

Advanced LIGO Technical Description Part I

NSF Review of Advanced LIGO Project 25-27 April 2011

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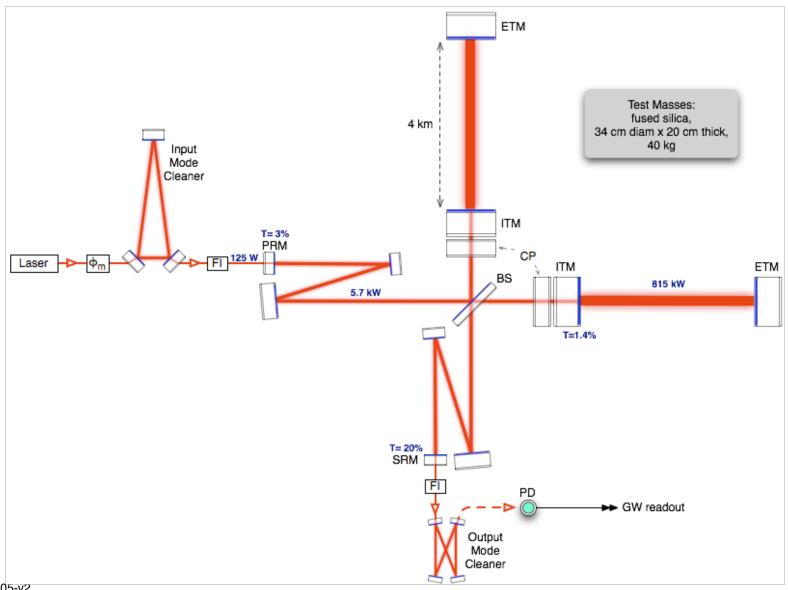


Agenda

- Systems Engineering (SYS) I: Interferometer design
- Pre-stabilized Laser (PSL)
- Input Optics (IO)
- Core Optics Components (COC)
- Interferometer Sensing & Control (ISC)
- Systems Engineering (SYS) II: High Power & gas damping
- Auxiliary Optics Subsystem (AOS)
- Seismic Isolation (SEI)
- Suspensions (SUS)
- Data Acquisition, Diagnostics, Networking & Supervisory Control (DAQ)
- Data Computing System (DCS)
- Facility Modifications & Preparation (FMP)
- Systems Engineering (SYS) III: layout, interfaces, etc
- Summary

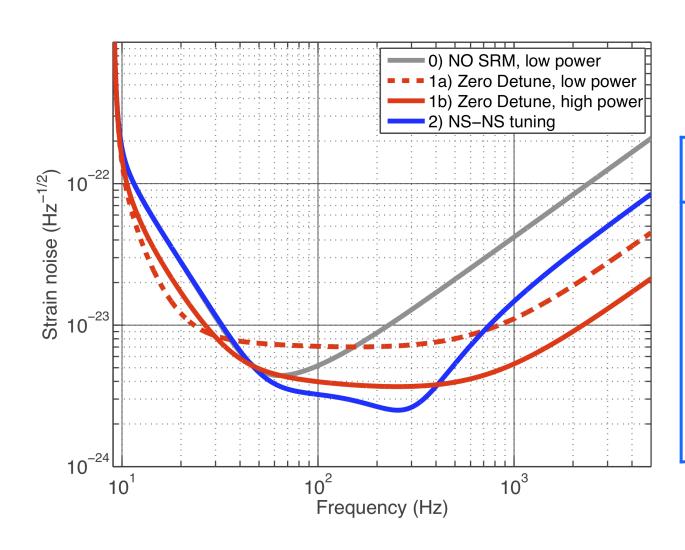


Systems: Interferometer Design





Interferometer Performance



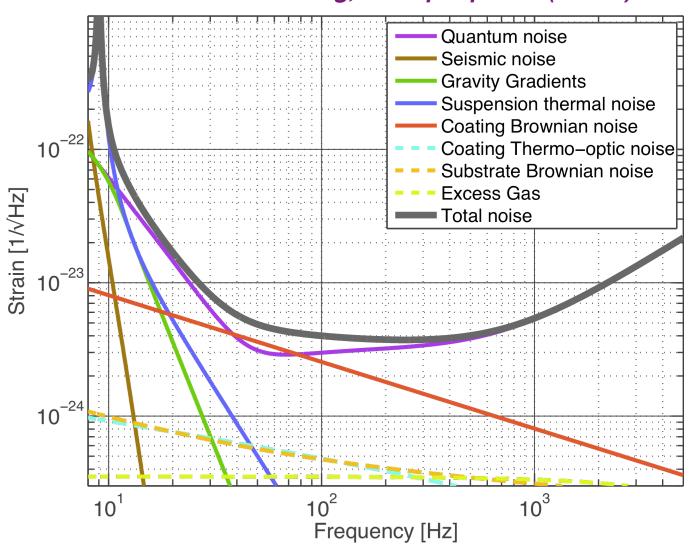
Detection range for binary inspirals

case	NS-NS	BH-BH (30 M _⊙)
0	150 Mpc	1.60 Gpc
1a	145 Mpc	1.65 Gpc
1b	190 Mpc	1.85 Gpc
2	200 Mpc	1.65 Gpc



Limiting Noise Sources

Broadband tuning, full input power (125 W)

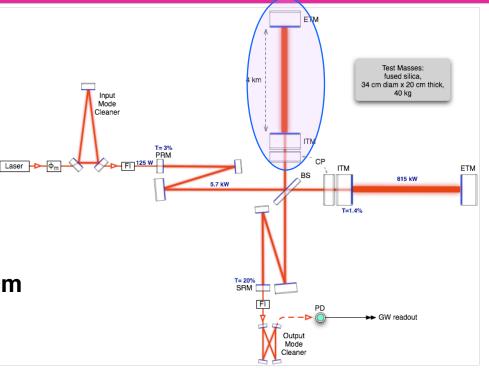




Key Interferometer Features

Arm cavity design

- Finesse: 450
 - » 2x higher than iLIGO
 - » Value involves trade-offs between optical loss, sensitivity to noise in other degrees-of-freedom, and interferometer sensitivity in different modes of operation
- Beam sizes: 6.2 cm on ETM, 5.3 cm on ITM
 - » Approx. 50% larger than iLIGO, to reduce thermal noise
 - » Smaller beam on the ITM to allow smaller optic apertures in the vertex
- Cavities are made to be dichroic
 - » Low finesse cavity for 532 nm to aid in lock acquisition



Near-confocal design

$$R_{ITM}$$
, $R_{FTM} \approx L$

» Gives better angular stability than the near flat-flat case



Key Interferometer Features

Signal Recycling

- Add a partially transmitting mirror to the anti-symmetric port
- Provides some ability to alter the interferometer frequency response

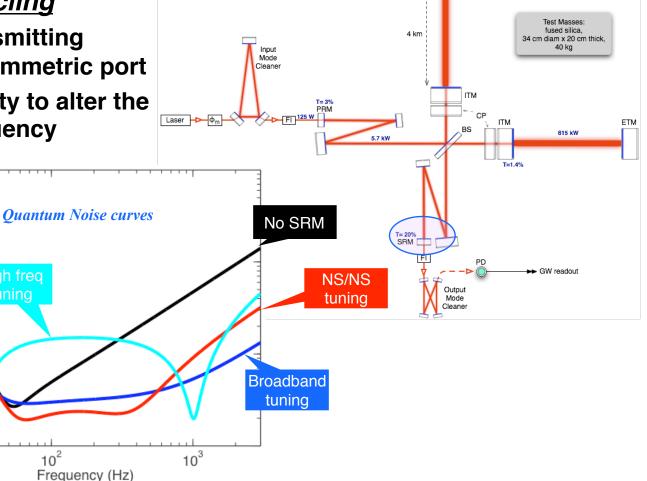
High freq

Strain noise (Hz^{-1/2})

10 -22

10 -24

10



Baseline is broadband tuning



Key Interferometer Features

Stable Recycling Cavities

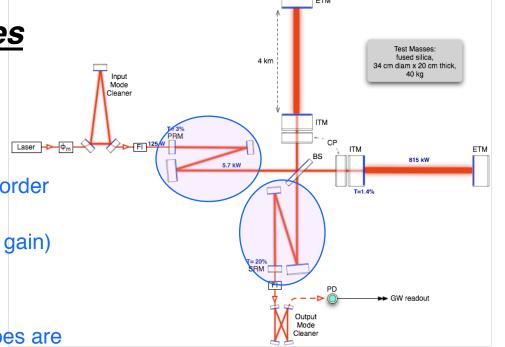
iLIGO has a marginally stable recycling cavity

» Nearly a plane-plane cavity; higher order spatial modes are nearly resonant

» Spatial mode quality (& thus optical gain) suffers

Stable geometry for AdvLIGO

- » Beam expansion/reduction telescopes are included in the recycling cavities
- » Higher order spatial modes are suppressed
- » Configuration is more tolerant to optical distortions





Pre-stabilized laser (PSL)

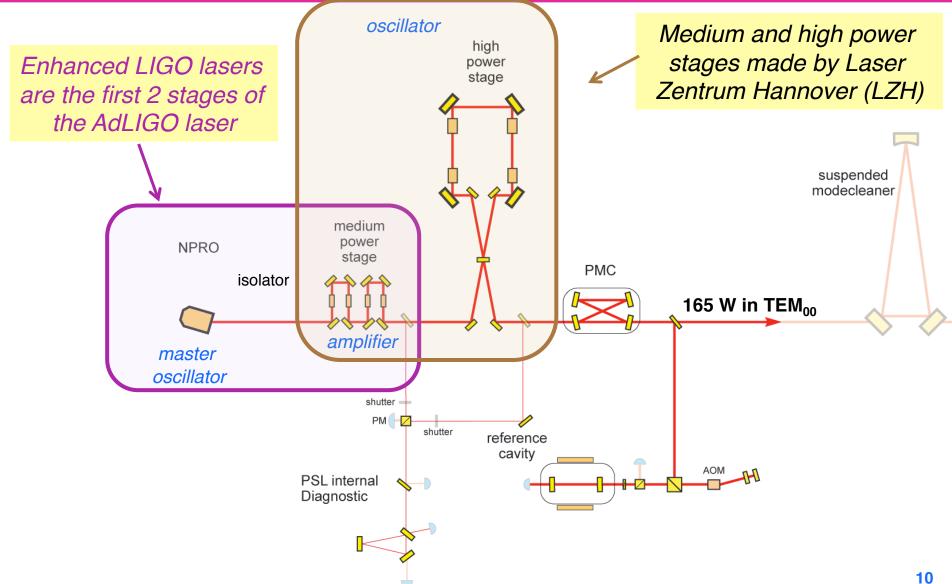
- High power laser: 180 Watts
- Laser frequency pre-stabilization & frequency actuation
- Pre-mode cleaner for spatial clean-up and high-frequency filtering
- Diagnostic tools
- Laser power stabilization
- Laser safety measures
- Facility infrastructure
 - » Laser and laser diode enclosures
 - » Instrument racks, crates, power supplies
 - » Supervisory controls & DAQ interfacing

Supplied by Albert Einstein Institute (Hannover)

Supplied by LIGO Lab

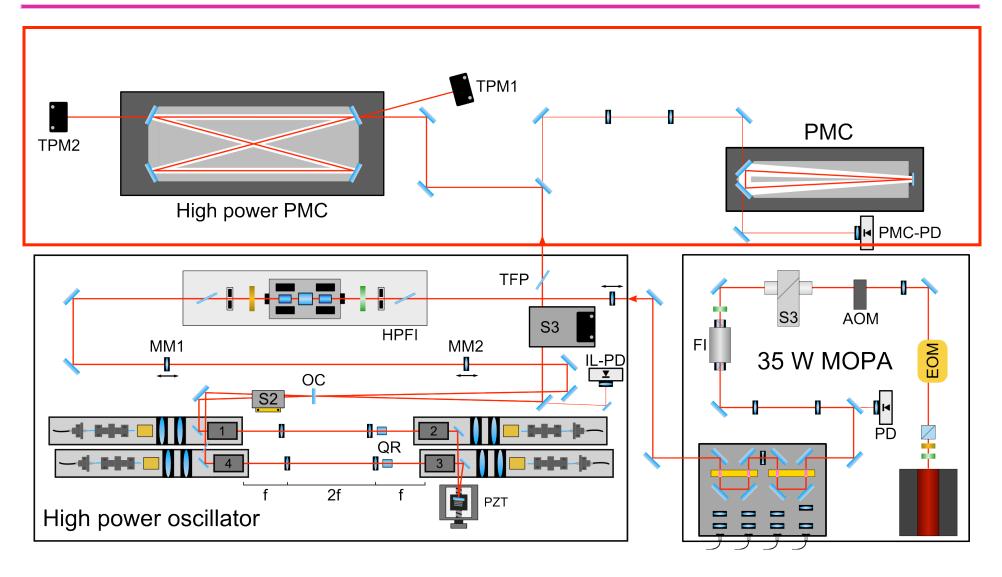


Pre-stabilized laser



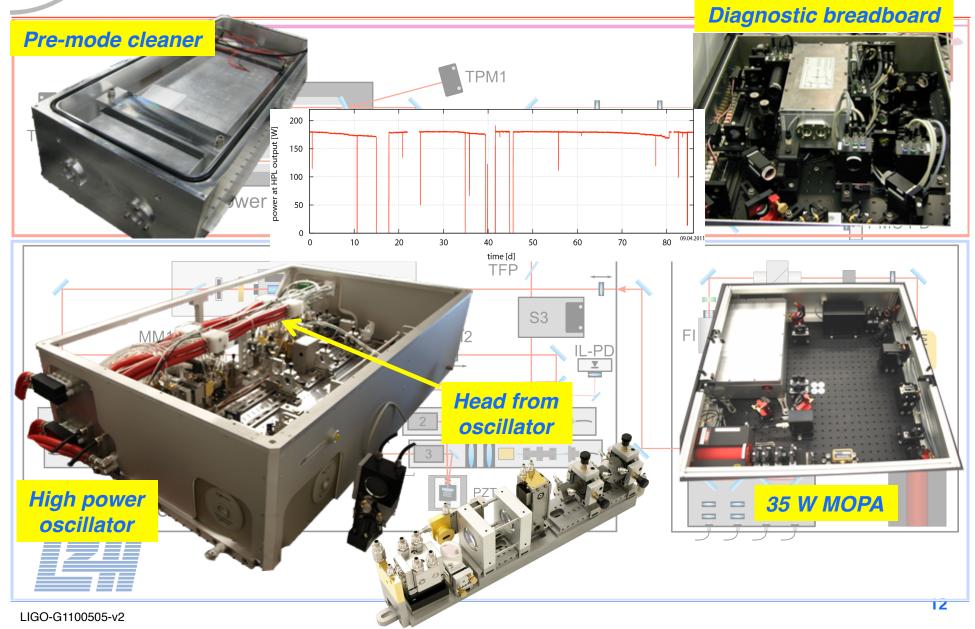


Pre-stabilized Laser





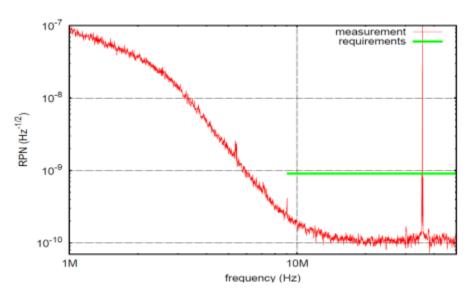
Pre-Stabilized Laser

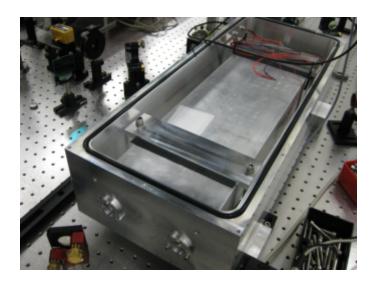


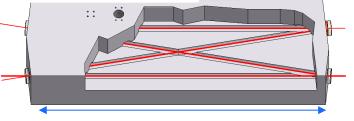


Pre-mode cleaner: spatial & temporal filtering

- bow tie configuration, round-trip length of 2m
- Finesse of 124, circulating power 9kW (200W input)
- Linewidth 575 kHz (HWHM)
- Length control with automatic lock acquisition
- PZT actuator / thermal actuator to off-load PZT



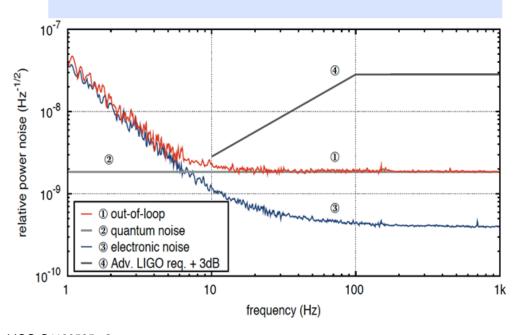


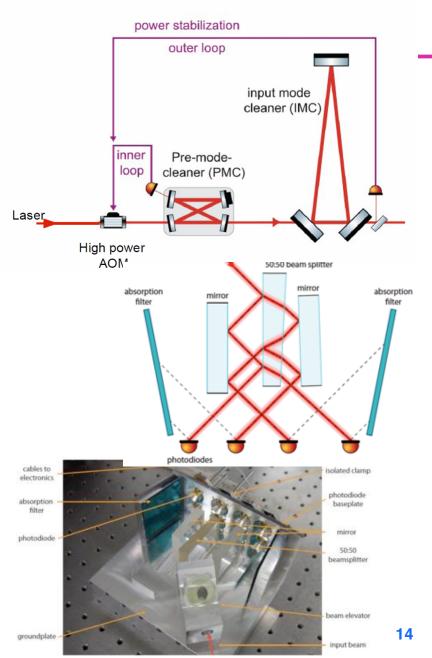




Laser Power Stabilization

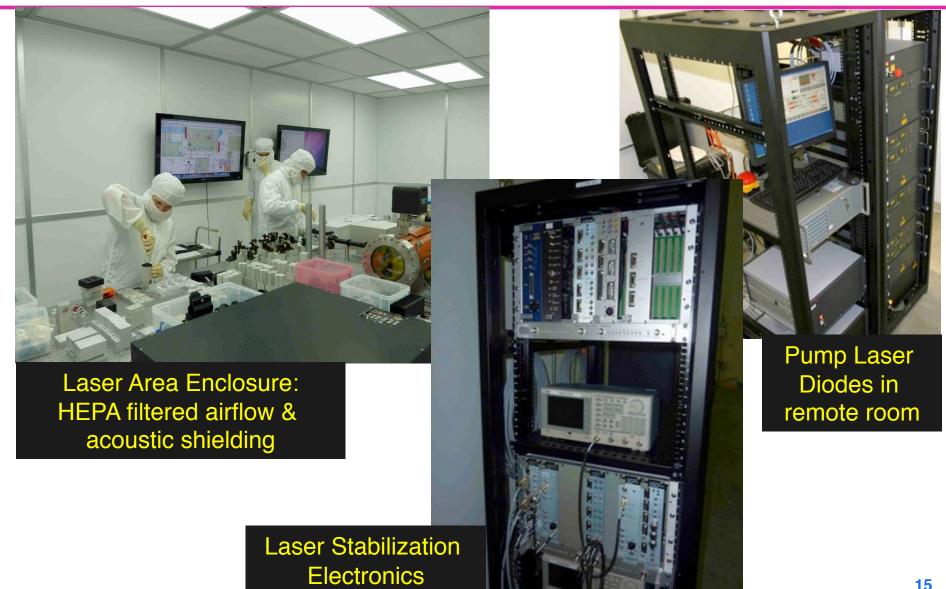
- High power acousto-optic modulator provides actuation
- Prototype power stabilization photodetector (outer loop)
- Stabilized noise requirement of RIN < 2x10⁻⁹ / Hz^{1/2} at 10 Hz: demonstrated w/ NPRO laser







LLO PSL currently being installed



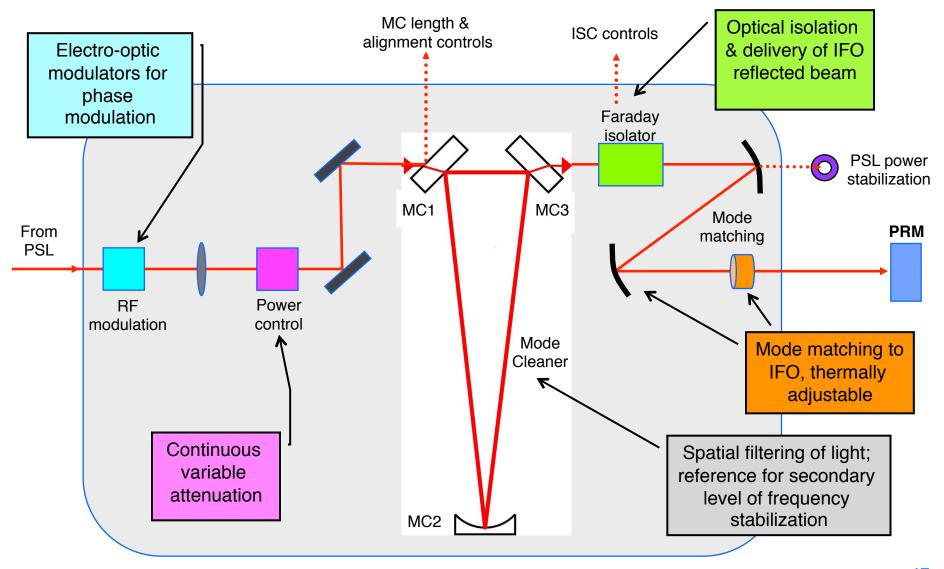


PSL Status

- First laser arrived in January 2011 & is being installed
 - H2 laser to ship in June 2011
- Fabrication continues at LZH
 - » All 35 W MOPA's have been fabricated
 - » 2nd and 3rd High Power Lasers have been assembled
- A full PSL 'Reference Laser' remains in operation at AEI
 - » Long term testing
 - » Control loop tuning and other testing
- Final design review of outer-loop photodetector in near term
- No significant technical issues remaining



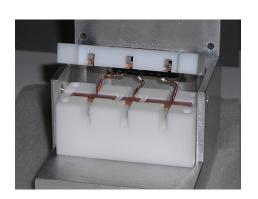
Input Optics





IO: Modulators and Isolators

- Phase modulator is rubidium titanyl phosphate (RTP)
 - » Electro-optic response similar to LiNbO₃
 - » lower absorption → lower thermal lensing
 - » Large aperture: 4 mm x 4 mm
 - Multiple electrodes on single crystal for multi-RF drive

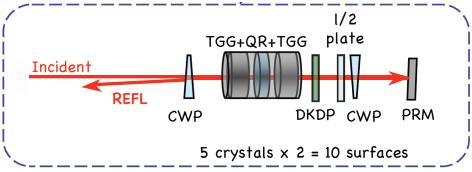


» Tested to 140 W

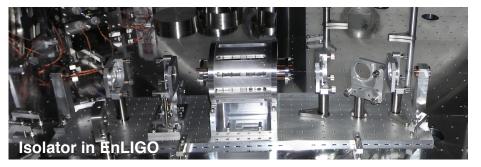


In-vacuum Faraday Isolator

» Thermal birefringence compensation using two crystals and a quartz rotator



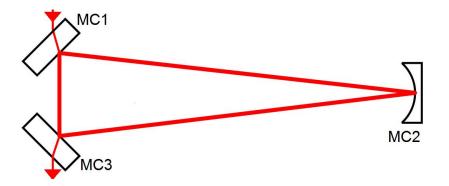
» -dn/dT element (DKDP) to compensate thermal lensing

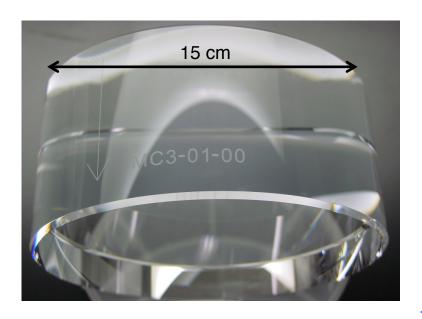




Input Mode Cleaner Design

- Triangular ring cavity
- L/2 = 16.5 m
- FSR = 9.1 MHz
- Finesse = 520
- P_{stored} = 23 kW (@ 165 W input)
- MC mirrors suspended from triple suspensions
- MC mirrors
 - » 15 cm diameter x 10 cm thick
 - » 3 kg: 12x heavier than iLIGO, to limit noise due to radiation pressure

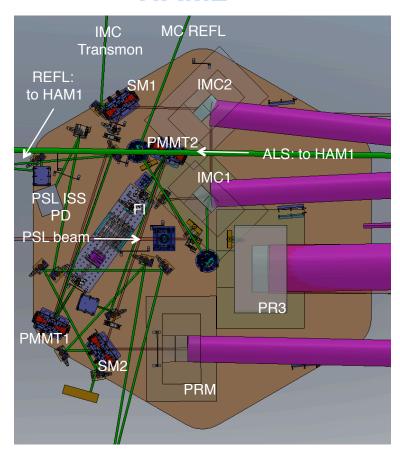




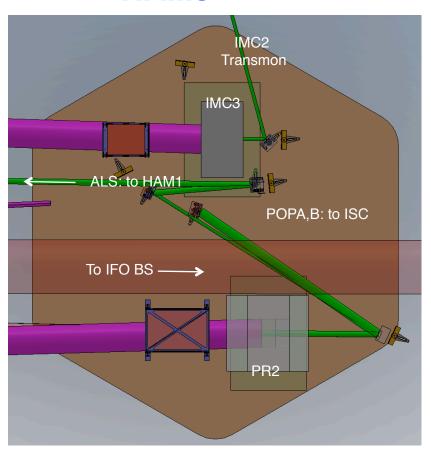


Fitting It All In ...

HAM2



HAM3





Ham Auxiliary Suspensions

- Steer the beam between the IMC output and the Power Recycling Mirror (interferometer input)
- Final design review completed in fall 2010

Single stage suspension, including blade springs for vertical compliance

Suspension provides isolation to maintain low beam pointing fluctuations, & active control of beam pointing





Input Optics Status

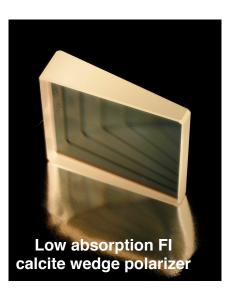
Final design elements completed in past ~6 months

» HAM Auxiliary Suspensions & IO section baffles

Production status

- » All Input Mode Cleaner mirrors and small recycling cavity mirrors (PRM, SRM, PR2, SR2) have been polished and coated
- » In-house Metrology in progress: IMC mirrors show suitably low absorption, 0.4-0.5 ppm
- » HAM Aux suspension components all fabricated
- » Modulator crystals and custom polarizers received
- No significant technical issues remaining







Core Optics Components

40 kg

- Substrate procurement
- Substrate polishing
- Dielectric coatings
- Metrology
- Transport, handling, cleaning

Large beam size on test masses (6 cm radius), to reduce thermal noise 40 kg **Compensation plates:** 34cm φ x 10cm 37cm **∮** x 6cm PR3 ITM Round-trip optical loss: T = 1.4%75 ppm max **Recycling Mirrors:** 26.5cm ϕ x 10cm SR3

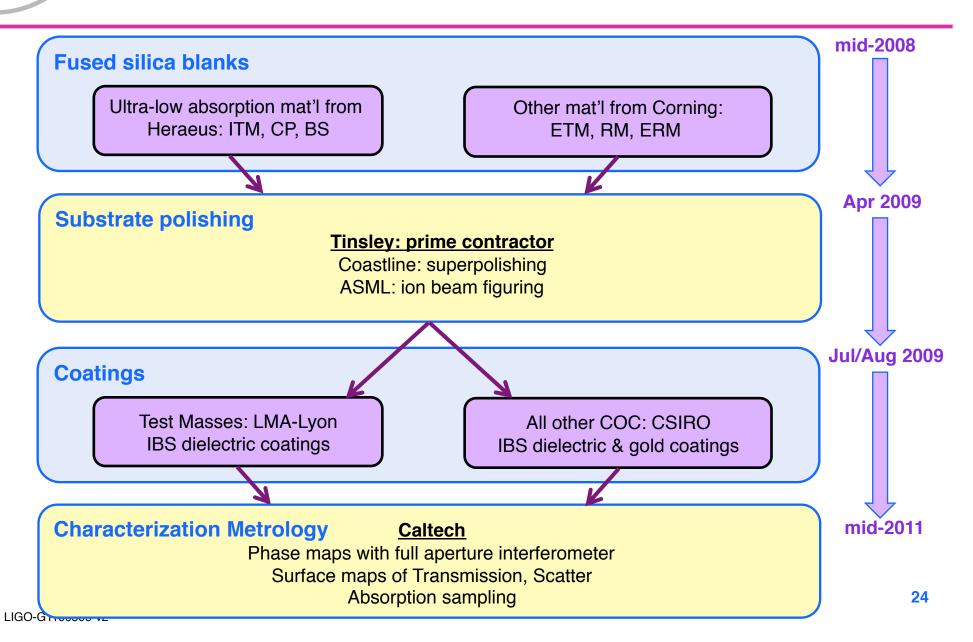
Test Masses:

34cm φ x 20cm

All COC are fused silica substrates with ion-beam sputtered dielectric coatings



Core Optic production flow





COC Polishing

- Arm cavity loss goal: 75 ppm round-trip (2x lower than iLIGO)
 - » Requires low micro-roughness, low mid-spatial frequency distortion, good ROC matching between optics

Test mass specifications:

- < 0.3 nm rms figure (tilt, astig., power removed)</p>
- Matching of ROCs to +/- 3 m (out of 2000 m)
- < 0.16 nm rms micro-roughness

Technique:

- Initial figuring and superpolishing done at Coastline Optics
- Final ion beam figuring at ASML

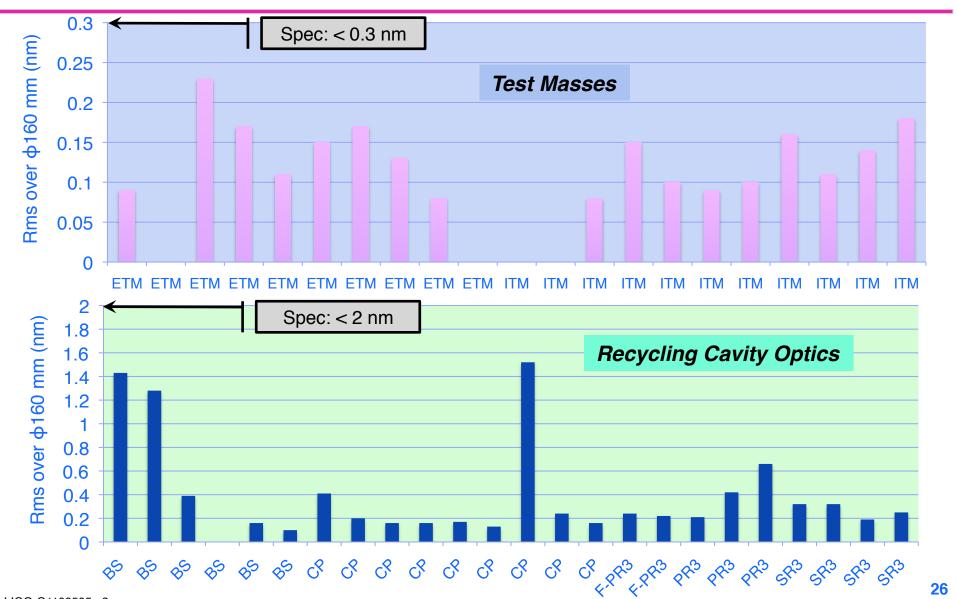
Polishing Results:

- 12 of 20 polished Test Masses received factoring in some to be redone
 - » Radius of curvature is being met to +/-0.6 m on average (vs 3 m spec)
 - » Micro-roughness is 0.12 nm rms on average (vs 0.16 nm spec)



Polishing: wavefront error

(power & astigmatism removed)





COC Coatings: Test Masses

Baseline Requirements for Test Mass coatings

- » Low scatter: < 2 ppm</p>
- » Low absorption: < 0.5 ppm</p>
- » Low mechanical loss

- Rely on IBS coating technology from qualified vendors
- Several years of LSC R&D resulted in a better coating formula
- Alternating layers of silica and titanium-doped tantala (25%); gives approx. 40% lower loss than non-doped tantala (20% reduction in thermal noise amplitude)
- » Low wavefront distortion
 - Radius-of-curvature change: < 8 nm sag over central area
 - Higher order Zernikes: < 0.5 nm rms

LMA coating designs for the test masses are completed

» Non-1/4-wave stack: accommodates arm locking w// green beam & reduces thermal noise

	ETM	ITM
1064 nm	T = 5 ppm	T = 1.4 %
532 nm	T = 5%	T = 1%
Thermal noise w.r.t. ½-wave design	-2.5%	-5%

- » Absorption has been proven on first TM coating: 0.3-0.35 ppm
- Wavefront distortion spec not yet met factor of ~2 off; LMA is actively pursuing techniques to improve this



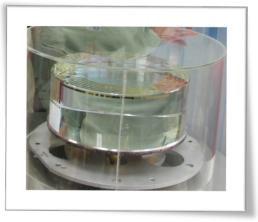
COC coatings: Recycling Cavity optics

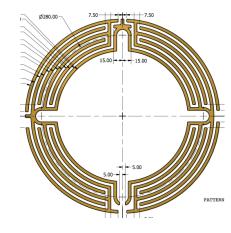
- CSIRO coating designs for other optics nearly complete
 - » Dielectric coatings also need to accommodate Hartmann sensor probe beams (near IR) & 532 nm beams
- Tooling/fixturing complete
 - » Sample coating runs made to prove fixturing
- Anti-Reflection coatings in the Recycling Cavities: need low AR and low absorption
 - » Much work to understand initial high absorption (~10 ppm); now understood and able to produce < 1 ppm absorption</p>
 - » AR < 50 ppm reg'd: indications are this will be achieved

Gold coatings on Reaction Masses for the Electro-Static

Drive

End Reaction Masses are completed & delivered







COC Status

- Polishing of initial set of mirror blanks nearly complete
- Replacement blanks being supplied for Fold Mirrors and some ETMs
 - » Corning material found to change sagitta (warp) under annealing: first at CSIRO with FMs, than at LMA with ETMs
 - » Both types are being replaced with Heraeus material that is stable under annealing

Dielectric coatings

- » Several technical issues have been found and fixed at both CSIRO and LMA
- » Critical remaining issue is achieving wavefront smoothness on the Test Masses (LMA)
- » First Test Mass, for the H2 Y-arm ITM, recently delivered to LHO; suitable for first arm cavity test, will need to be replaced in the long term

Characterization Metrology

» Zygo full aperture phase-shifting interferometer up and running at Caltech





Interferometer Sensing & Control (ISC)

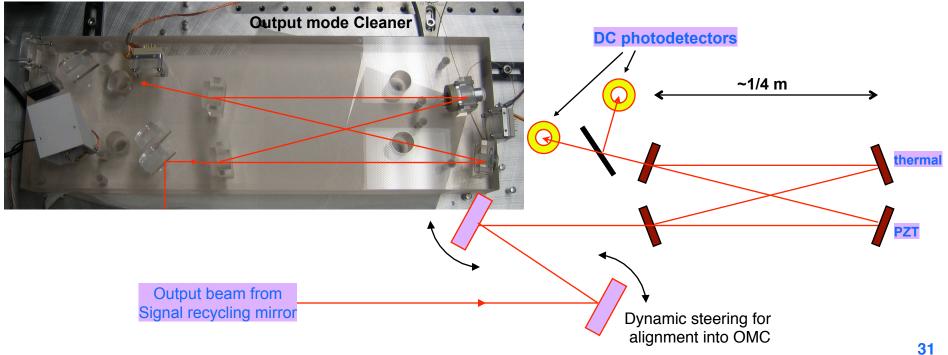
- Global sensing & control of the interferometer length degreesof-freedom
 - » LSC: Length Sensing & Control
 - y 4km arm lengths, recycling cavity lengths, Michelson, final stage of frequency control
 - » Readout of the gravitational wave channel
- Global sensing & control of the interferometer alignment
 - » ASC: Alignment Sensing & Control
 - y 4 test masses + 1 beamsplitter + 2 recycling mirrors = 7
- Lock acquisition of the interferometer
 - » Arm Length Stabilization system
- Detection tables for all senses beams
 - » Opto-mechanical hardware; photodetectors
- RF components: sources, distribution, demodulation
- Digital controls hardware and software for all length and alignment controls



ISC: Gravitational Wave channel readout

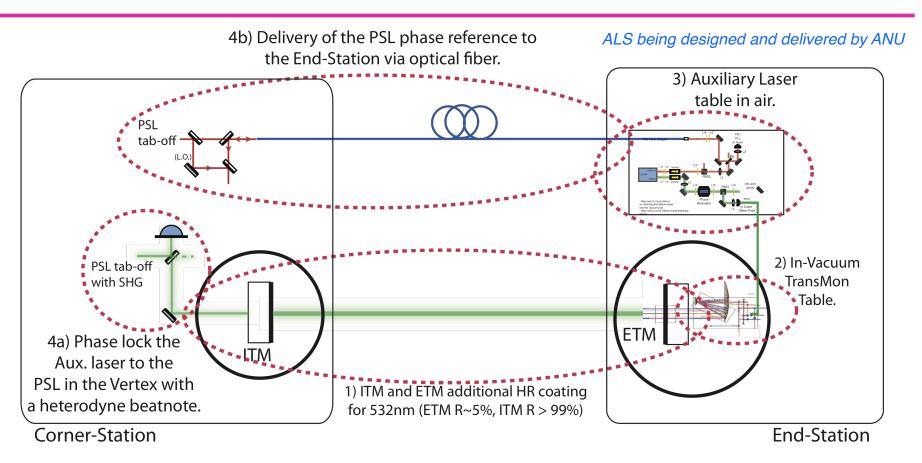
DC (homodyne) detection

- » Offset the arm from the dark fringe, to get a signal linear in strain
- » Use an output filter cavity to reduce shot noise (OMC = Output Mode Cleaner)
- » Two OMCs made for and operated in Enhanced LIGO; these will be re-used for first 2 aLIGO interferometers
- » Next generation OMC will be made for 3rd interferometer, & eventual replacement of other 2





ISC: Lock Acquisition & Arm Length Stabilization



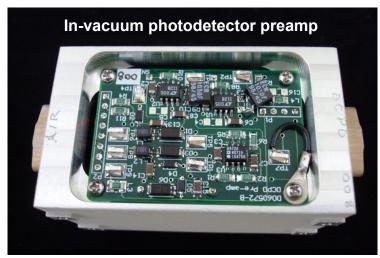
Lock Acquisition: strategy developed with E2E time-domain simulation

- » ALS stabilizes the arms to ~10 nm off-resonance, to ~ 1nm residual motion
- Three DOF in the corner are controlled using RF signals
- » Arms are brought into resonance in a controlled fashion

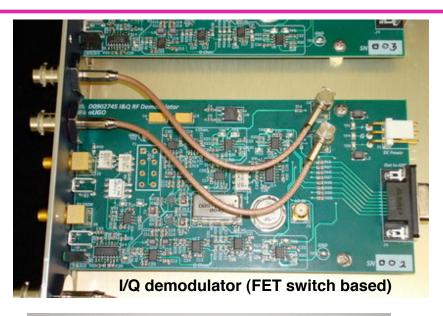


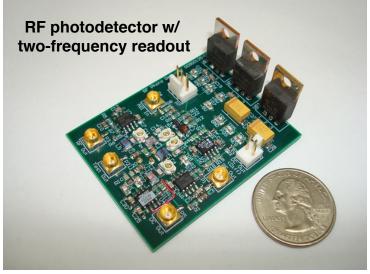
ISC Electronics Development

approximately 20 types of custom electronics modules











ISC Status

- Final design review completed in June 2010
- Electronics production underway
 - » RF oscillators and distribution amplifiers complete
 - » RF I&Q demodulators complete
 - » Quadrant photodetector transimpedance amplifier
 - » Whitening / VGA chassis
- Custom optics all ordered
 - » 1" & 2" mirrors, splitters, lenses: super-polished, IBS coated
- Opto-mechanical components largely procured
 - » In-vacuum mirror mounts, piezo-actuators, etc.
- Current focus is preparations for the first Arm Cavity
 - » Arm Length Stabilization: optics table at End Station
 - » Transmission Monitor optical breadboard





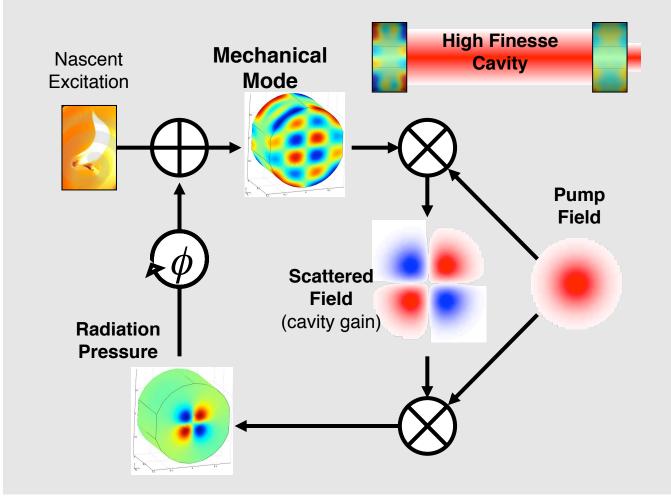
Systems design: high power operation issues

- Operational complexities associated with increasing power
 - Enhanced LIGO serves as a stepping stone: operation achieved at
 W into vacuum system
- Excess absorption in the high-reflector coatings
 - » Thermal Compensation System being designed to handle 2x specified coating absorption level
 - » Concern that contamination could go beyond that see Dennis' talk
- Parametric Instabilities



Parametric Instabilities

Combination of high stored optical power and low mechanical loss could cause an instability:



Model predictions:

A few – 10 modes per test mass could be unstable

Models assume very high acoustic mode Q-values: 10-30 million

Best defense is to reduce the acoustic mode Q's

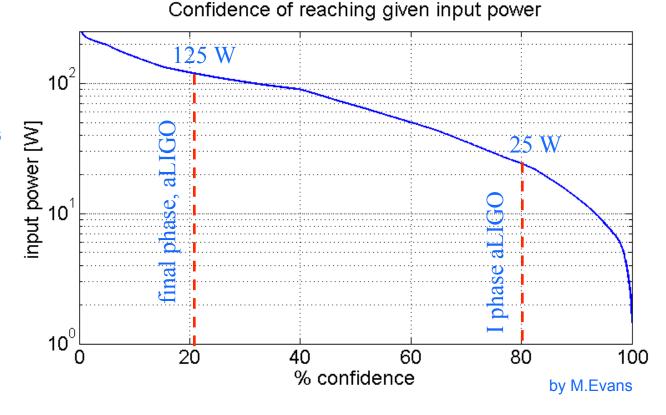


Parametric Instability: Modeling & predictions

- High parametric gain relies on close frequency matching of acoustic & optical modes
 - » These frequencies not known well enough to accurately calculate PI

Monte Carlo simulation with parameters varied over their plausible ranges

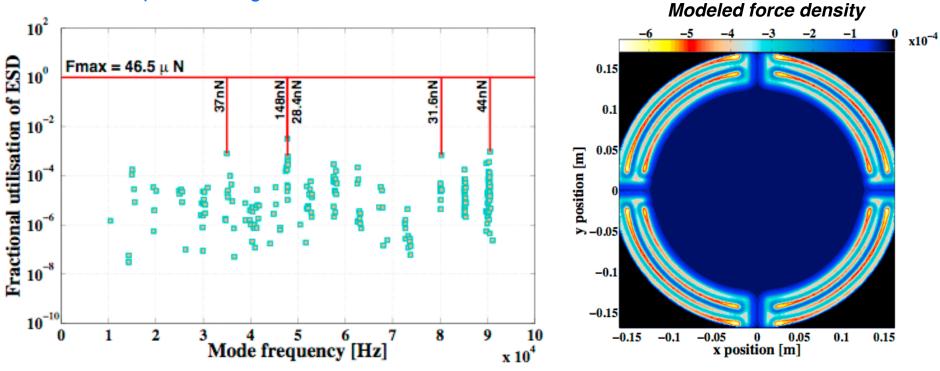
Plot shows result of ~100,000 trials





Active Acoustic Mode Damping

- Active damping using the electro-static actuators on the test masses
 - » FEA modeling of actuator force density & acoustic modes
 - » Calculate ESD force required to damp acoustic modes so that parametric gain is reduced to 0.1

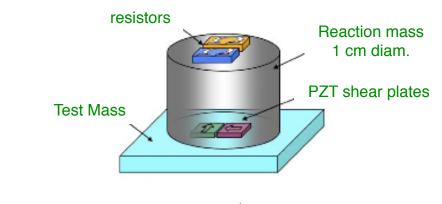


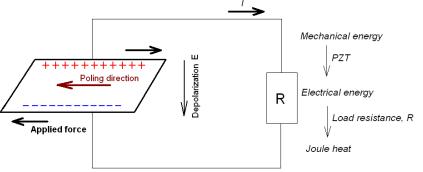


Passive Acoustic Mode Damping

Add a few resonant mechanical dampers to the Test Mass

- Resonant frequencies > 10 kHz
- Damper resonances are fairly broad (not 'tuned' dampers)
- Mounted to the barrel of the optic

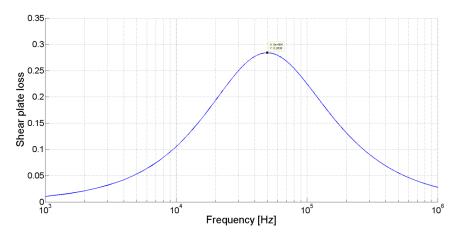




Shunted shear plate.

AMD: Acoustic Mode Damper Principal resonances designed to

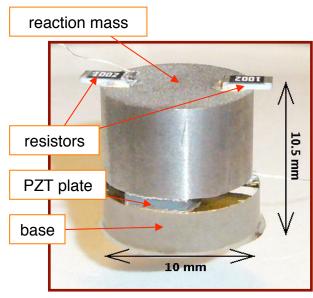
be between 10 - 60 kHz





Acoustic Mode Damper development

AMD prototyped on LASTI's quad suspension





- Test Mass Q's are very high:
 10-20 million measured for a dozen modes
- AMD damps these by 1-2 orders of magnitude
- However, most of this damping due to something other than resistor dissipation: PZT material & epoxy; these would produce excess thermal noise
- Concept still viable if lower loss
 PZTs and epoxy used; currently researching better materials



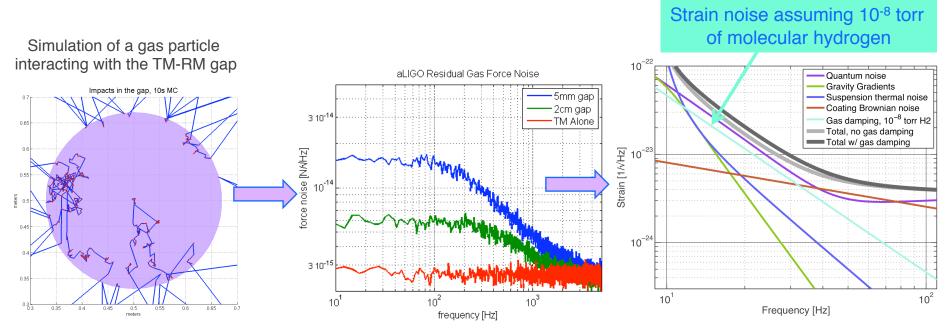
Summary of PI control strategy

- Active damping with Electro-Static Actuators is currently the first option
 - » Feasible if 1 or 2 modes per test mass are unstable; beyond that it gets complicated
- Acoustic Mode Dampers: better approach if we had a low noise AMD in hand
 - » Continued R&D on low noise AMDs
 - » Possible retrofit on installed Test Masses



System design: squeezed-film gas damping

- Residual gas in the gap between Test Mass and Reaction Mass produces increased damping of the TM pendulum motion
 - » Increased damping means higher suspension thermal noise, could be important for frequencies below about 50 Hz
 - » Monte Carlo simulations following gas particles in the gap used to calculate force noise





Mitigation of squeezed-film damping

Gap between ITM & CP was increased from 5 mm to 2 cm

- » Reduced the thickness of the CP
- » Minor changes to accommodate in the quad suspensions
- » ESD force reduced as a consequence, but there was margin to spare for the ITMs
- » Force noise reduced by factor of 2.6

ETM-ERM gap is a different issue

- » Rely on ESD force for lock acquisition & global control: don't want to reduce the force before we get experience with what we really need
- » New reaction mass geometries could reduce damping and retain ESD force
- » Solution could be a combination of new ERMs and more pumping; will be taken when we know more about required force & chamber pressure

