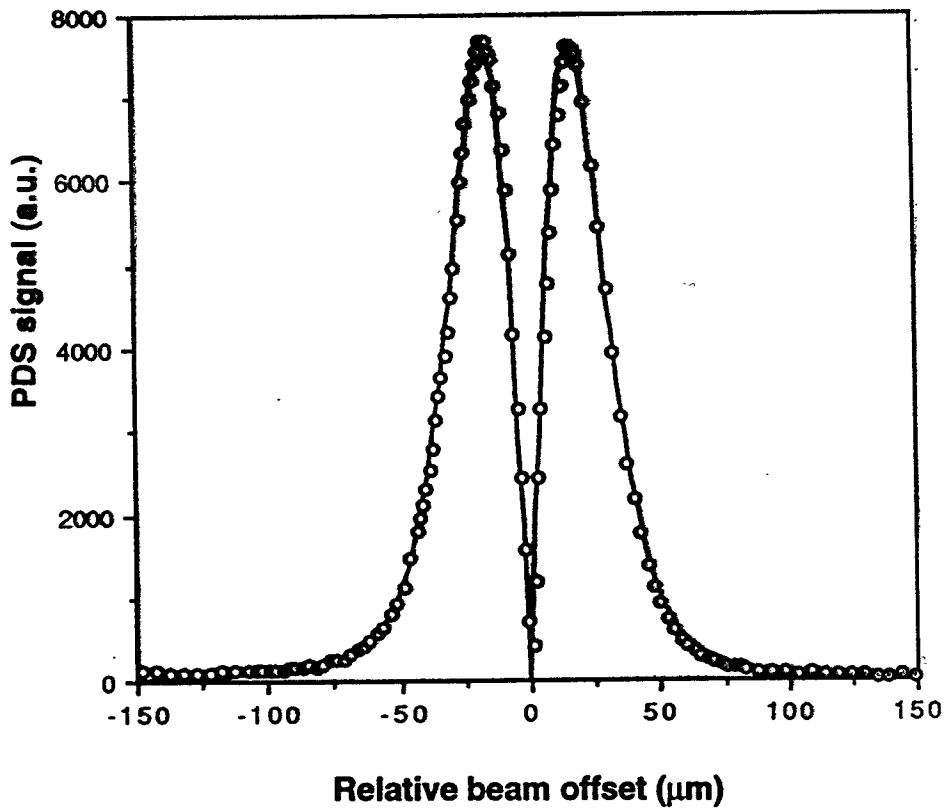
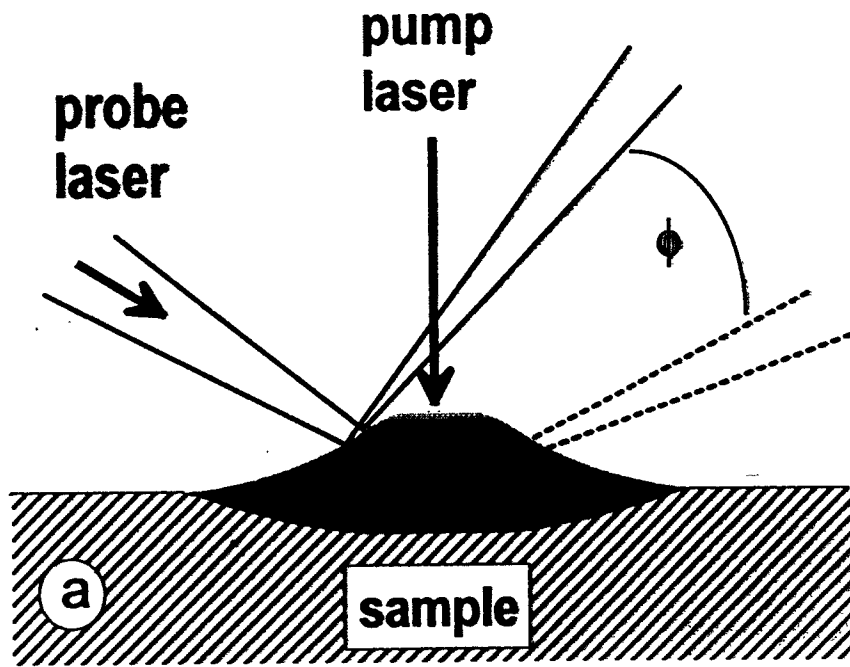
Wave velocity:  $v = \frac{\omega\lambda}{2\pi} = (2\alpha\omega)^{1/2}$

Heavily damped

Very dispersive

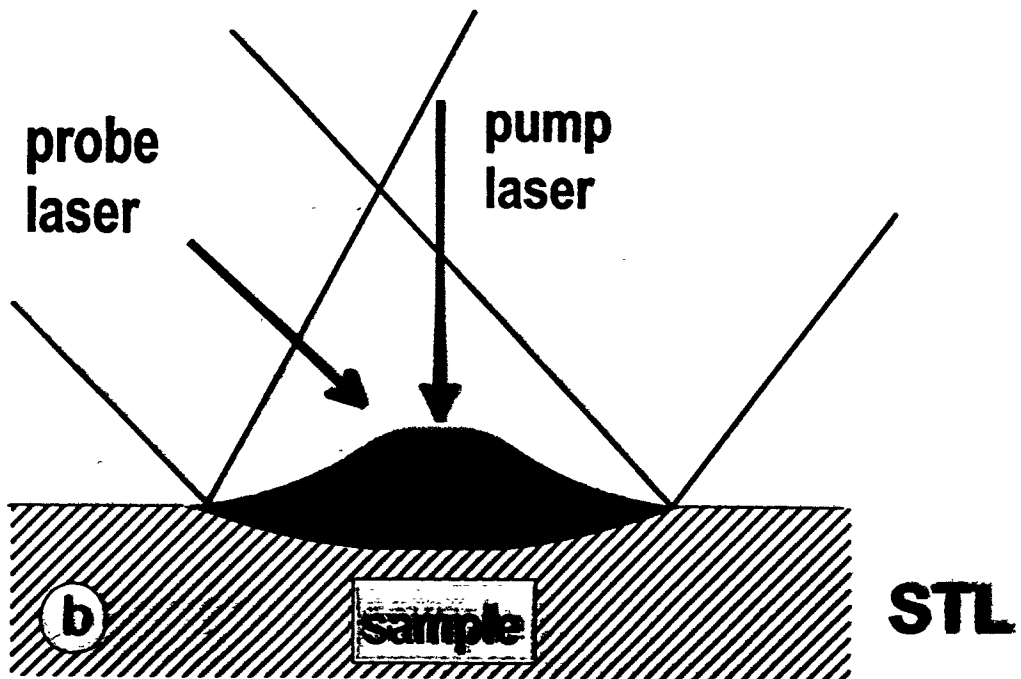
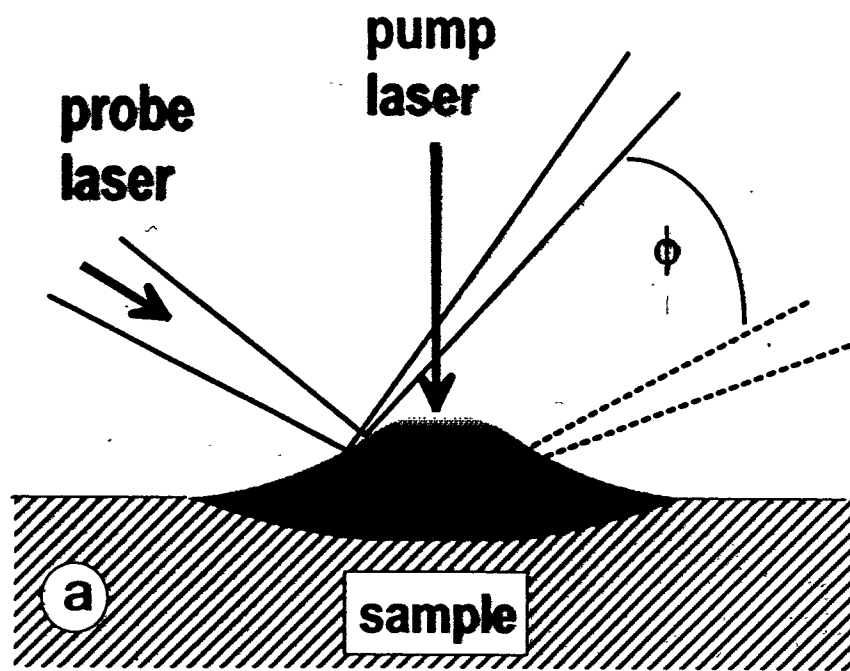
Earliest reference: Ångstrom, Ann. Physik, 114 (1861)

# Detection of photothermal deformation using photothermal deflection spectroscopy (PDS)

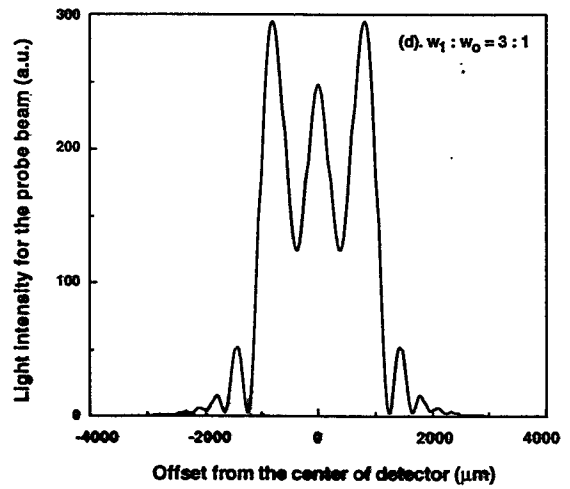
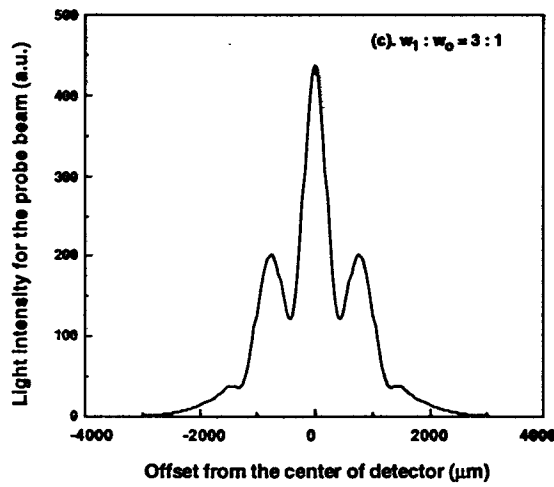
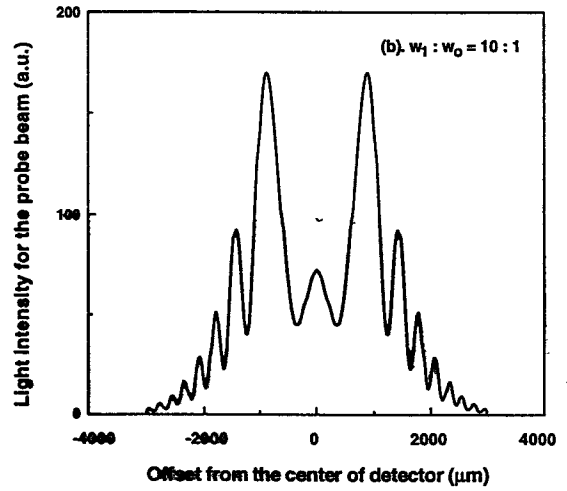
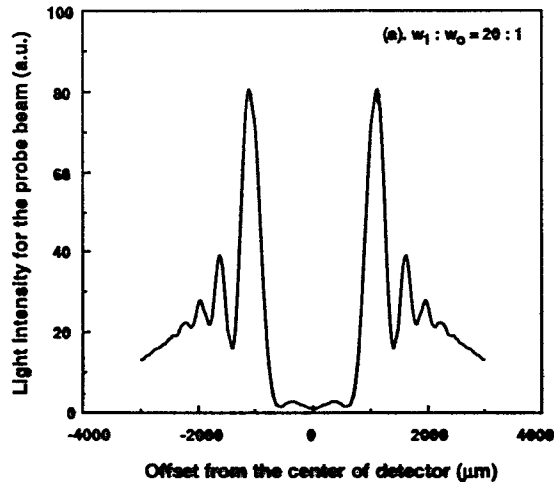




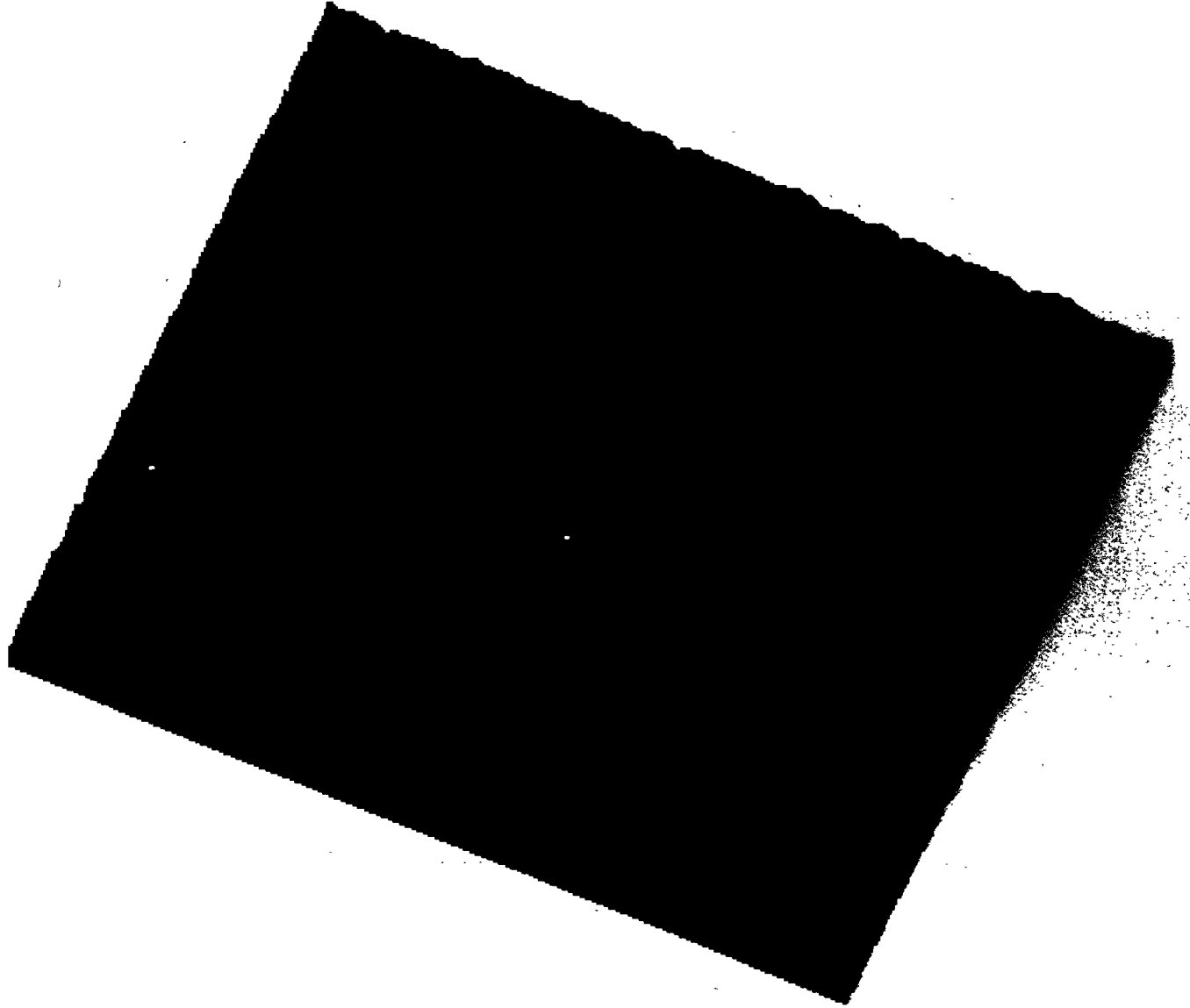
# Comparison between PDS and Surface Thermal Lensing (STL)



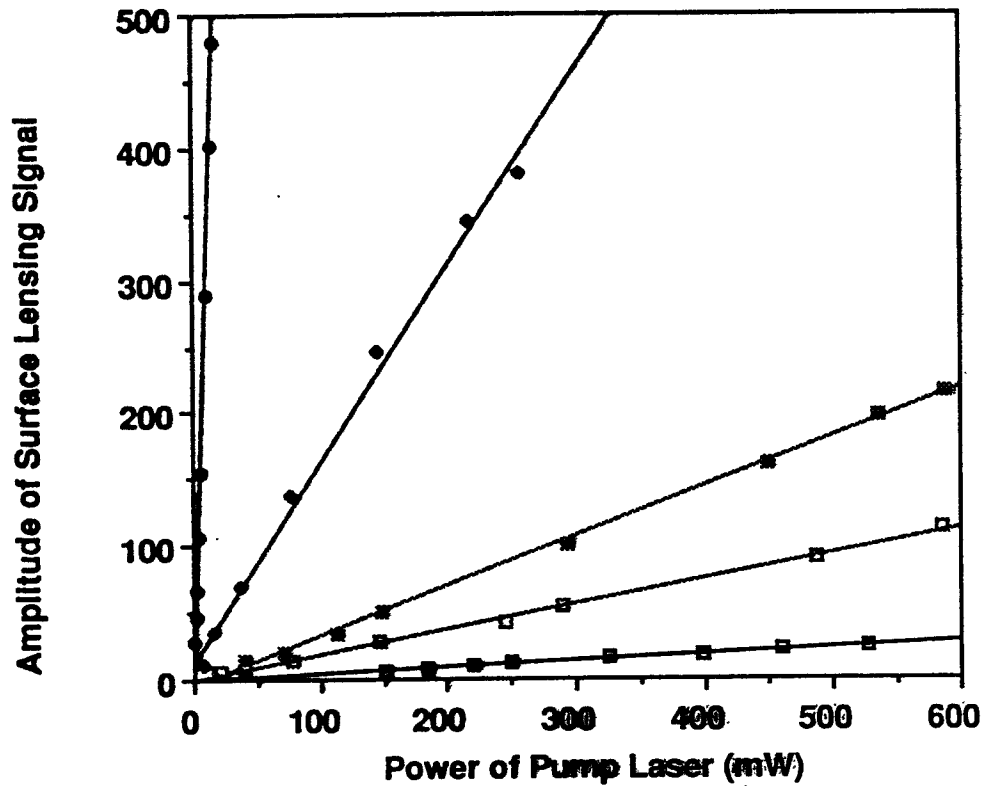
# Modeled Results of the Diffraction Pattern of the Probe Laser Beam in the Detection Plane



# Probe beam profile in the observation plane



## Absorption Measurement Results Using Surface Lensing Effect



**Sample**

**Fitting result**

**Absorption**

● Ag film on BK7

$y = 1.3005 + 28.401x$   $R^2 = 0.999$

$1.52 \times 10^{-2}$

◆ TiO2 on BK7

$y = 11.582 + 1.4880x$   $R^2 = 0.995$

$7.86 \times 10^{-4}$

■ Ta2O5 on BK7

$y = -4.4776 + 0.37251x$   $R^2 = 0.999$

$1.99 \times 10^{-4}$

□ ZrO2 on BK7

$y = 0.69165 + 0.18633x$   $R^2 = 0.998$

$9.97 \times 10^{-5}$

■ SiO2 on BK7

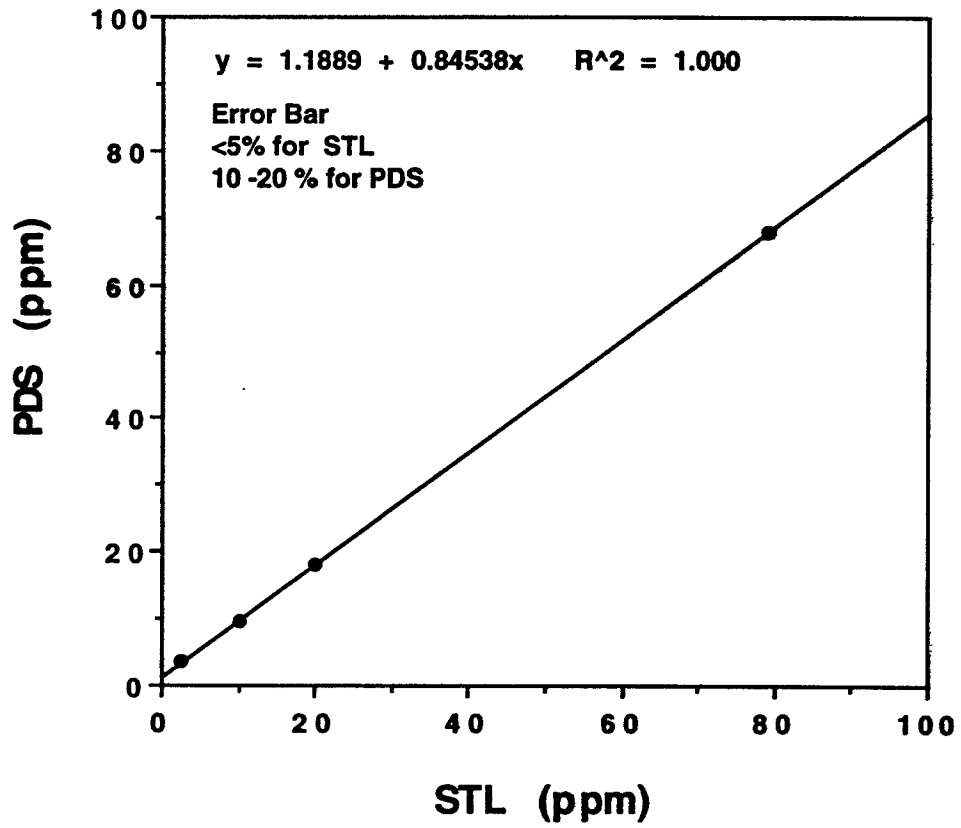
$y = -0.76352 + 4.9054e-2x$   $R^2 = 1.000$

$2.63 \times 10^{-5}$

**Absorption measured by using STL and their comparison with those by our in-house PDS**

<b>Sample</b>	<b>SiO<sub>2</sub></b>	<b>ZrO<sub>2</sub></b>	<b>Ta<sub>2</sub>O<sub>5</sub></b>	<b>TiO<sub>2</sub></b>	<b>Accuracy</b>
<b>STL</b>	<b>2.6 ppm</b>	<b>10 ppm</b>	<b>20 ppm</b>	<b>79 ppm</b>	<b>&lt; 5.0 %</b>
<b>PDS</b>	<b>3.5 ppm</b>	<b>9.6 ppm</b>	<b>18 ppm</b>	<b>68 ppm</b>	<b>~ 10 - 20 %</b>

**Correlations: STL vs PDS**



#### 4.2 *In-situ* studies of optical absorption

Many thin films are not stable under laser irradiation [9,10, 23, 24]. Even for stable optical components, its performance may still be a function of time due to possible contamination process. STL, thanks to its time resolution (typically a few ms), presents itself as a powerful tool for monitoring in real time the dynamics of the change, as shown by the example in Figure 7. In this example, the sample is under  $\text{Ar}^+$  laser irradiation when the absorption data is taken. In about ten minutes, the absorption of the sample was reduced by a factor of about seven.

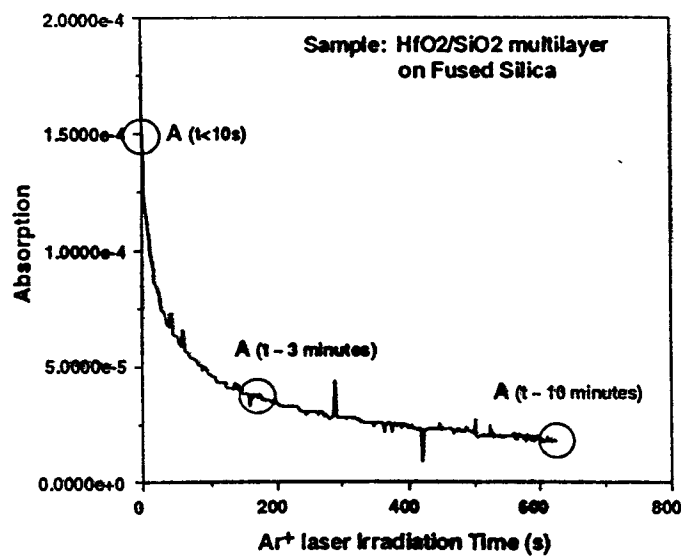
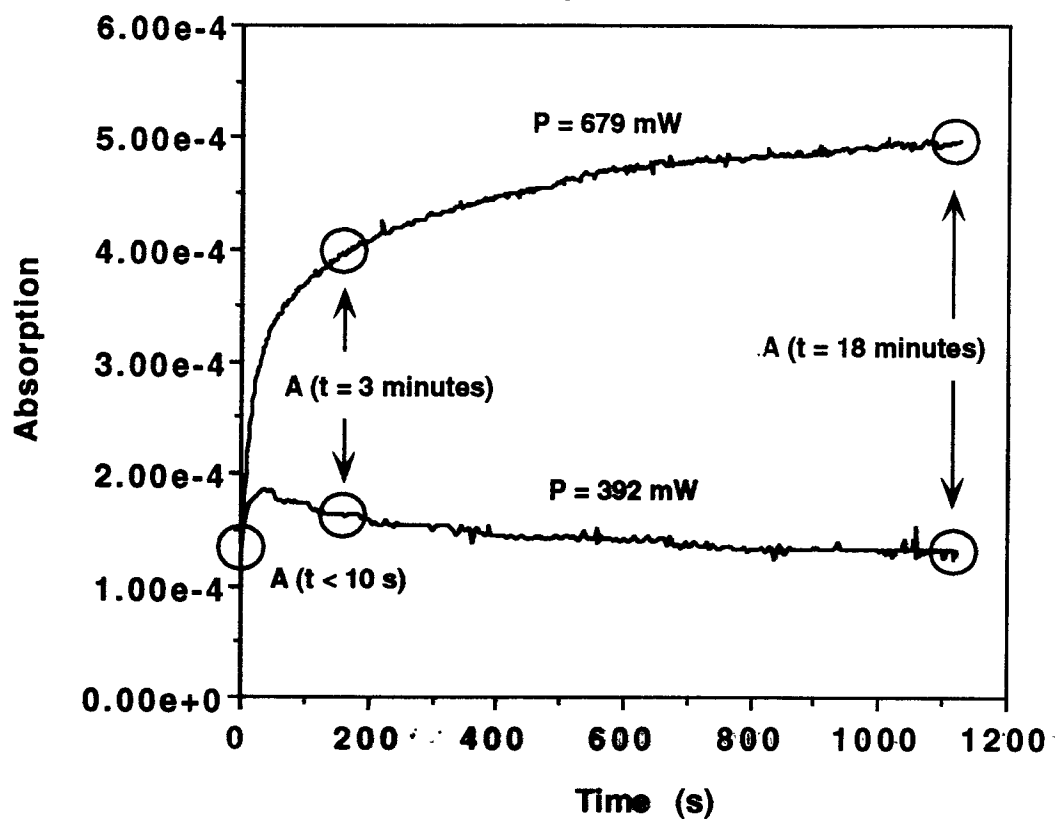


Figure 7. Laser-induced reduction in optical absorption observed in real time using the STL method.

Sample: SN325



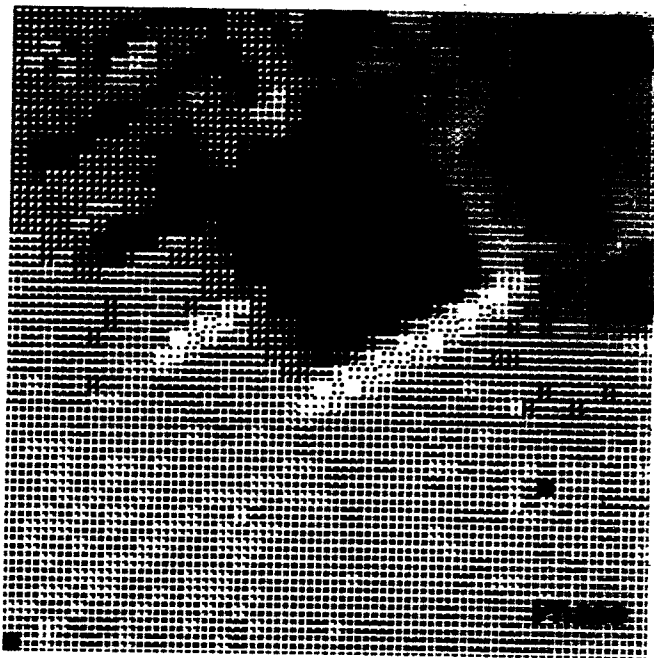


5e-2



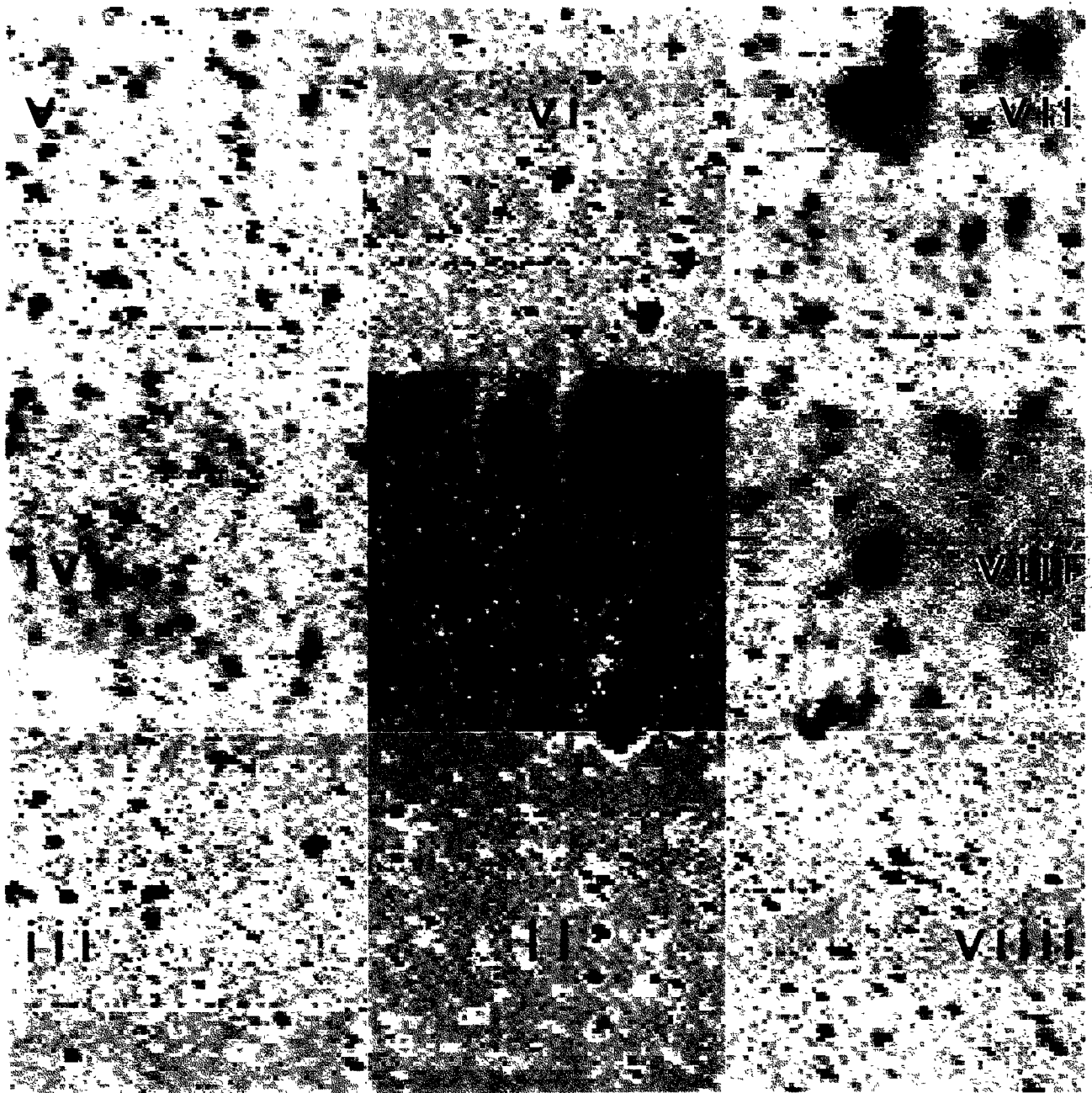
1e-2

-120

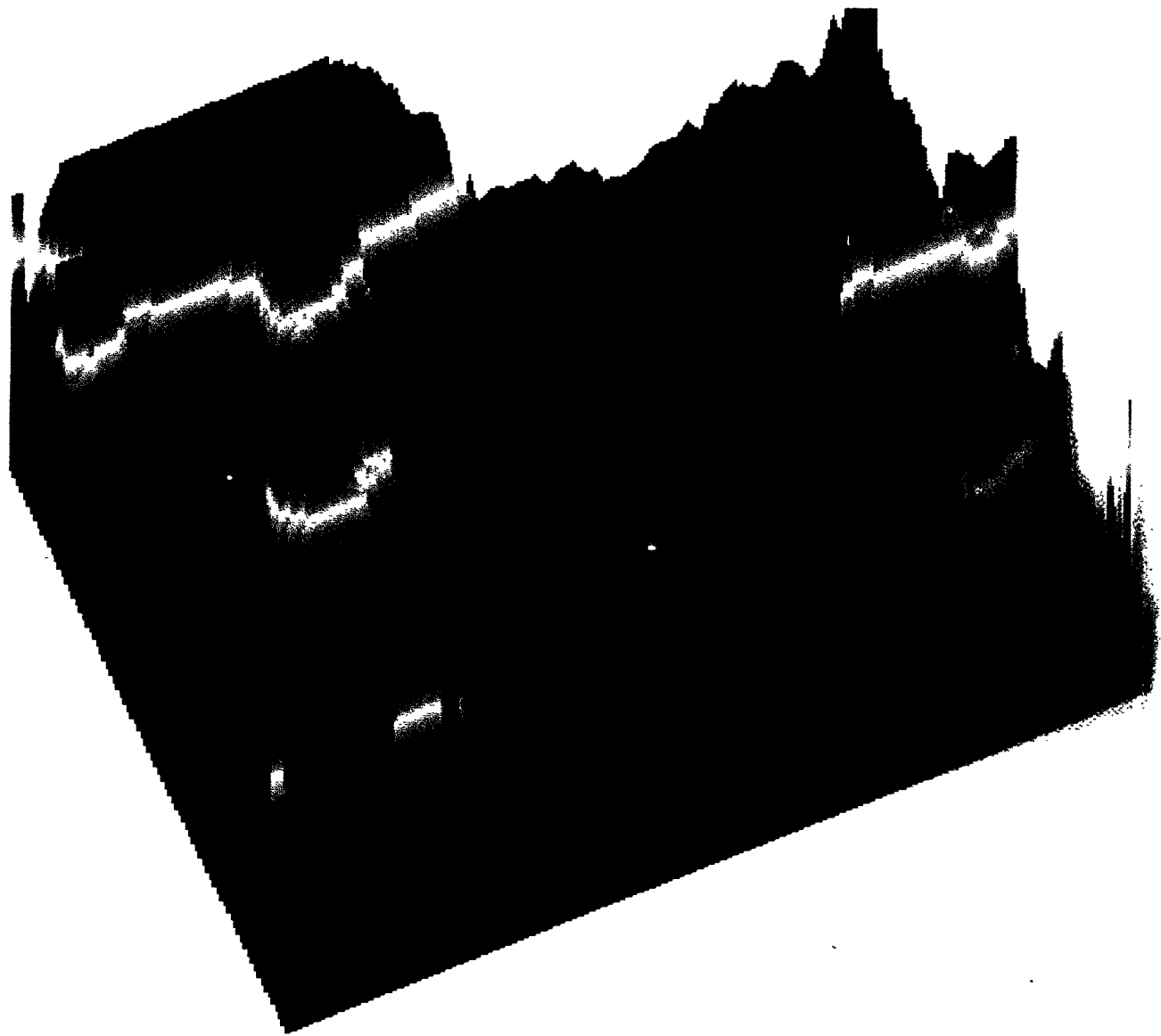


-160

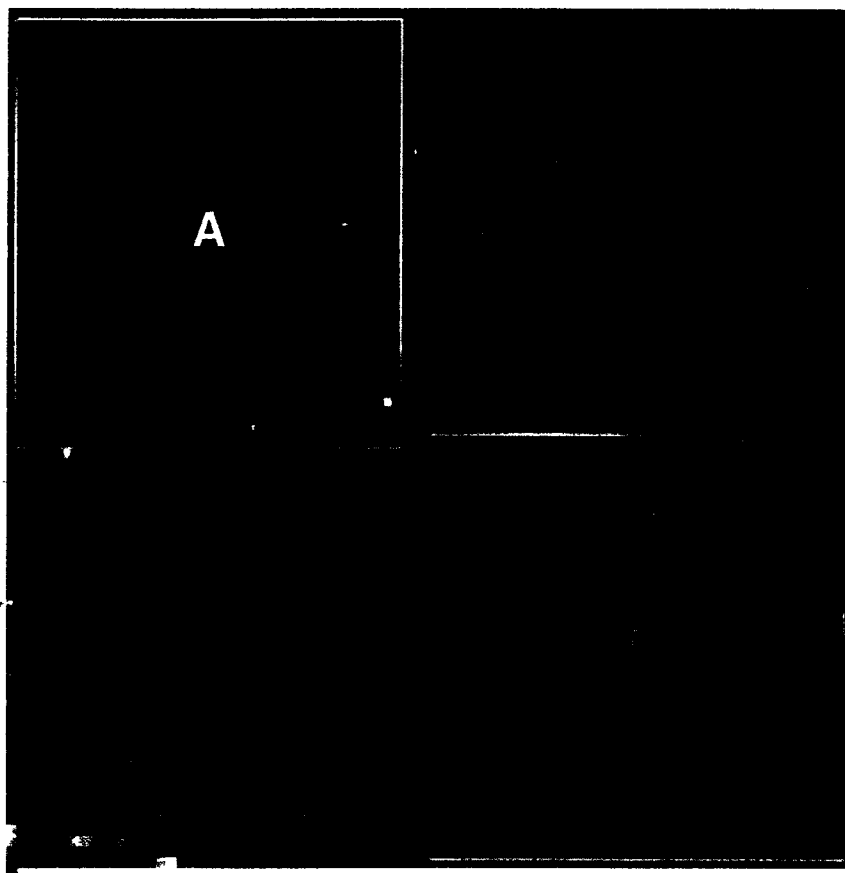
Scanned area: 600  $\mu\text{m}$  x 600  $\mu\text{m}$   
Modulation frequency:  $f = 500 \text{ Hz}$



**Sample:** SNB282  
**Scanned area:** 3 mm x 3 mm  
**Spatial resolution:** ~10 $\mu$ m



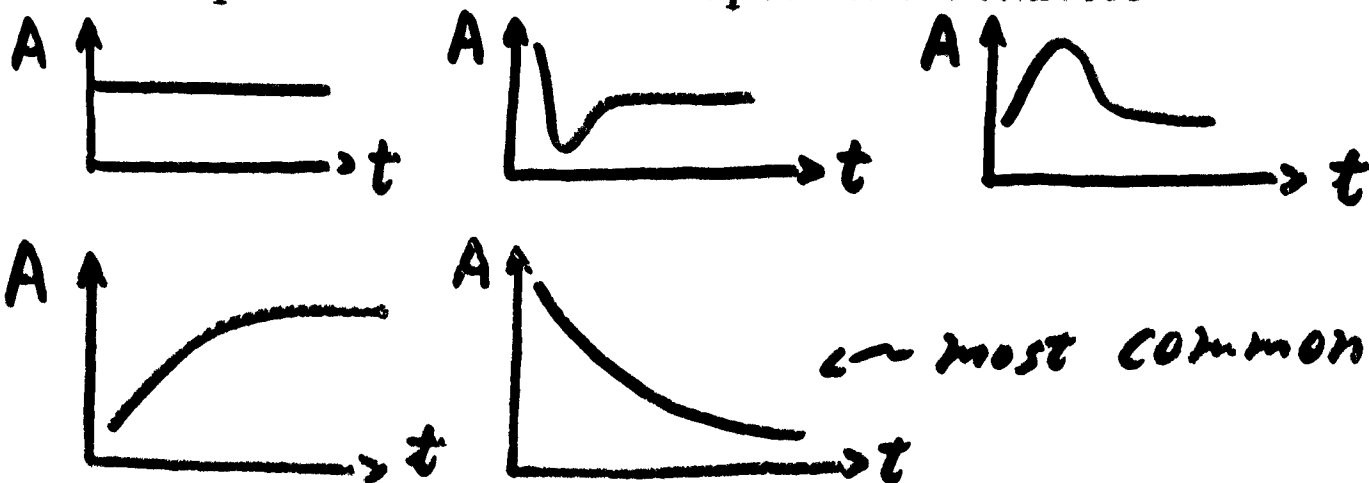
## Sample 325



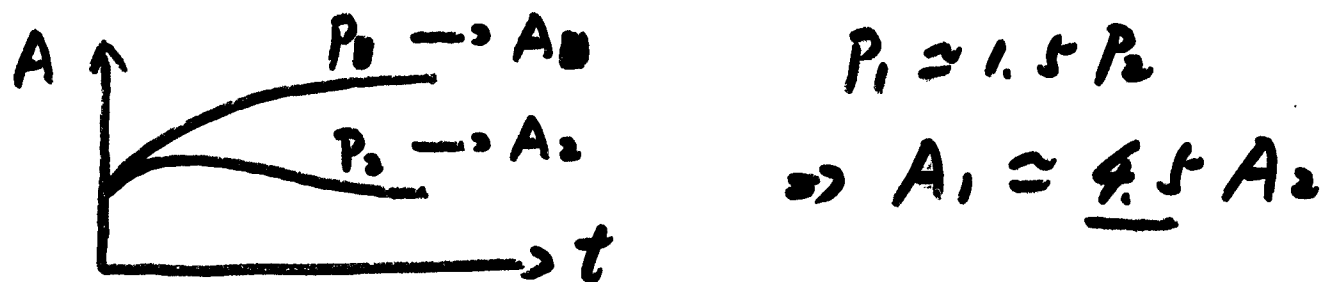
<u>Sampling Area</u>	<u>Averaged Pixel Value</u>	
Whole picture	Mean: 16.67	Dev: 20.20
Area A	Mean: 12.41	Dev: 6.86
Area B	Mean: 24.18	Dev: 34.50

## Observation Summary

1. Absorptance has a time-dependent behavior



2. Absorptance has a non-linear behavior



3. Coatings are spatially non-uniform in absorptance.

# Conclusions

## Surface Thermal Lensing (STL)

**Sensitive:** 10 ppb at 1 watt incident power

**Stable:** precision < 5% at 0.5 ppm absorptance

**Fast:** time resolution  $\approx$  10 msec

**Spatial resolution:**  $\approx$  1  $\mu\text{m}$

**Non-contact and non-destructive**

*Low cost absorptance system*

*Small footprint (< 2 ft<sup>2</sup>)*

*Easy to use*

## **Recommended procedure for absorptance measurements for high power laser applications**

### **Required:**

- 1. Measurement conditions are as close as possible to operational conditions (e.g. power density).**
- 2. Record time-dependence (on the order of a few minutes).**

### **Optional:**

- 3. Random sampling or 2-dimensional scanning to assess spatial non-uniformities.**

### **Academics**

- 4. Non-linear mechanisms**
- 5. Absorptance sources and distributions**

system will combine the advantage of being both highly sensitive and easy-to-use, as in the case for the STL technique.

Fig. 5 shows the design of the experimental setup. The CPD system is going to share with the STL method the same pump laser source, and the two systems are designed such that they can work both independently and simultaneously.

For absorption measurements of bulk materials using CPD, the calibration of the absorption value is going to be achieved by using accurate modeling. The model will be verified by samples with known absorption before it is used for calibration.

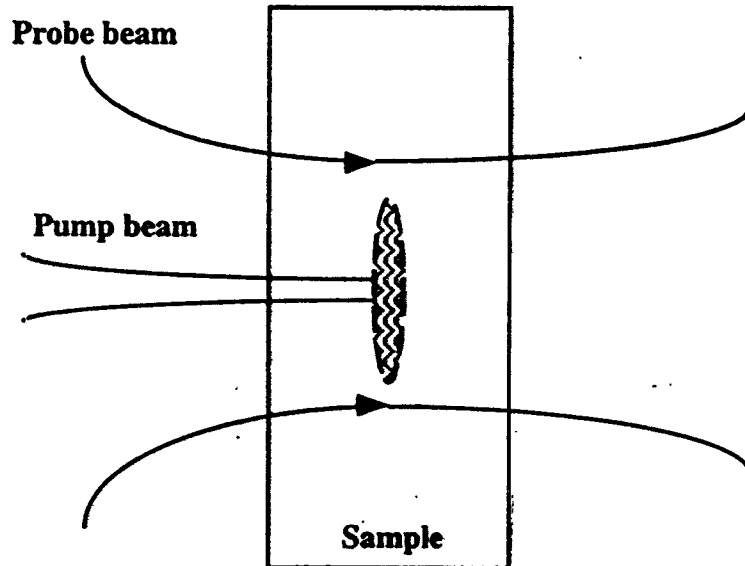


Figure 4. Illustration of the principle of collinear photothermal diffraction (CPD).

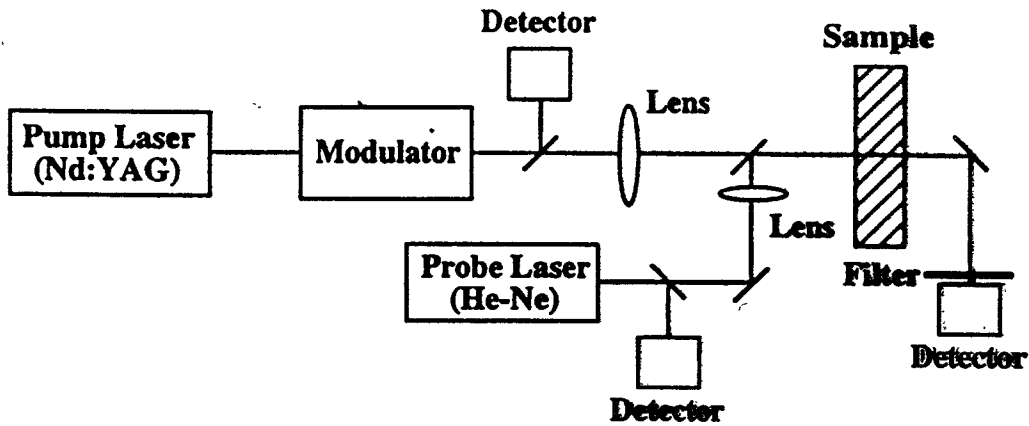


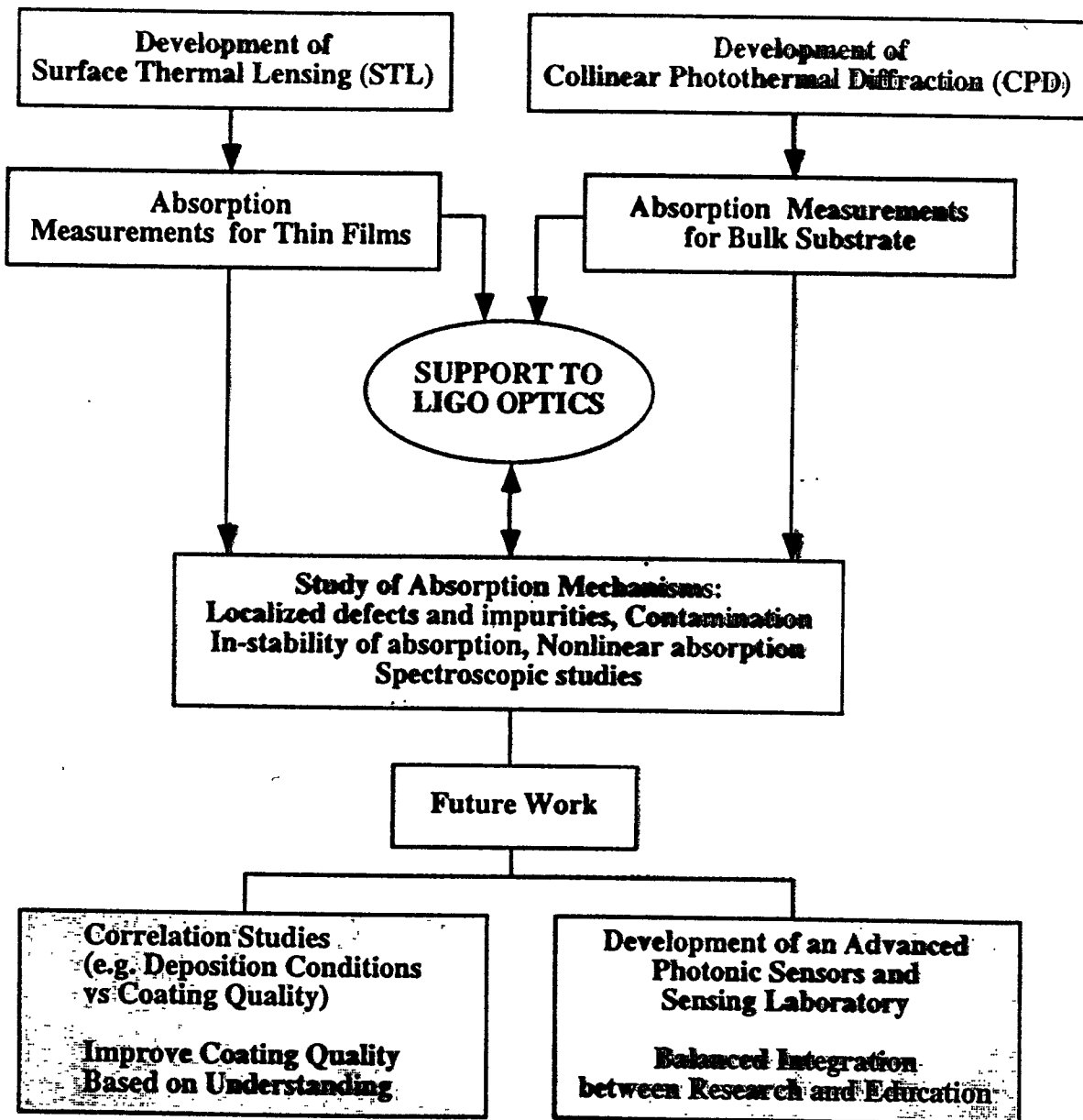
Figure 5. Depiction of the experimental setup for CPD.

#### 4. Study of Absorption Mechanisms for Thin Film Coatings

For dielectric thin films the absorption loss is usually higher than that of the corresponding bulk material and depends strongly on the specific film deposition processes. To reduce the absorption and, hence, to develop high quality optical coatings, it is necessary to better understand the absorption mechanisms. For this reason we propose to use the third year of the project to perform the following studies.



For STL, in contrast to PDS, a probe beam with a size similar to or larger than the lateral dimension of the thermally deformed area is reflected from the sample surface, as shown in Figure 1 (b). In this case the deformed area on the sample surface is acting as a curved mirror which distorts the wavefront of the probe beam. The shape of the surface deformation is thus recorded in the diffraction pattern of the reflected probe beam, which can be analyzed by using either a CCD camera or a scanned photo-detector.



**Figure 1. Outline of the proposed work.**

The advantages of STL over PDS and other photothermal techniques are multiple. It has the same high sensitivity but it avoids the critical alignment requirements for PDS, and, hence, is an easy-to-handle method which can be easily applied to the study of a variety of materials in different environments. Furthermore, if a CCD camera is used for detecting the diffraction pattern, STL obtains the full field information of the surface deformation.