

# “ Performance of a thermally deformable mirror for correction of low-order beam aberrations”

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## **1. Motivation**

## **2. Prototype of a Thermally Deformable Mirror (TDM)**

- **Principle**
- **Experimental setup**

## **3. How to perform correction of low-order aberrations**

- **Calculation of the correction**
- **Zernike polynomials**
- **TDM properties**

## **4. Performance of the TDM**

- **Experimental results**
- **Actuation limits**
- **Possible improvements**

## **5. Conclusion and perspectives**

Advanced  
Gravitational  
Wave Detectors

Injection system

High power continuous laser > 100 W

Thermal lensing effects in the Input Mode  
Cleaner and the Faraday Isolator optics

Distorsion of the laser beam fundamental mode

Potential source of noise - Power losses :  
up to 10% mismatching onto the interferometer

**Advanced Virgo  
 injection laser beam**  
 @1064 nm  
 2.6 mm beam radius  
 Estimated RoC  
 variations: 200 m

Detection system

Thermal lensing effects

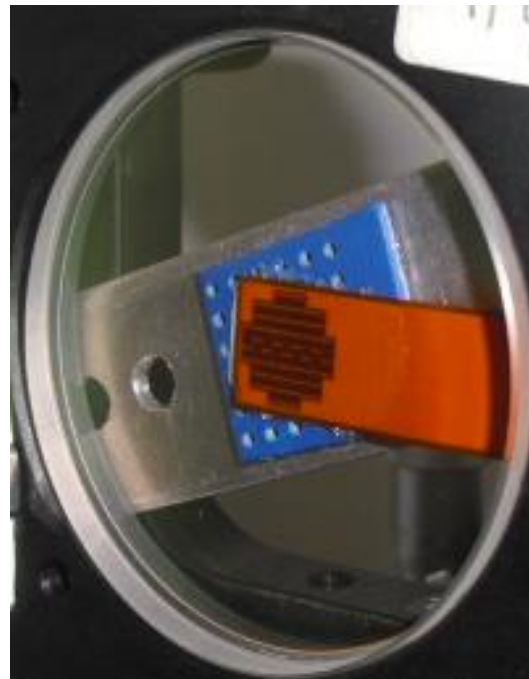
Mismatching onto the  
Output Mode Cleaner<sup>[1]</sup>

→ Need of optimisation of the coupling by **correction of optical aberrations due to thermal lensing in the system**

[1] "Modematching feedback control for interferometers with an output mode cleaner"

N. Smith-Lefebvre, N. Mavalvala, submitted for publication

## First prototype of a Thermally Deformable Mirror (TDM)



**Local temperature control of the substrate**

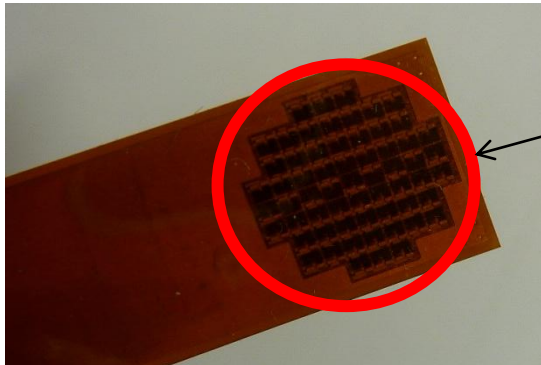
Modification of the optical path length (OPL) according to<sup>[2]</sup>:

$$OPL = \int_C \left( \Delta T(s) \left[ \frac{dn}{dT} + \alpha_T(1 + \nu)n \right] + n \right) ds$$

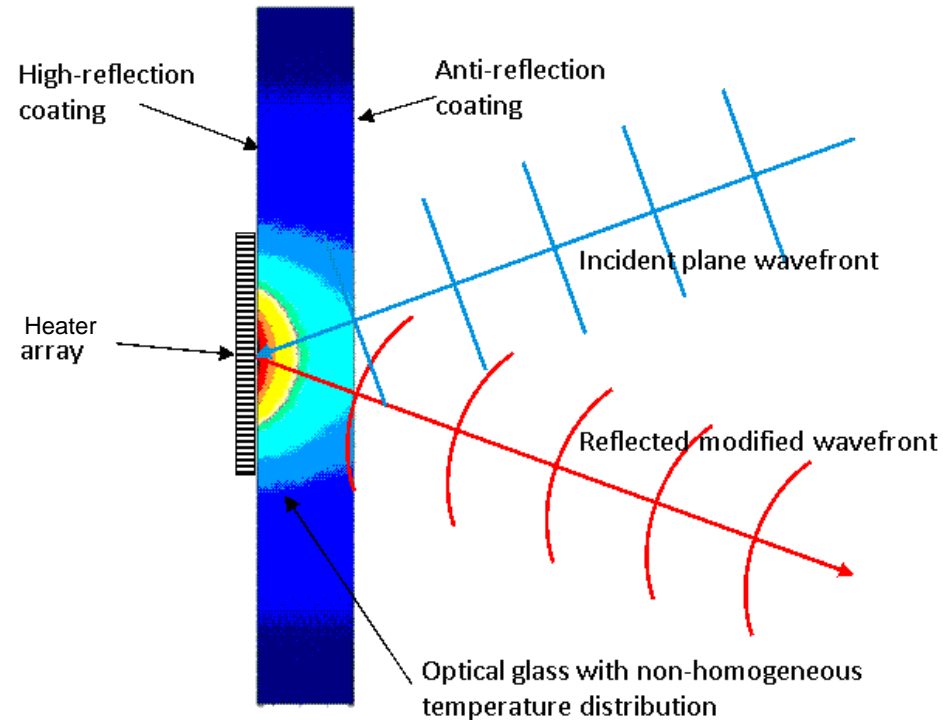
Temperature local increase

Thermo-optic coefficient

Thermo-elastic coefficient



Array of 61 independently controlled actuators



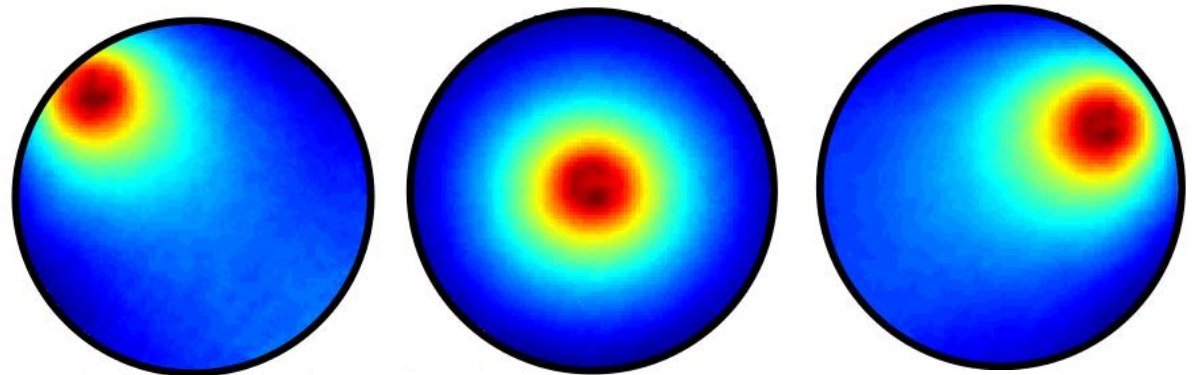
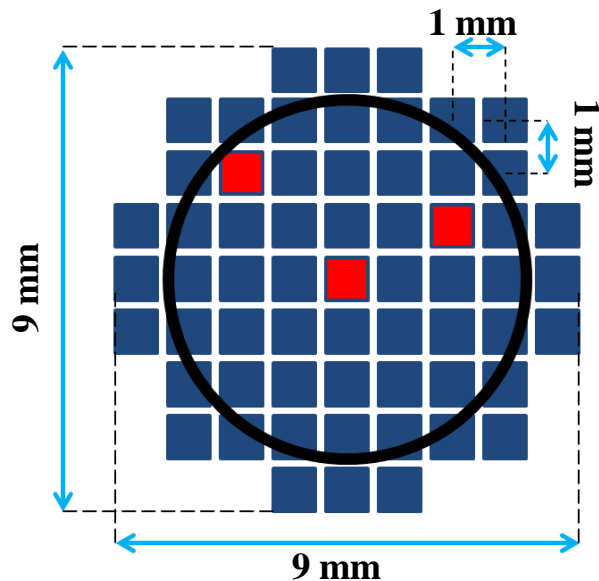
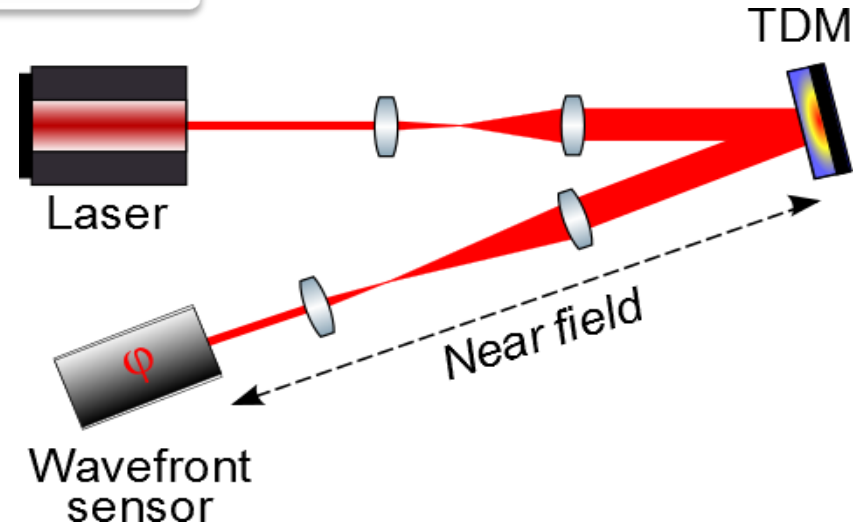
**Thermally deformable mirror**

[2] "Wavefront aberration compensation with thermally deformable mirror"

B Canuel et al 2012 *Class. Quantum Grav.* **29** 085012

## In-air experiment

- Laser beam @ 1064 nm
- Fused silica standard dielectric mirror 2"
- Resistors in contact with the HR coating of the mirror
- Phase measurement with a wavefront sensor (abs. accuracy rms  $\lambda/100$ )

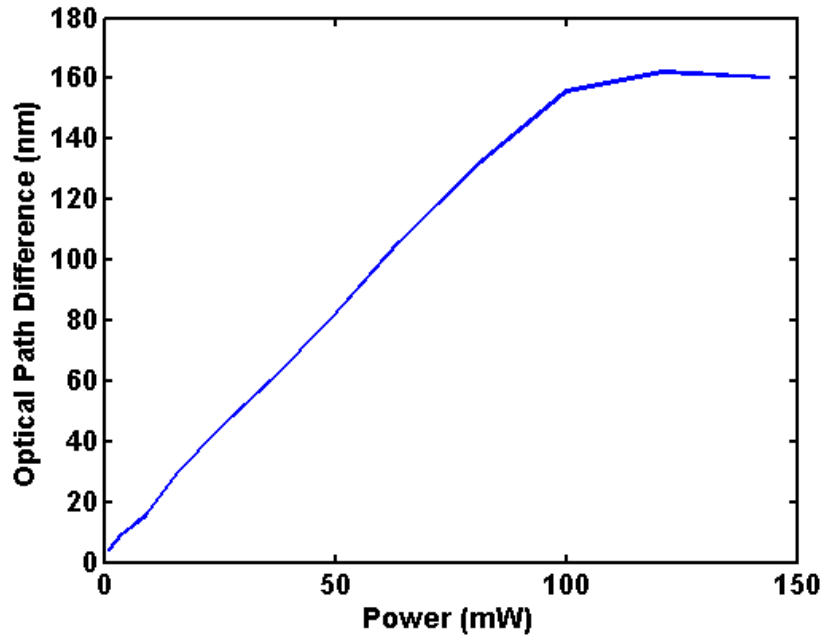


Experimental phase images

➔ Local control of the wavefront by resistor actuation

## Mirror response

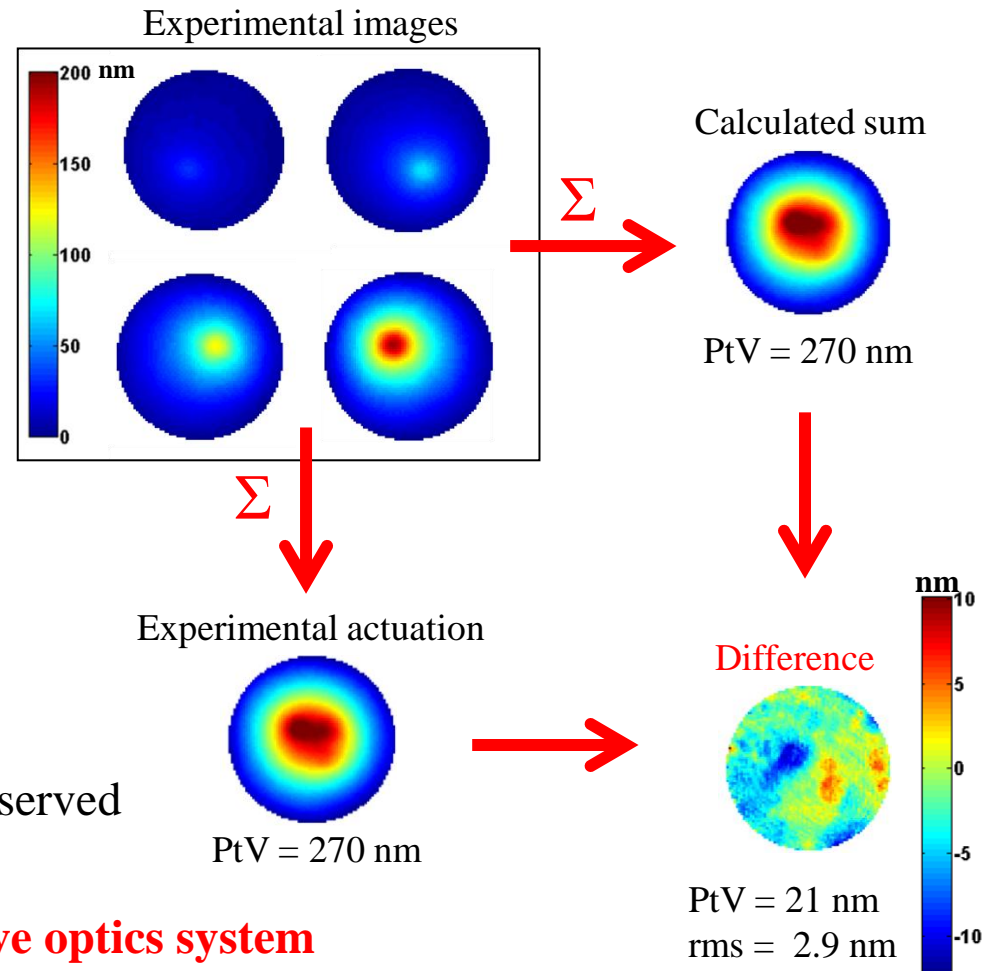
### Linearity with power



Time response of a few seconds :  
time constant  $\sim 4$ s and no hysteresis observed

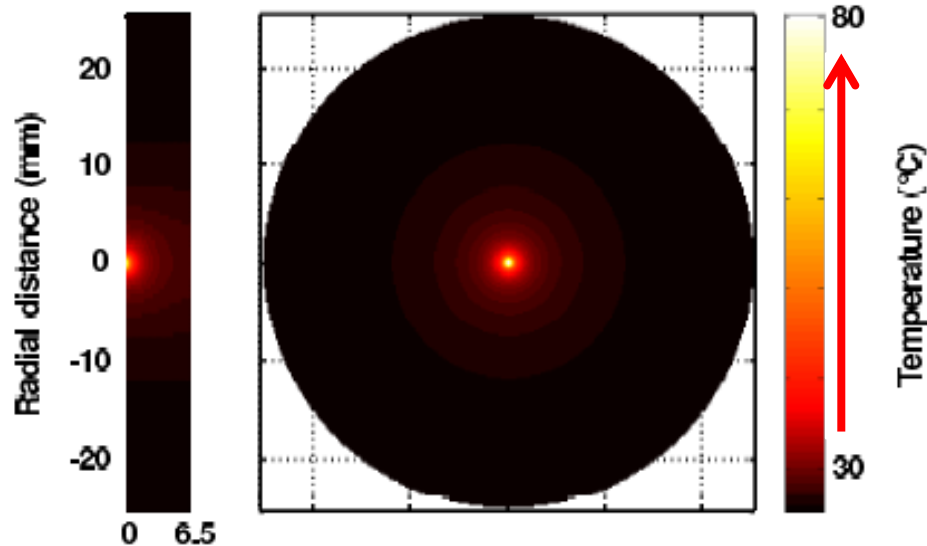
**→ Possible use of the TDM as an adaptive optics system**

### Verification of the superposition principle



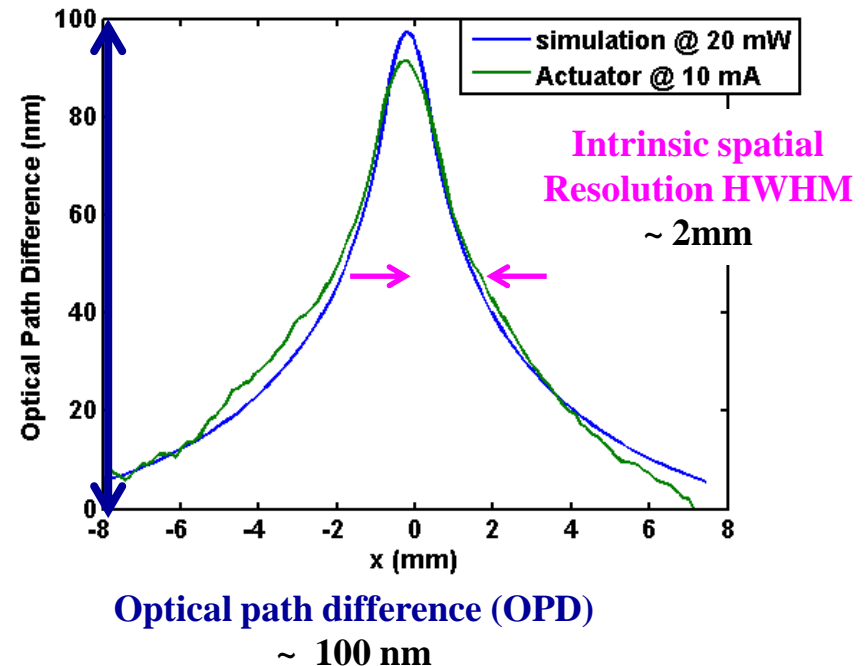
## Simulations by Finite Element Analysis

- Temperature diffusion in the mirror substrate for a heating surface of 1 mm<sup>2</sup>



Temperature profile for 100 mW actuation

- Comparison of the OPD between simulation and experiment



➔ **Good agreement with experimental results : possibility of modeling an ideal TDM**



# How to perform correction of low-order aberrations

## How to find the actuator values

Distorted  
wavefront  
 $\omega_{distorted}$

Wavefront  
Sensor

Computation of  
the correction

TDM

Corrected  
wavefront  
 $\omega_{correction}$

Open control loop in  
adaptive optics

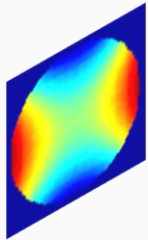
$$\omega_{correction} = -\omega_{distorted}$$

Use of the influence functions

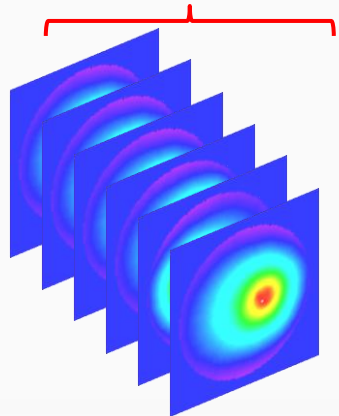
Distorted  
wavefront

Interaction Matrix  
61 actuators x Zernike coefficients

61 actuation  
values



=



X



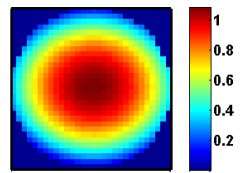
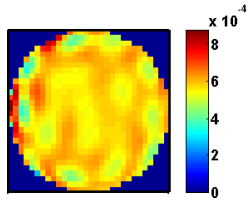
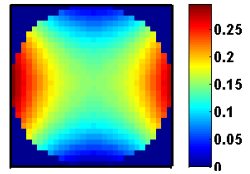
$$actuation\ values = (Interaction\ Matrix)^{-1} \cdot \omega_{correction}$$

→ Easy and fast calculation for correction of large number of Zernike modes

## Correction parameters

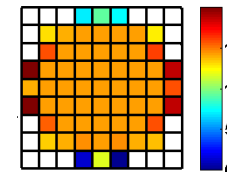
➤ **Zernike polynomials**  
orthogonal basis to describe  
the aberrations in spherical geometry

➤ Performance described by :



- **Dynamic range**

PtV amplitude of the zernike mode limited  
by the maximum value of actuation →

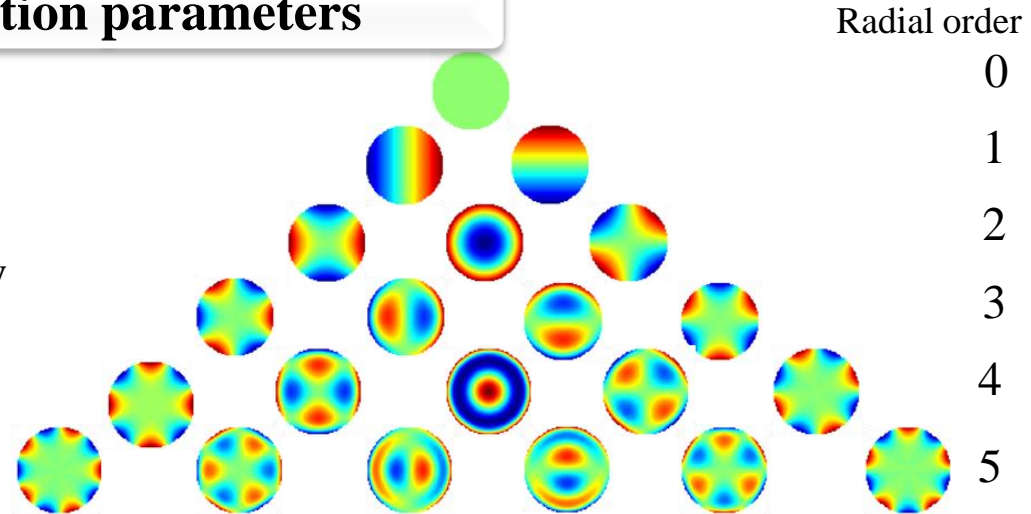


- **Residual error**

rms value of the residual error limited by the footprint of the actuators

- **Induced focus**

unwanted focus generated by this type of actuators, has to be removed

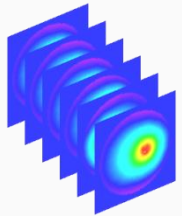


➔ **Characterisation of the TDM performance by ability to produce Zernike modes**

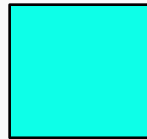
## Eigen modes of the mirror

### Singular Value Decomposition

Interaction Matrix

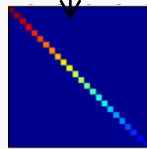


=

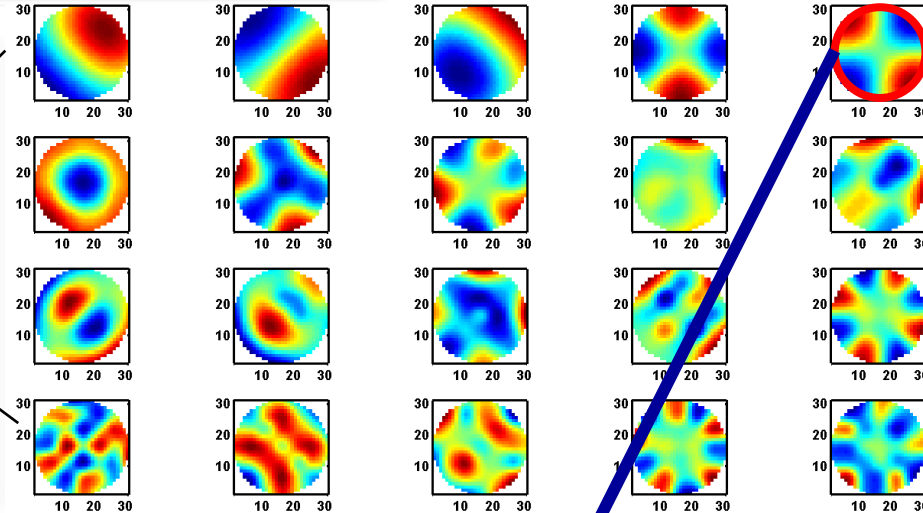


Base of  
command modes

Eigen values

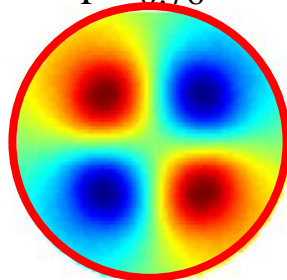


Base of mirror  
deformation modes

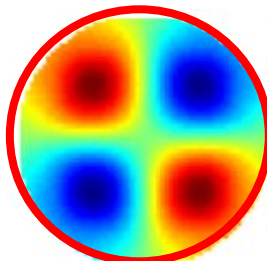


- Comparison of each eigen mode with the corresponding Zernike
  - **Purity** = Indication of the ease to reproduce the Zernike mode

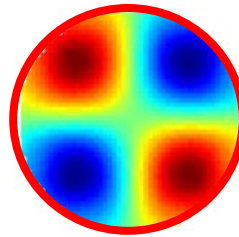
$\varnothing = 14$  mm  
P = 0.76



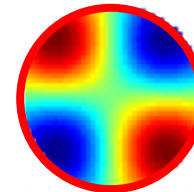
$\varnothing = 12$  mm  
P = 0.82



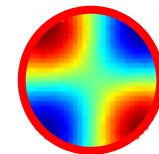
$\varnothing = 10$  mm  
P = 0.87



$\varnothing = 8$  mm  
P = 0.91

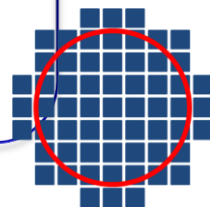


$\varnothing = 6$  mm  
P = 0.88



Example  
with mode 5

➔ Choice of the pupil size according to the maximum value of the purity



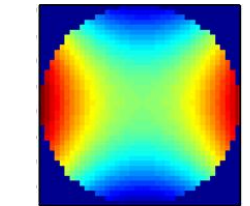
# TDM performances

## Closed-loop on first Zernike modes

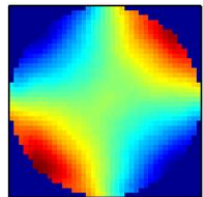
### Command

### Experiment

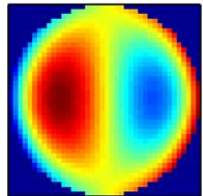
### Simulation of ideal TDM



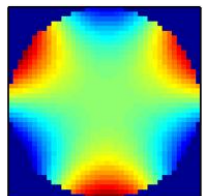
PtV = 0.130  $\mu\text{m}$



PtV = 0.140  $\mu\text{m}$

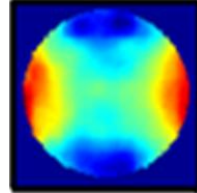


PtV = 0.106  $\mu\text{m}$

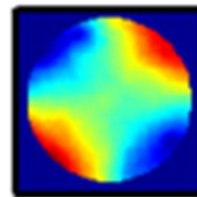


PtV = 0.106  $\mu\text{m}$

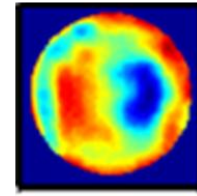
### Correction image



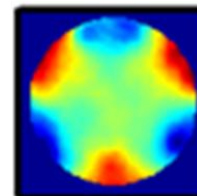
PtV = 0.136  $\mu\text{m}$



PtV = 0.142  $\mu\text{m}$

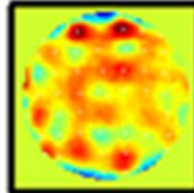


PtV = 0.072  $\mu\text{m}$

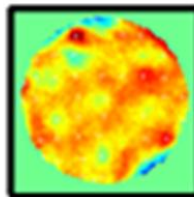


PtV = 0.099  $\mu\text{m}$

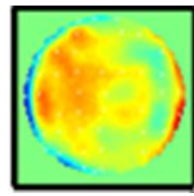
### Residual error



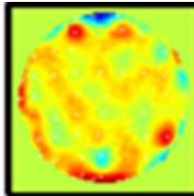
rms = 4.4 nm



rms = 3.2 nm

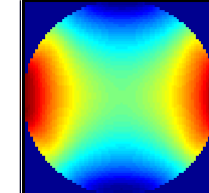


rms = 12 nm

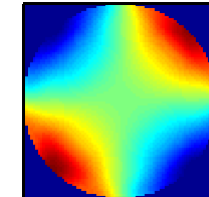


rms = 4.3 nm

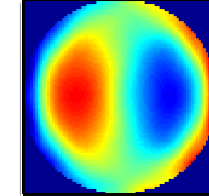
### Correction image



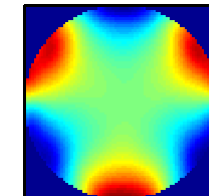
PtV = 0.130  $\mu\text{m}$



PtV = 0.140  $\mu\text{m}$

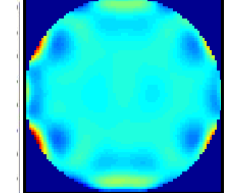


PtV = 0.106  $\mu\text{m}$

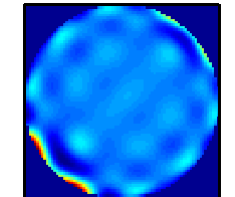


PtV = 0.106  $\mu\text{m}$

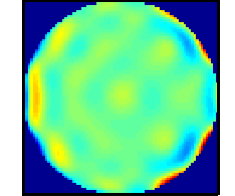
### Residual error



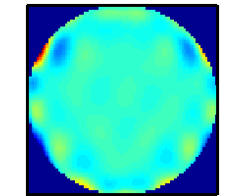
rms = 1.1 nm



rms = 1.6 nm



rms = 2 nm

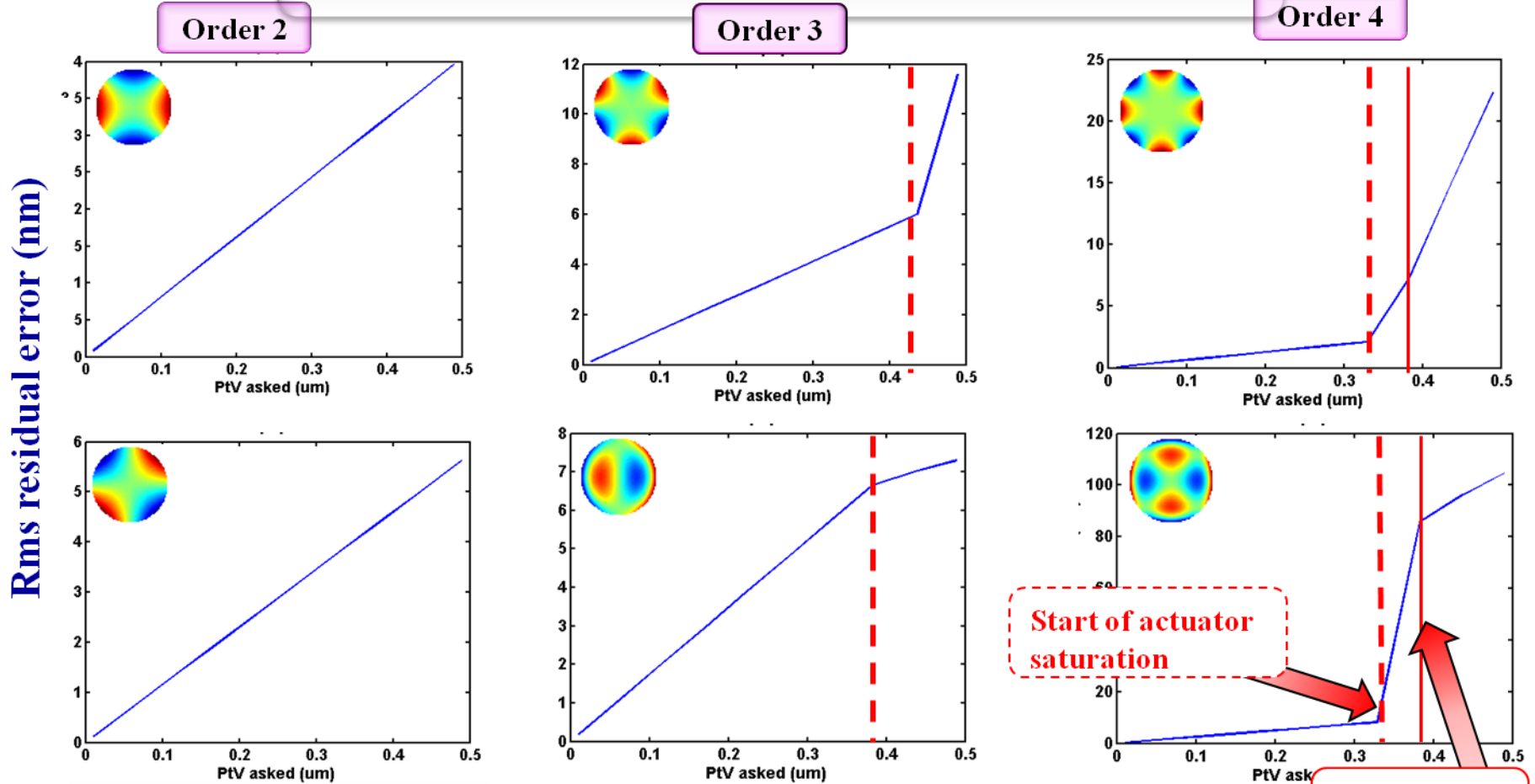


rms = 1.5 nm

**→ Limited by sensor precision and by the spatial non uniformity of actuation**

## Rms value of error vs. Amplitude of correction

### Simulation results

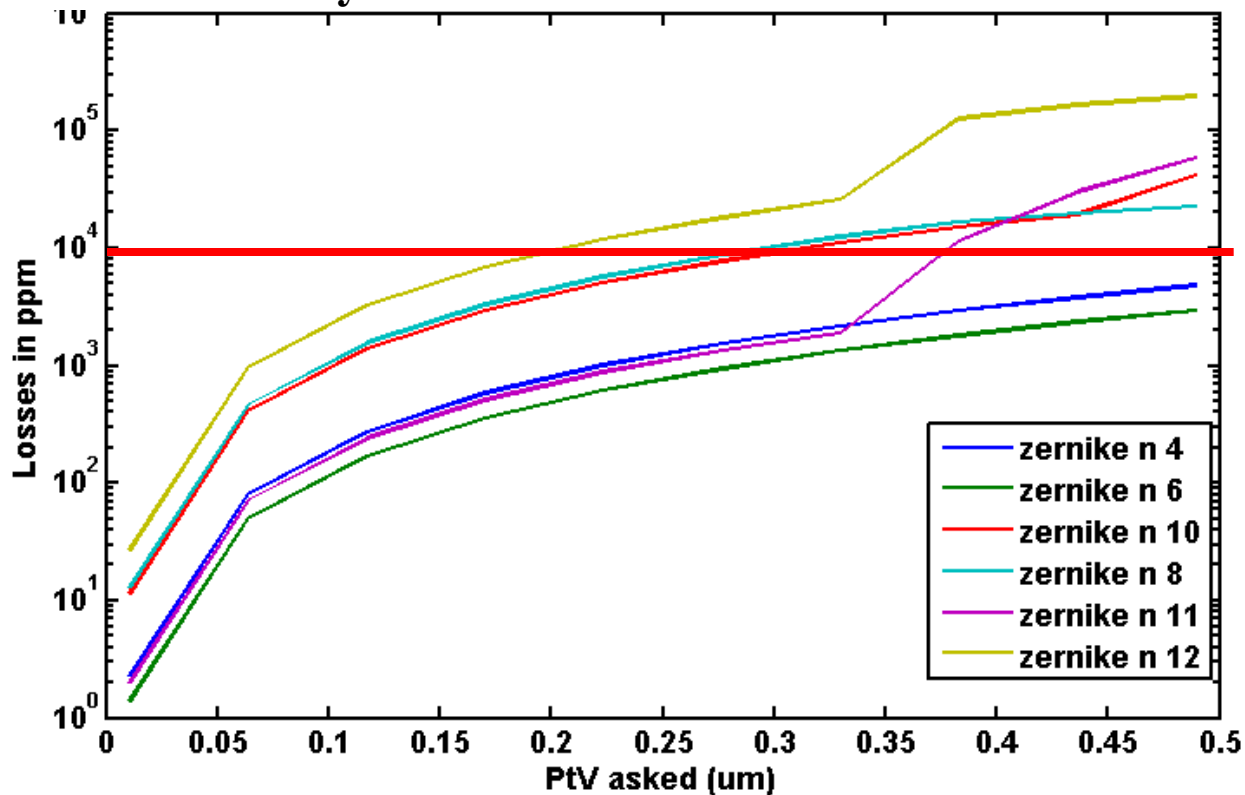


→ Possible amplitude of correction > 0.3 um for Zernike order 4  
 → Value of the focus to remove from infinity to 100 m

## Losses and weighting *Simulation results*

- Matching requirements for the injection system of Advanced Virgo :  
Mode matching  $\geq 99\%$

### Ability to correct an aberrated wavefront



➔ Losses meet the requirements in the dynamic range of the first order aberrations



## Possible improvements

- Improvement of the dynamic range by:
  - Better thermal contact
  - Change substrate material
  - Improvement of power coupling in the mirror substrate
  
- Reduction of the residual rms value by:
  - Increase of actuator density
  - Improvement of homogeneity of the heating pattern

## ➤ **First prototype under characterization**

Innovative device with a lot of great advantages:

- Not limited by electronic noise
- Vacuum compatible
- Low cost and compatible with use of standard mirrors
- Possible correction of first Zernike modes with a good precision

Next steps:      Complete the experimental characterization  
                          Experimental optimisation of cavity matching  
                          Tests under vacuum

## **Possible applications**

- Injection system of Advanced Gravitational Wave Detectors
- Output mode cleaner optimisation of matching
- Optimised mode matching for squeezed light injection system