

**LIGO Meeting: December 2, 1997**

# **Doubly Resonant Sideband Control for LIGO**

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## **Agenda**

1. Brief Outline of current scheme - Singly Resonant SideBand (SRSB) - and potential problems
2. The Doubly Resonant SideBand (DRSB) method
3. Summary of advantages/disadvantages of the SRSB
4. Issues surrounding the DRSB method
5. Risk Assessment
6. Schedule Impact
7. A.O.B.

It will be assumed that the document "Doubly Resonant Sideband Control for LIGO" has been widely distributed.

## 1. *SRSB*

- Carrier resonant in arm cavities and Power recycling cavity (PRC)

RF sidebands resonant in PRC only

non-resonant sideband used for alignment

- *Length Control*
  - In-phase demodulation at ports 1 and 2
  - > common mode length control
  - > requires reasonable sb gain

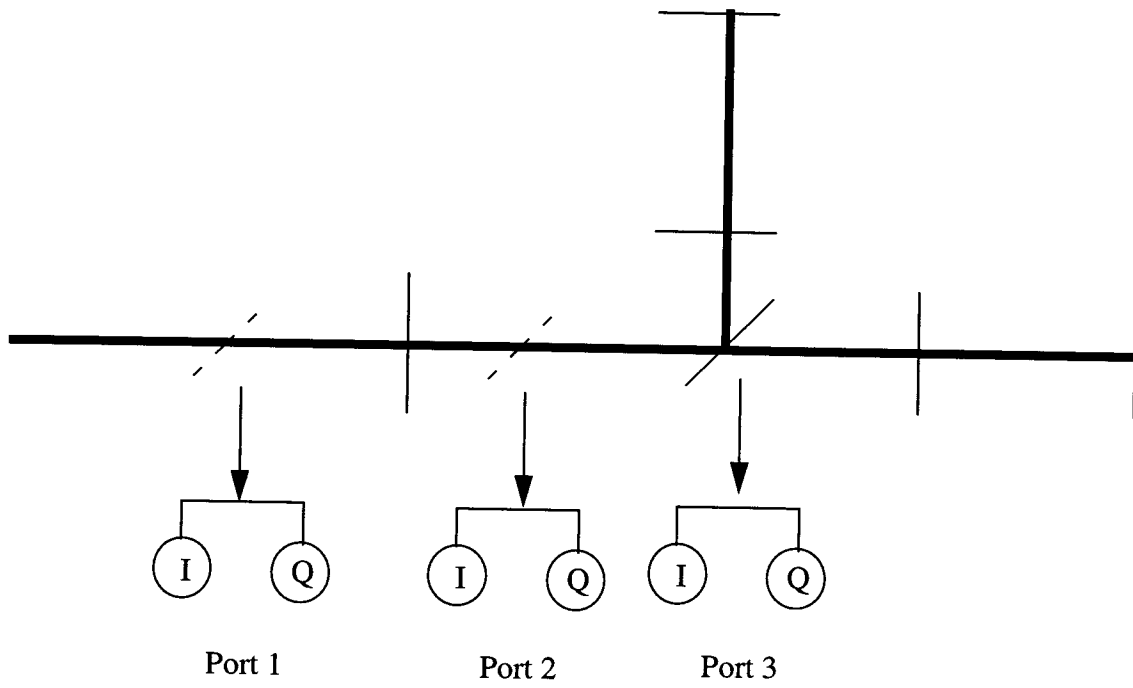
Quad. demodulation at ports 2 and 3

-> differential mode length control

Table 2

- *Temporal stability* Table 3

-> dominated by audio noise on the rf sidebands as carrier is highly filtered in coupled arm cavity/PRC system



**Figure 1: Schematic layout of LIGO interferometer**

**Table 2: SRSB Matrix of Discriminants ( $f = 24$  MHz)**

	$d\Phi_+$	$d\phi_+$
$dV_1$	-1	-0.001
$dV_2$	-1	+0.0007
	$d\Phi_-$	$d\phi_-$
$dV_2$	0.0076	1
$dV_3$	-1	-0.0076

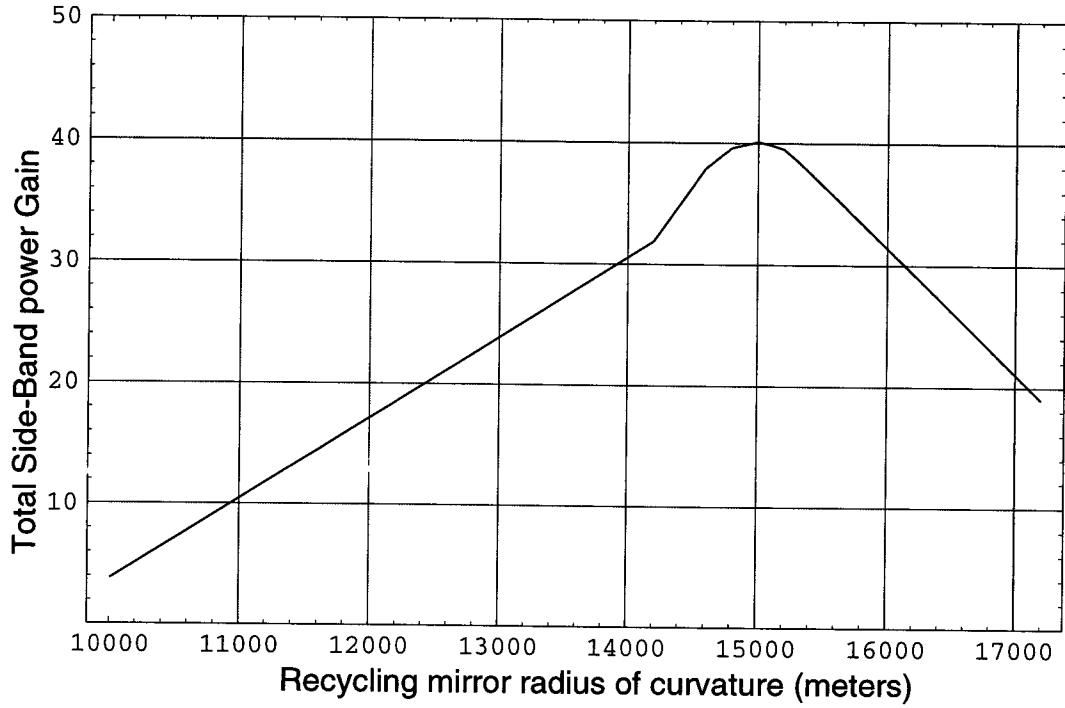
**Table 3: Stability Requirements (/radish) on SRSB at 100 Hz<sup>a</sup> ( $f = 24$  MHz)**

Laser		Oscillator		LO
Freq	Amp	Phase	Amp	Phase
$2 \times 10^{-7}$	$2 \times 10^{-8}$	-90 dBc	$2 \times 10^{-8}$	-80 dBc <sup>b</sup> -120 dBc <sup>c</sup>

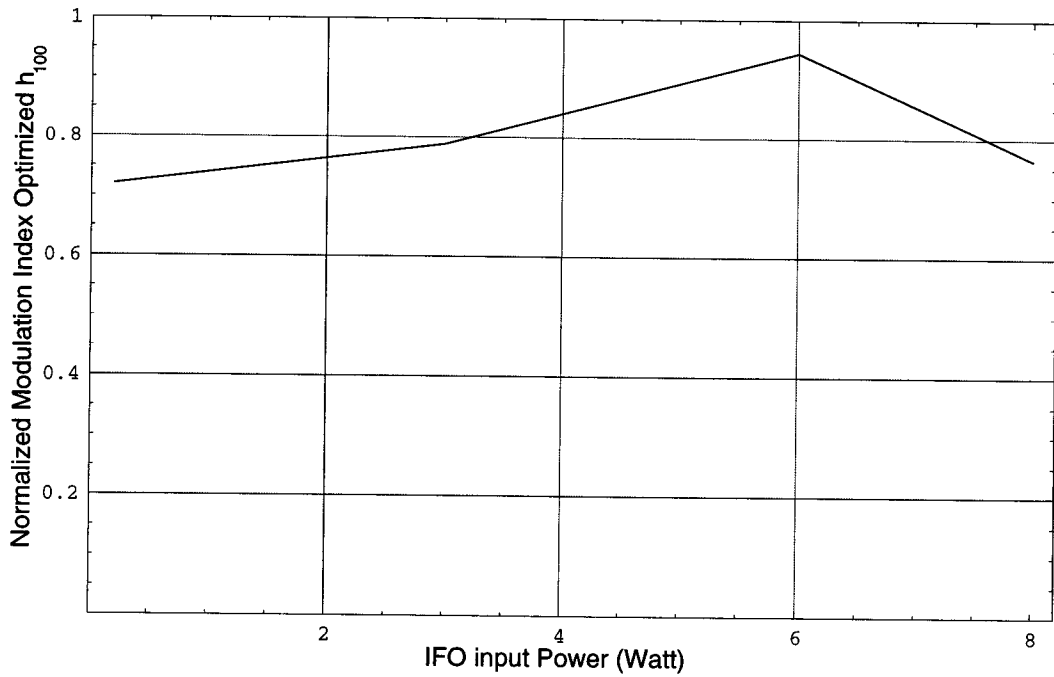
a. assumes  $dL_- = 10^{-13}$  m

b. assumes sideband exact resonance in mode cleaner

c. assumes sideband detune from mode cleaner of 100 Hz



**Figure 2: SB gain for optimal Recycling Mirror ROC of 15 km**



**Figure 3: IFO sensitivity**

## Summary of Control Issues with SRSB

Power, W	$\delta/2,$	$\Gamma$	Panti, 00	Gsb, 00	1- sig strength	Matrix, cm
8	0.21,	0.36	0.26	4.6	0.2	1 0.008 -1 -0.005
6	0.11,	0.3	0.72	34	1	-1 -0.003 -1 0.005
3	0.22,		0.22	5	0.2	1 0.008 -1 -0.005
0	0.33,	0.44	0.11	.94	0.1	1 0.008 -1 -0.006

Nb: for NRSB cm signal change at Port 1 is 1 0.008,

For DRSB Meets

TODAY

LIGO.

- *Spatial stability*

Carrier propagates in a stable geometry  
-> resilient to spatial errors

Sidebands propagate only in an essentially degenerate plane mirror cavity

- > highly sensitive to spatial errors
- > sets tolerance on ROC s. (6%)

- *Thermal Lensing*

Carrier is again resilient for the same reason as above and phase distortions tend to cancel

Sidebands are strongly lensed

- > without correction of the ROC of the power recycling mirror, sb gain falls from 40 to less than 2 compromising length control system and sensitivity
- > recovered if ROC adjusted

Figs 2 and 3.

- *Issues:*

prediction of the correct ROC

interferometer restricted to operate properly at only one input power

other PRC effects



## 2. *The DRSB Method*

- RF sidebands are set to resonate in the arm cavities and the PRC along with the carrier
- signal still extracted as it is the difference between the carrier fields reflected off each arm which is measured, not a comparison between the rf sidebands and the carrier  
-> sensitivity achievable is similar to standard technique

- *Thermal lensing*

RF sidebands now propagate in coupled cavity geometry -> resilient to lensing

- *Spatial Stability*

tolerance to ROC error ~ 50%

- *Temporal Stability*

RF sidebands are now highly filtered

see Table 5

- rf oscillator phase noise
- cavity length matching

- *Length Control*

linearly dependent length control

-> cannot extract Michelson d.o.f.

see Table 4

### 3. *Summary Comparison*

Table 1.

**Table 5: Stability Requirements (/radish) on DRSB at 100 Hz<sup>a</sup> (f = 19.7 MHz)**

Laser		Oscillator		LO
Freq	Amp	Phase	Amp	Phase
$1 \times 10^{-5}$	$1 \times 10^{-6}$	-84 dBc	$1 \times 10^{-6}$	-120 dBc <sup>b</sup>

a. assumes  $dL_- = 10^{-13}$  m

b. assumes sideband exact resonance in mode cleaner; not greatly changed by 100 Hz MC detuning.

**Table 4: DRSB Matrix of Discriminants**

	$d\Phi_+$	$d\phi_+$
$dV_1$	-1	-0.0076
$dV_2$	1	+0.0076
	$d\Phi_-$	$d\phi_-$
$dV_2$	1	0.0076
$dV_3$	-1	-0.0076

Because of the linear dependence of the mixer signals we cannot extract Michelson d.o.f.

## 2 SUMMARY OF ADVANTAGES / DISADVANTAGES OF DRSB

**Table 1: Modulation Scheme Comparison**

	<b>DRSB</b>	<b>SRSB</b>
<b>DRSB Advantages</b>		
<u>Spatial Filtering - Tolerance to Input Power, ROC, at 10% loss in sens</u>		
Maximum power input (6 W nominal)	> 60 W	7 W
Maximum ROC error in RM	> 50 %	6 %
<u>Length Sensing and Control</u>		
Change in sideband gain for above power and ROC tolerances	1 %	40 %
Change in sideband gain for lock acquisition (cold) mode	1 %	factor 25
<u>Temporal Filtering - Coupling of Laser Fluctuations to GW signal</u>		
Frequency Noise	1	50
Intensity Noise	1	50
Beam Jitter Noise	1	50
RF Intensity Noise	1	50
<b>DRSB Disadvantages</b>		
DC Arm length control	0.3 mm	-
Required sidebands	19.7 MHz, 502.35MHz	25 MHz
Schedule impact on ISC	~ 3 months (?)	-

The most serious technical problem in the implementation of DRSB is control of the arm cavity DC length at the level of 0.3 mm. We have no experience in DC control of a 4 km cavity at this level; however we find an adequate error signal for the DC length control is available. We also have no experience with sideband generation and detection at 500 MHz, but the technology for this is available. These problems are discussed in later sections.

#### 4. *Issues with DRSB*

- (a) DC arm cavity length control required to  $\sim 0.3$  mm
  - > should be possible
- (b) RF oscillator phase noise
- (c) Controlling the Michelson
  - propose to use SRSB for these d.o.f.
  - $f_{\text{SRSB}} > 4.5 \times f_{\text{DRSB}}$  to avoid intermod. products (unless MZ used?)
  - given this must choose frequency close to 1 FSR of Michelson asymmetry to recover sb gain
  - permits the choice of SRSB such that transmission to antisymmetric port is small  $\implies f_{\text{SRSB}} = 25.5 \times f_{\text{DRSB}}$
  - Control matrix given in Table 6.

**Table 6: DRSB Matrix of Discriminants with  $f_D = 19.7$  MHz,  $f_S = 502.35$  MHz**

	$d\Phi_+$	$d\phi_+$
$dV_1^S$	-1	-0.004
$dV_2^S$	-1	+0.006
$dV_1^D$	1	0.0076
$dV_2^D$	-1	-0.0076
	$d\Phi_-$	$d\phi_-$
$dV_2^S$	0.0076	1
$dV_3^S$	-1	-0.0076
$dV_2^D$	1	0.0076
$dV_3^D$	-1	-0.0076

This matrix yields linear independence of the arm and Michelson d.o.f.

## Two Obvious Issues:

(i) This SRSB will still suffer strong thermal lensing  
-> still need to carefully determine appropriate ROC;

But: - SRSB is only used for auxiliary length control, where requirements are lower, not GW signal extraction  
- SRSB is overcoupled, so can suffer some loss

In addition:

- extra noise filtering can be used to allow greater tolerance to differential length change and hence impact of distortions such as thermal lensing is much less significant.

The bottom line: if the SRSB control used here with the DRSB is compromised, it would have catastrophically failed as the primary control system.

(ii) detection at 500 MHz  
alternatives

## 5. *Risk Assessment*

S. Whitcomb

## 6. *Design and Schedule Impact*

Electronics

Mechanics

The 2 km Interferometer

## 7. *A.O.B.*



# SRSB RISK ASSESSMENT

## WHAT MIGHT GO WRONG

- THERMAL LENSING OFF BY 25%
- " " " " 100%
- RM RADIUS OFF BY 6%
- CONTAMINATION CAUSES ABSORPTION
- LASER INTENSITY STABILIZATION NOT ADEQUATE
- RF OSCILLATOR AM FEEDTHROUGH
- POINTING NOISE (BEAM JITTER)
- START-UP PROBLEM FOR LOCK-ACQUISITION
- COMPLETE BREAKDOWN OF CONTROL SYSTEM

## PROBABILITY/IMPACT

- HIGH /  $h_{SN} \uparrow 10\%$
- LOW /  $h_{SN} \uparrow 50\%$
- MODERATE /  $h_{SN} \uparrow 5\%$
- LOW-MOD /  $h_{SN} \uparrow 10\%$   
IN 6 MONTHS
- LOW /  $h_{SN} \uparrow \times 2$
- LOW(?) /  $h_{SN} \uparrow \times 2$
- LOW(?) /  $h_{SN} \uparrow \times 2$
- LOW / SEVERAL MONTH DELAY IN COMMISSIONING
- V. LOW / MAJOR DELAY/REWORK

ALMOST CERTAINLY

- + SRSB SCHEME WILL ~~PROBABLY~~ WORK FOR INITIAL LIGO
- WILL PROBABLY SUFFER  $\sim 10\%$  IN SHOT NOISE
- SYSTEM DOES NOT HAVE MUCH ROBUSTNESS OR ROOM FOR GROWTH

# DRSB RISK ASSESSMENT

## WHAT MIGHT GO WRONG

- RF OSCILLATOR CAN'T MEET  $\phi$  NOISE SPEC
- HIGH  $f$  PHOTODIODE PROBLEMS
- DELAY IN COMMISSIONING (DUE TO EXTRA LSC WORK)
- DIFFICULTIES MATCHING ARMS
- UNKNOWN NOISE COUPLING

## PROBABILITY/IMPACT

- ? LOW /  $h_{SN} \uparrow \times 2$
- LOW / COMMISSIONING DELAY ?
- LOW-MOD / DELAYS IN FINDING "REAL" PROBLEM
- LOW / MINOR DELAYS
- ?? / ??

- 
- + DRSB WILL (ALMOST) CERTAINLY WORK IF SRSB WORKS, AND IN SOME CASES WHEN IT WON'T.
  - + SIGNIFICANT MARGIN FOR MANY NOISE SOURCES (LASER INTENSITY NOISE, ...)
  - + - POSSIBLE DELAYS NOW VS. POSSIBLE LATER ONES
  - WILL NEED SIGNIFICANT DEVELOPMENT
  - + GIVES SOME ROOM FOR GROWTH (THOUGH NOT AS MUCH AS I WOULD LIKE)

# (SW's) ESTIMATE OF SCHEDULE IMPACT

## WHAT CHANGES

## HOW MUCH DELAY

- OPTICAL/MECHANICAL LAYOUT  
M/C, RC LENGTHS  
PICK-OFFS, RELOCATIONS, ETC  
1 MONTH  
3 MON
- SUSPENSION HEIGHT ADAPTORS  
1 MONTH (+ 1 MONTH)
- RM COATING  
—
- RF SOURCE  
NEW FREQUENCIES  
TIGHTER PHASE SPEC  
} 4-6 MON(?)
- HIGH FREQUENCY MODULATORS  
NEGLIGIBLE?
- HIGH FREQUENCY PHOTODIODES  
6 MON(?)
- SERVO DESIGN  
MODELING  
TUNING  
} 6 MON(?)
- NEW WFS PHOTODIODE  
4 MON

# LASERS AND OPTICS

## Core Optics: Substrate Absorption

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