



# Core Optics related loss hierarchy of aLIGO

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- Introduction
- Loss related to geometry
- Loss related to as-built arms
- Loss related to aberrations
- Loss related to thermal deformations
- Summary

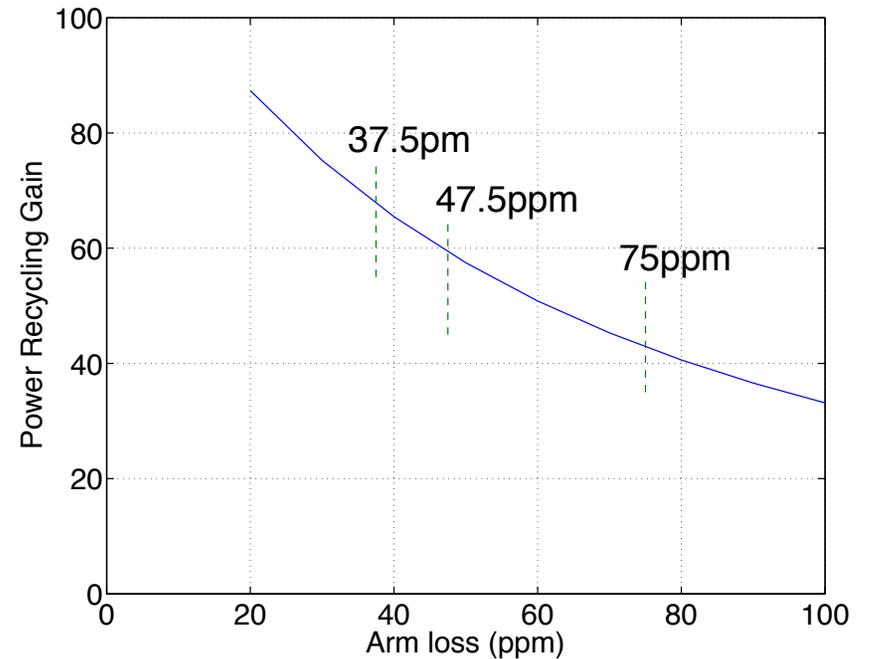
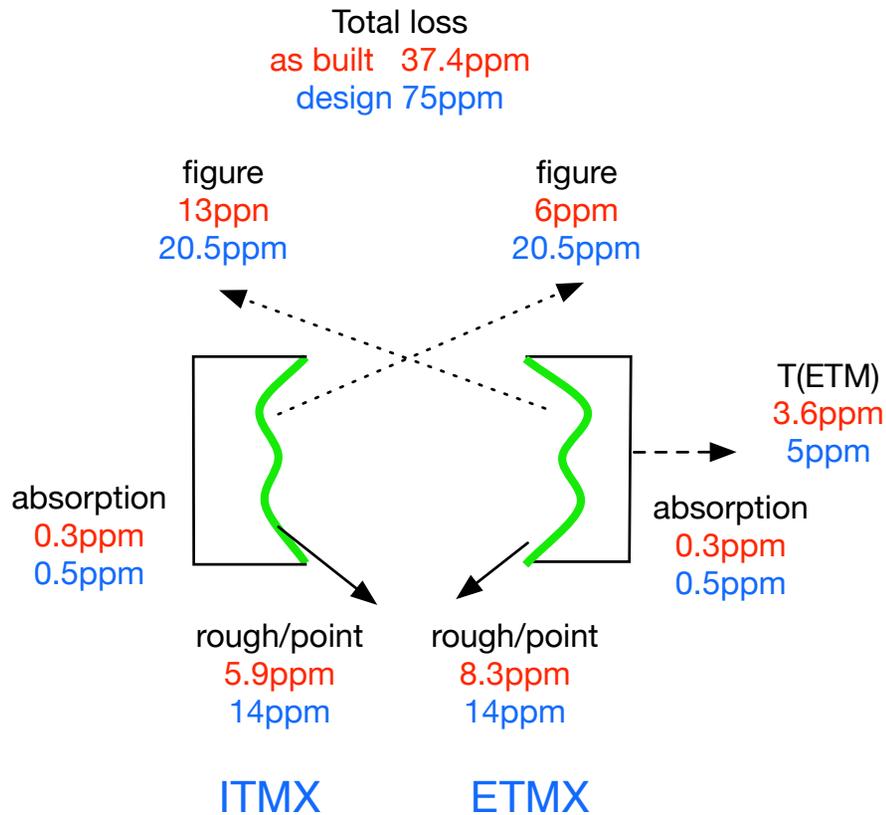




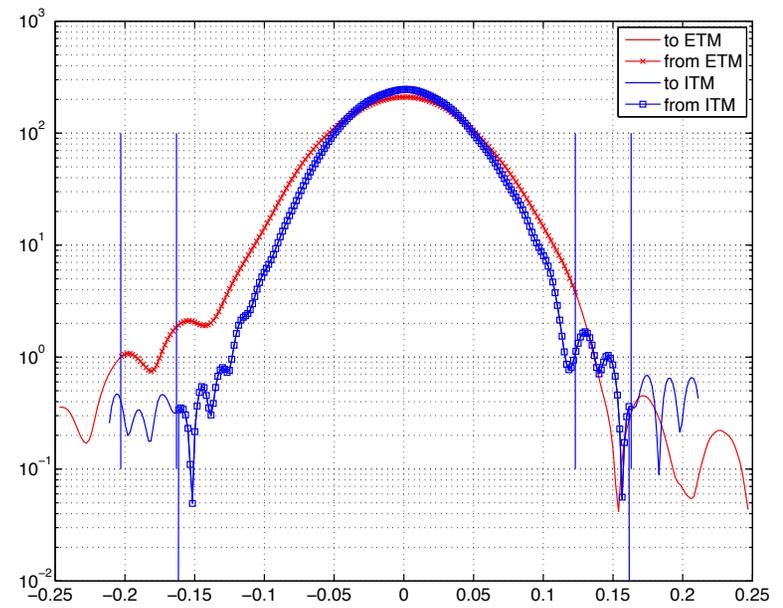
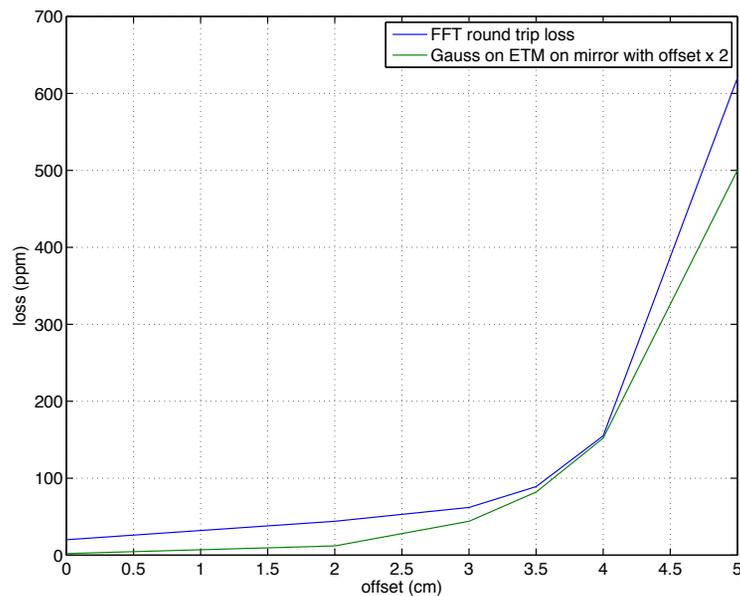
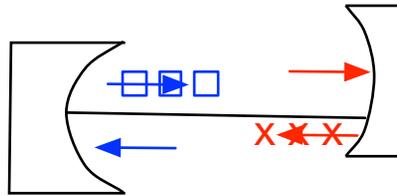
# Arm loss designed vs as-built

Loss in arm : as-built vs design

Power Recycling Gain vs Arm loss



# Loss by offcentering





# Introduction

now that almost all COCs have been delivered and measured

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- Purpose of the talk
  - » Understanding the fundamental limitation by COC
- Optics data
  - » Use as built / measured RoC, maps, losses
  - » <https://galaxy.ligo.caltech.edu/optics/> and links from this URL
- Simulation tool used
  - » FOGPrime13
    - matlab program
  - » Documentations, source codes and data files for LLO and LHO available from DCC-T1300942

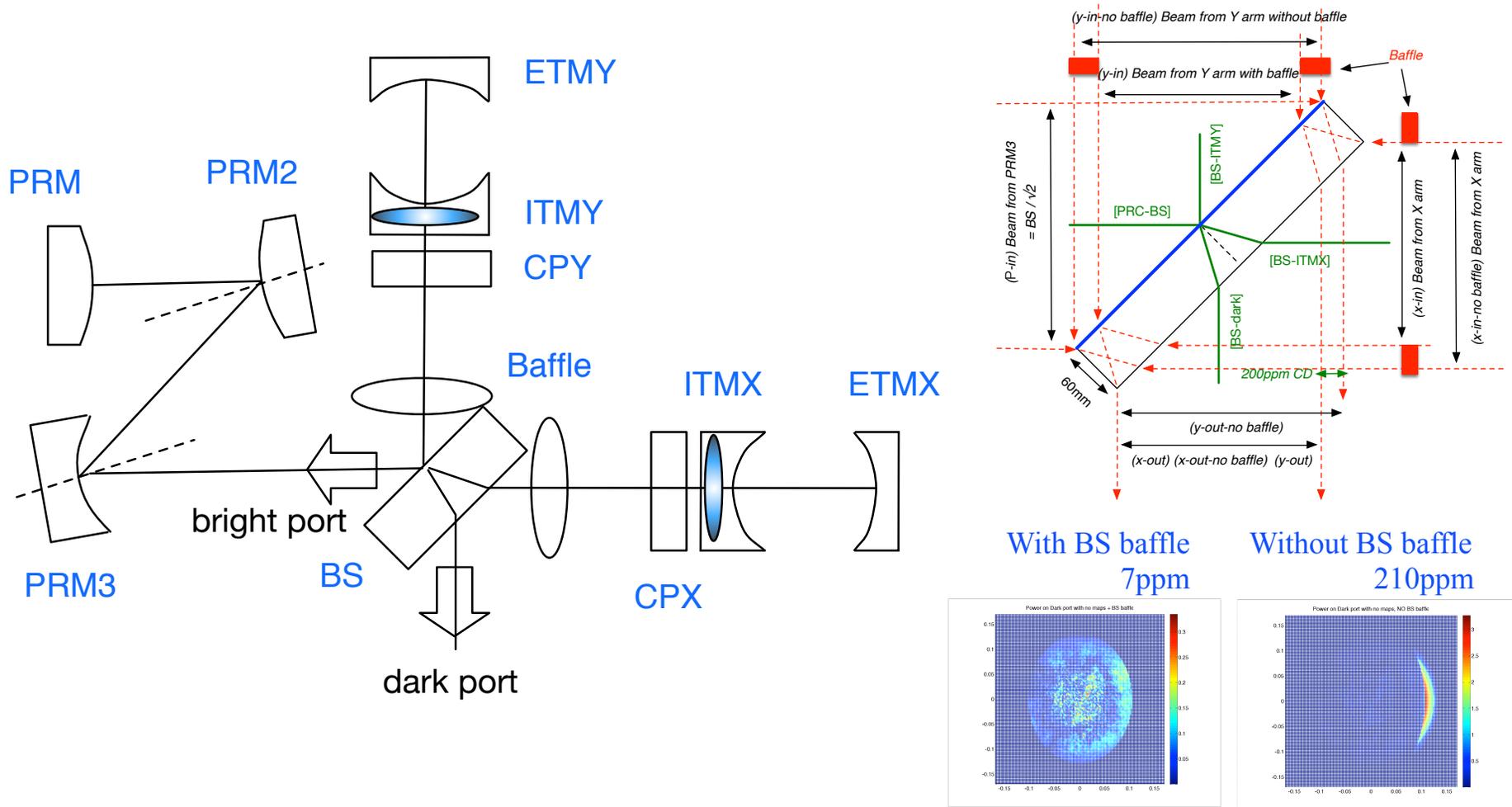


# FOGPrime13

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- FOGPrime13
  - » Objet oriented FFT-based IFO simulation and analysis package on matlab
    - FP to full aLIGO with input and output MCs, transMon
  - » FOGPrime13 = FOG + SIS + e2e + twiddle
    - FOG as the field calculation engine
    - SIS as base of the user interface design and support package
    - e2e as base of the object oriented package infrastructure
    - twiddle for setting the initial condition of fields, especially for coupled cavities
- Based on matlab
  - » Matlab functions, built-in and user provided, can be easily integrated
  - » Can interact with COMSOL, like thermal deformation
- No setting of Wfft and Nfft
  - » User defines optics quantities and resolution of maps

# Loss related to geometry

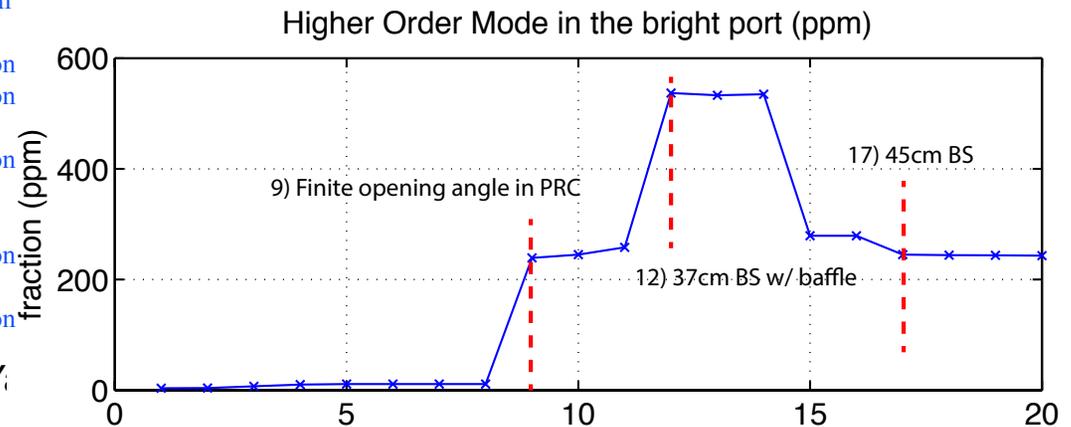
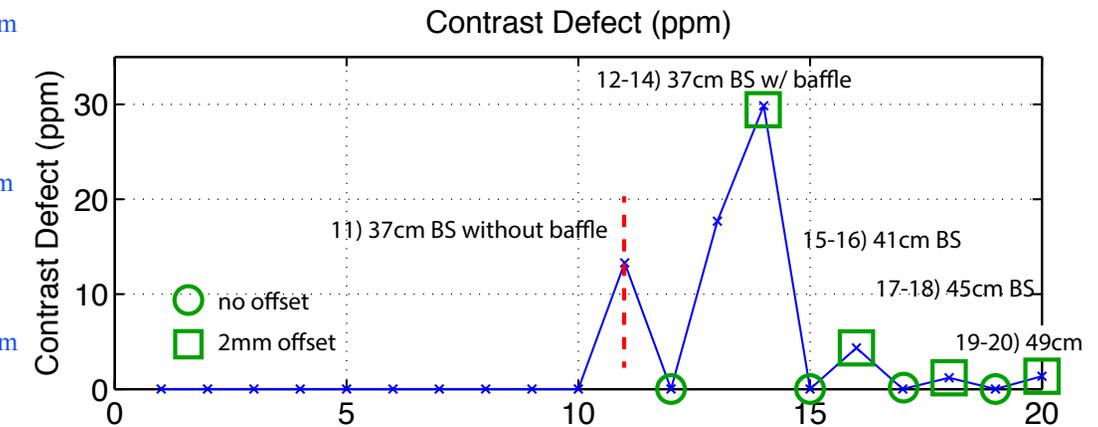
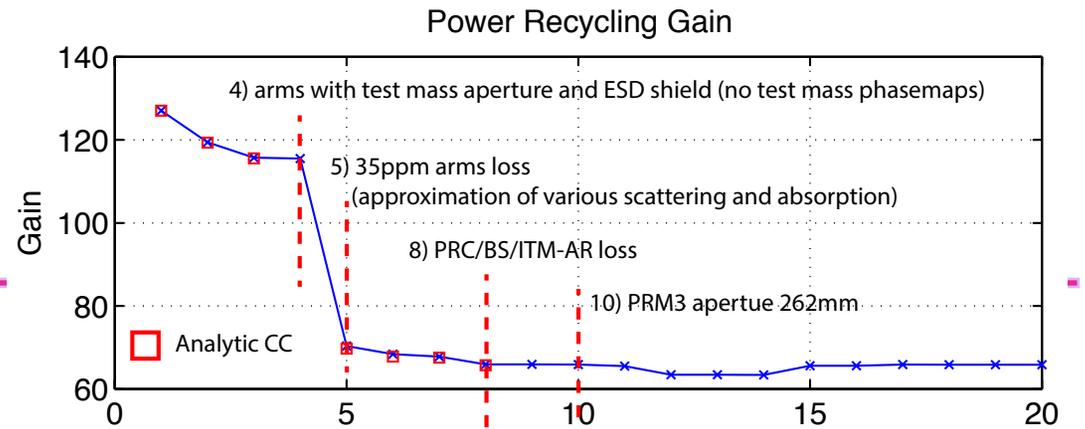




# Performance limitation by design LLO case

## T1400055

- 1) no loss at all, with large mirrors. A finite HOM (3.7ppm) looks a nice gaussian so probably the base mode parameter is slightly off.
- 2) 1) + ETM transmittance 3.7ppm
- 3) 2) + test mass aperture 326mm, round trip loss by the aperture is 1.94ppm (with 340mm, RTL is 0.6ppm)
- 4) 3) + 266mm ESD aperture, placed using BS baffle (266mmx266mm) in front of BS
- 5) 4) + 35ppm arm loss
- 6) 5) + power recycling mirror and beam splitter loss and transmission. Sum of losses + RM2 transmission is 583ppm
- 7) 5) + ITM AR side loss, (ITMX loss 206ppm, ITMY loss 330ppm)
- 8) 5) + 6) and 7), i.e., losses and transmission in the PRC, BS and ITM AR
- 9) 8) + finite opening angles in PRC (0.79° for PRM2 and 0.615° for PRM3). Among the total HOM of 240ppm, major ones are HG(1,0) of 12ppm and HG(0,2) of 210ppm.
- 10) 9) + PRM3 aperture 262mm
- 11) 10) + BS 367.1mm/60mm no baffle
- 12) 11) + BS baffle (210mmx260mm). Total HOM goes up to 540ppm from 260ppm by clipping using BF baffle. The major is HG(4,0) of 170ppm.
- 13) 12) with BS baffle facing to X arm offset by 1mm in horizontal direction
- 14) 12) with BS baffle facing to X arm offset by 2mm in horizontal direction
- 15) 10) + BS 410mm/67mm with BS baffle (237mmx260mm)
- 16) 15) with BS baffle facing to X arm offset by 2mm in horizontal direction
- 17) 10) + BS 450mm/73.5mm with BS baffle (260mmx260mm) : no performance impact by the BS baffle
- 18) 17) with BS baffle facing to X arm offset by 2mm in horizontal direction
- 19) 10) + BS 490mm/80mm with BS baffle (260mmx260mm)
- 20) 19) with BS baffle facing to X arm offset by 2mm in horizontal direction





# Arm performance

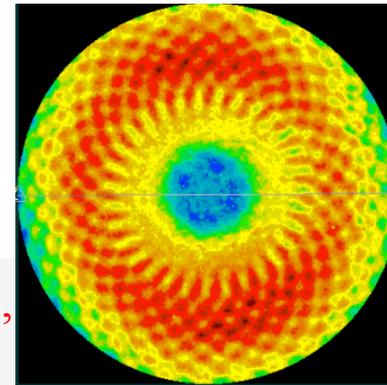
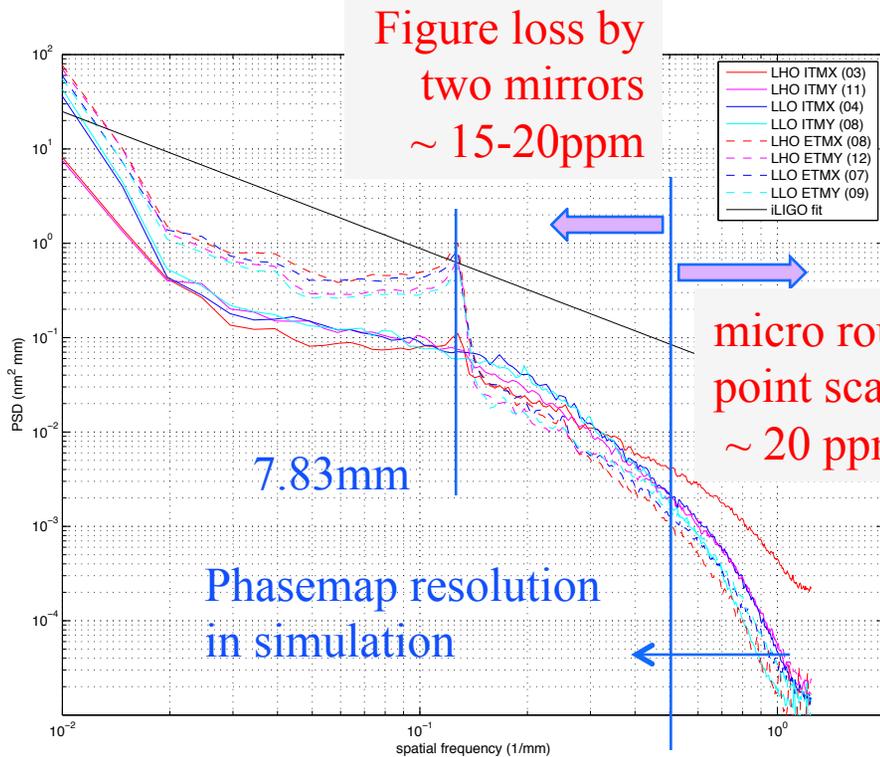
## only aberrations in arms included

- Low arm loss (70 ppm design to 35-50 ppm expected)
- High power recycling gain and high arm power
- High ( $\sim 0.15$ ) reflected power
- High higher order mode content in the bright port

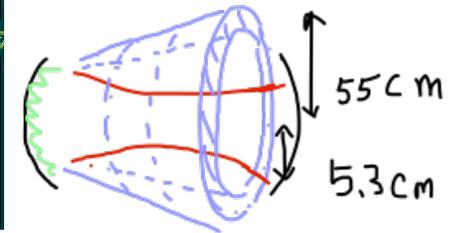
	LHO TITM=1.39%,1.42%	LLO TITM=1.48%,1.48%	LLO (no maps)
CD	29 ppm	48 ppm	44 ppm
PRG	63	61	74
Arm power	8800 W (1W input)	8100	9900
HOM in bright	1900	1600	520
HOM in x/y arm	95 / 114 ppm	97 / 113	38 / 62
Round trip loss	33 / 37 ppm	40 / 38	23 / 26



# Noise injection by the spiral pattern on test mass coatings

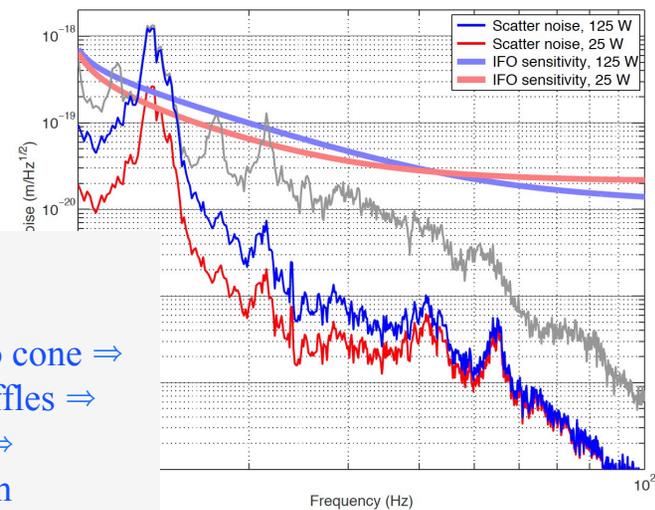


ETM07 map

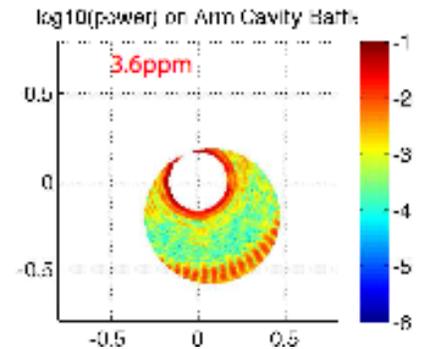
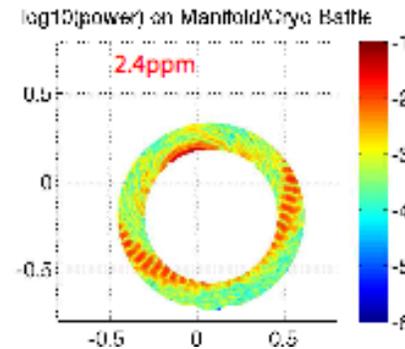
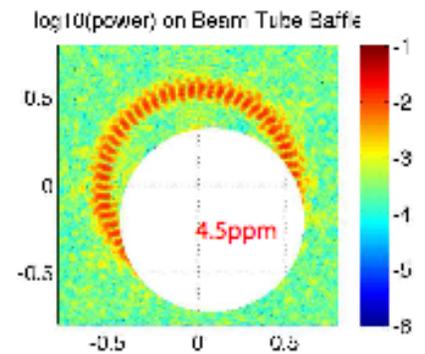
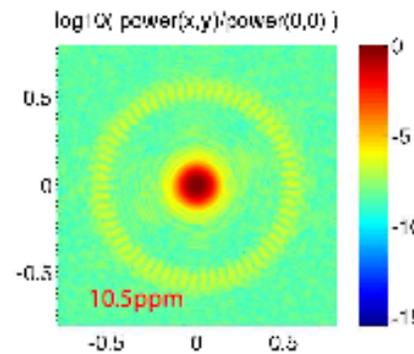
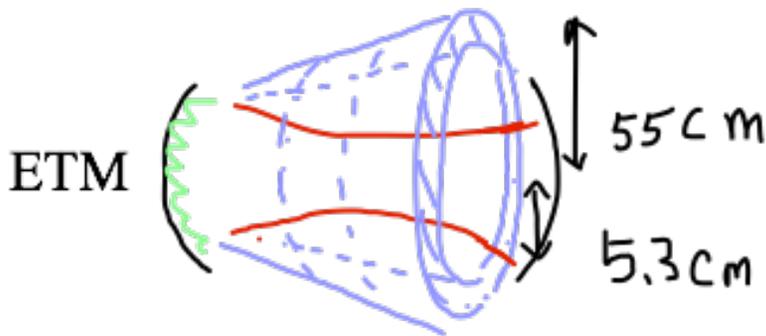
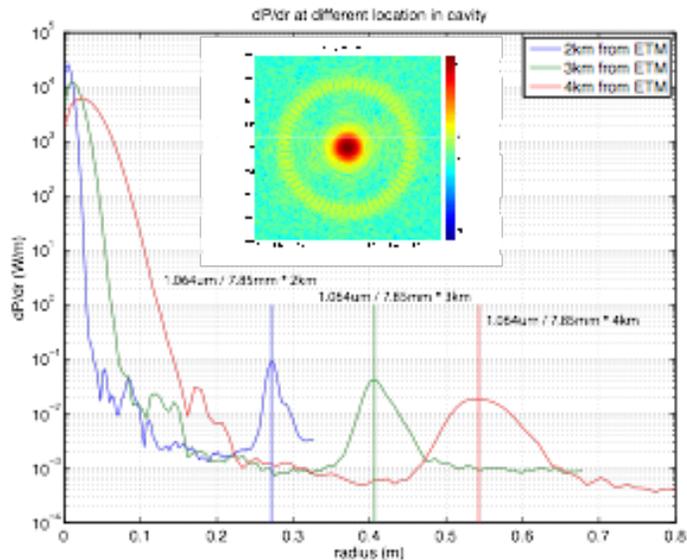


main beam ⇒  
 ETM reflection ⇒  
 larger angle scattering into cone ⇒  
 reflected by beam tube baffles ⇒  
 back scattered into ETM ⇒  
 merged into the main beam

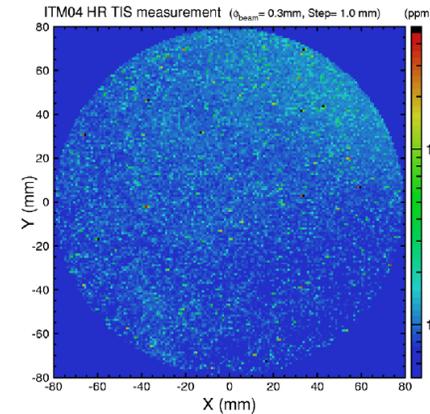
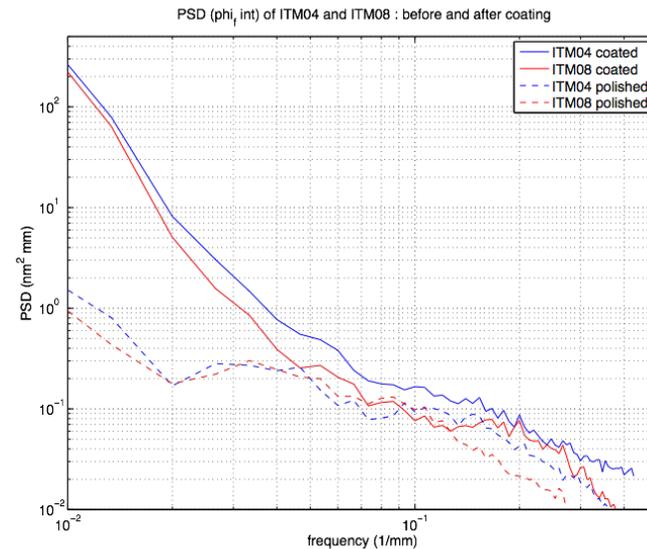
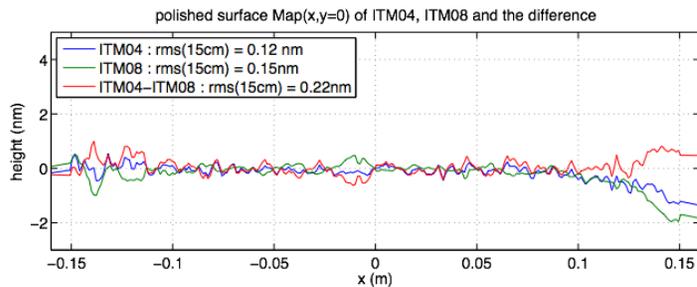
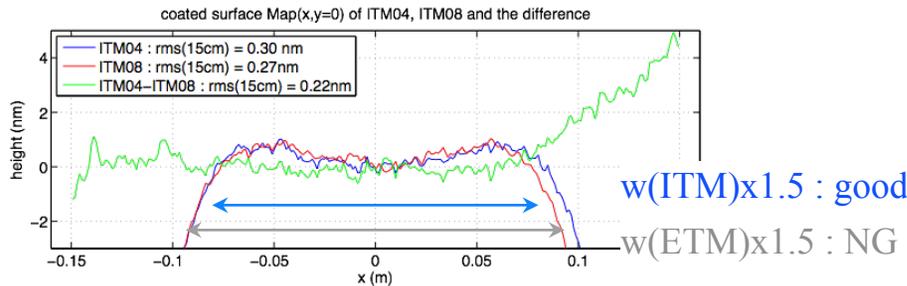
T1300354 by PF, HY



# Scattered light ring pattern



# Higher order mode due to imperfect test mass coating figures

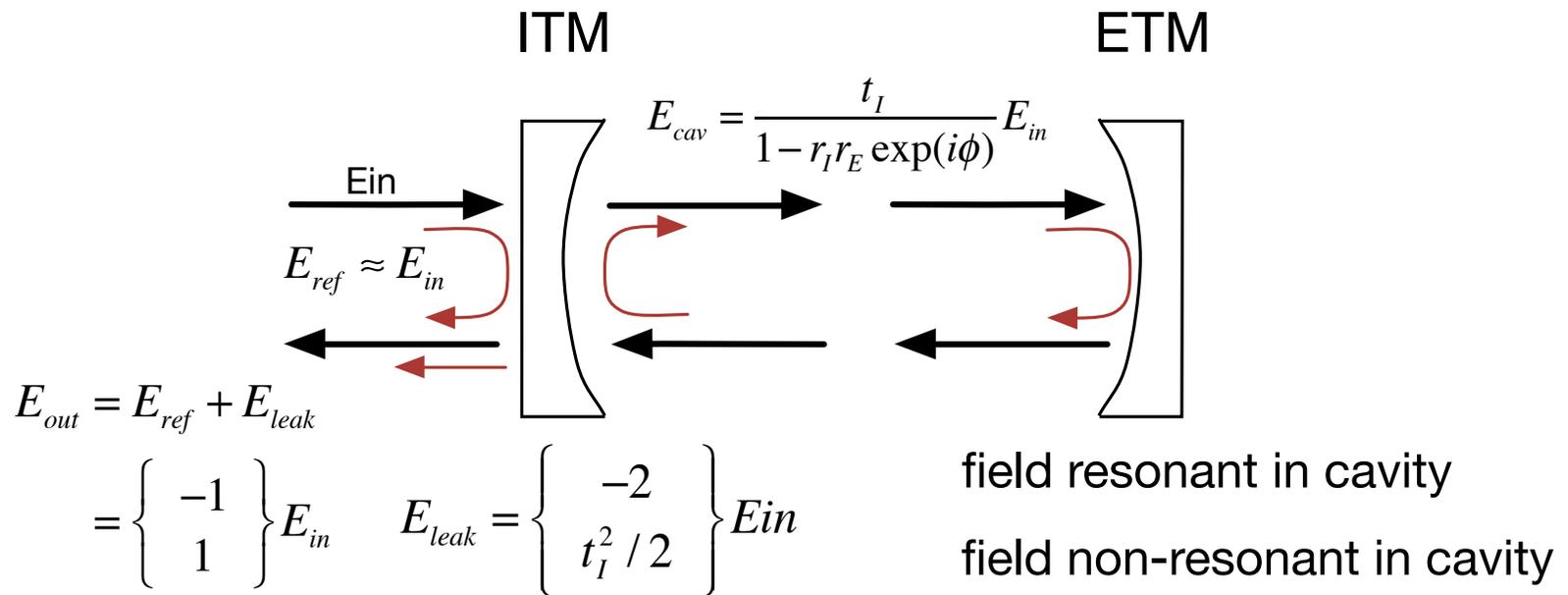


Caltech : 10ppm  
LMA : 4.5ppm

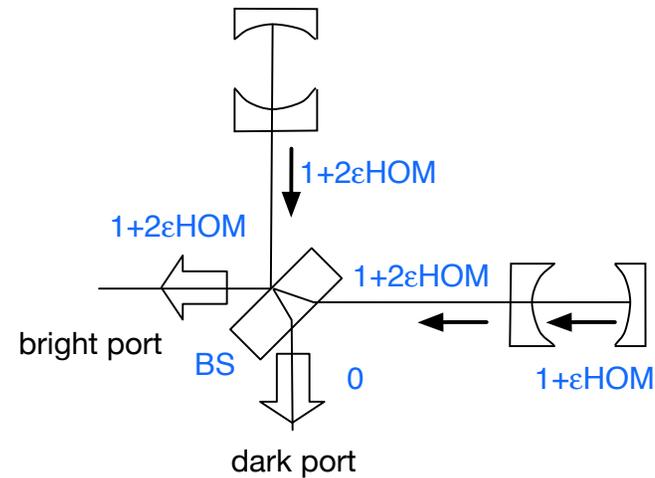
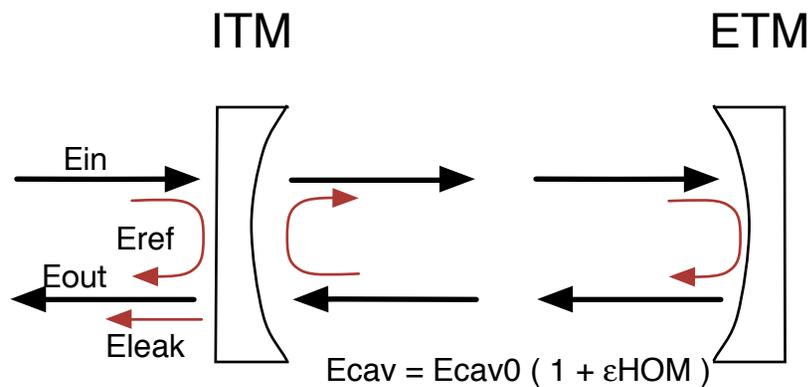
		Round trip loss (ppm)	Non 00 mode in cavity (ppm)	LG20 mode in cavity (ppm)
polished	ITM04	2.9	3.2	0
	ITM08	3.0	3.5	0
coated	ITM04	2.7	8.8	2.8
	ITM08	3.0	9.0	4.9

Table 1 Cavity quality factors

# The sign flip basic



# HOM amplification



$$E_{ref} = E_{in}$$

$$E_{leak} = -2E_{in}(1 + \epsilon HOM)$$

$$E_{out} = -E_{in}(1 + 2\epsilon HOM)$$

$$HOM(\text{arm}) = \epsilon HOM^2$$

$$HOM(\text{bright}) = 4\epsilon HOM^2$$

$$HOM(\text{dark}) = 0$$

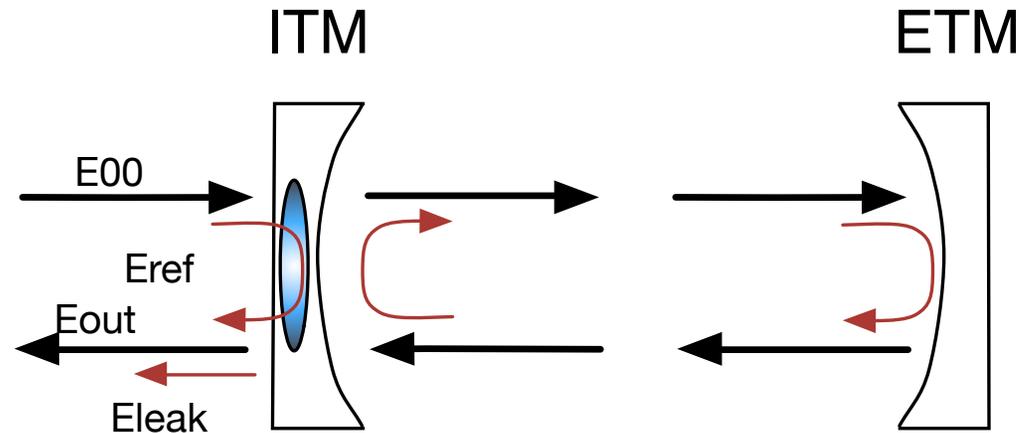
## Higher order mode power fraction (H1)

	ITMX	ITMY	BS bright
LG10	26	43	83
LG20	40	38	890
LG30	7.8	9.9	47

# ITM lens

## some sees, some not

- CR ( $E_{out}$ ) : don't see
- SB ( $E_{ref}$ ) : see
- Signal SB ( $E_{leak}$ ) : see

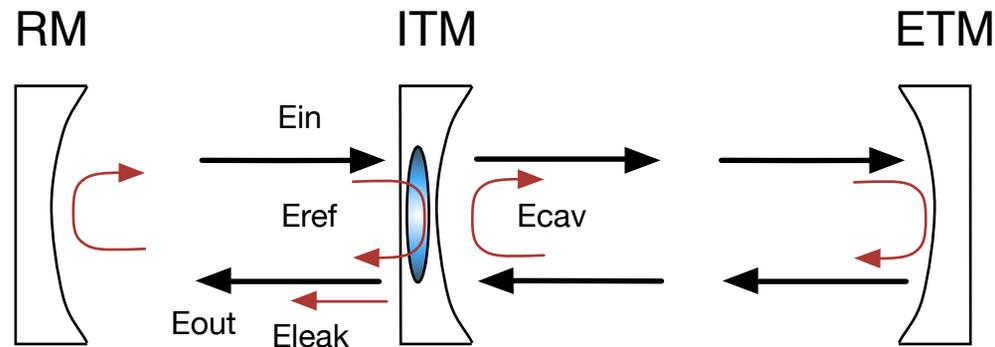


$$E_{ref} \approx \exp(i2\phi)E_{00}$$

$$E_{leak} = \exp(i\phi) \begin{Bmatrix} -2 \\ 0 \end{Bmatrix} E_{in}$$

$$E_{tot} = \begin{Bmatrix} \exp(2i\phi) \\ \exp(i2\phi) \end{Bmatrix} E_{00} + \begin{Bmatrix} -2\exp(i\phi) \\ 0 \end{Bmatrix} E_{00} \approx \begin{Bmatrix} -1 + O(\phi^2) \\ 1 + i2\phi \end{Bmatrix} E_{00}$$

# Cavity mode



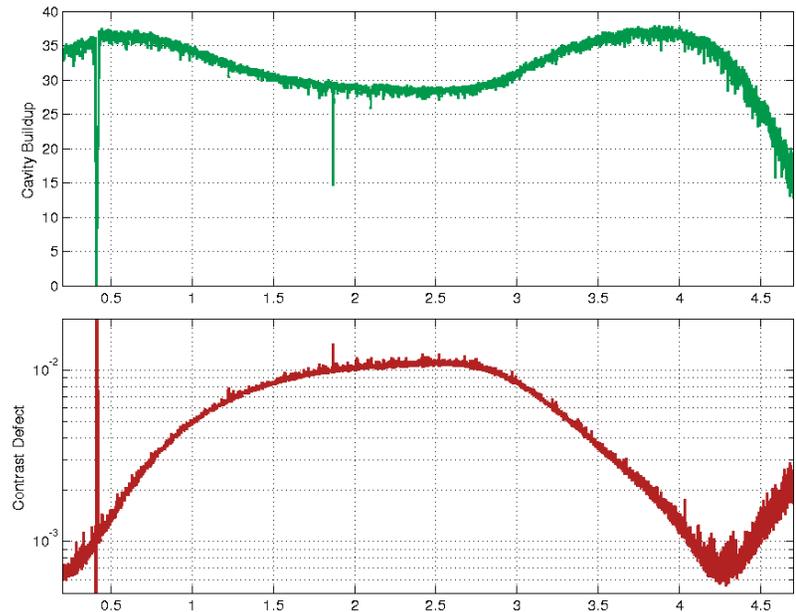
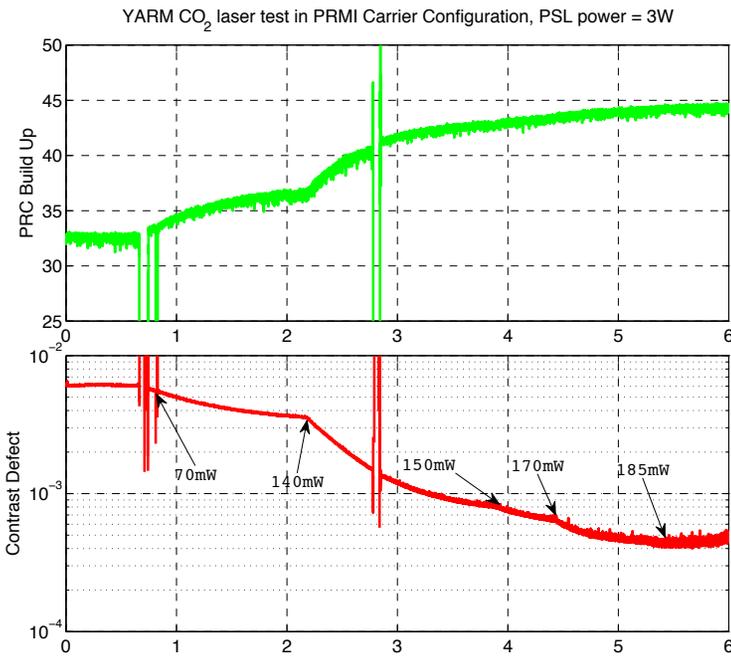
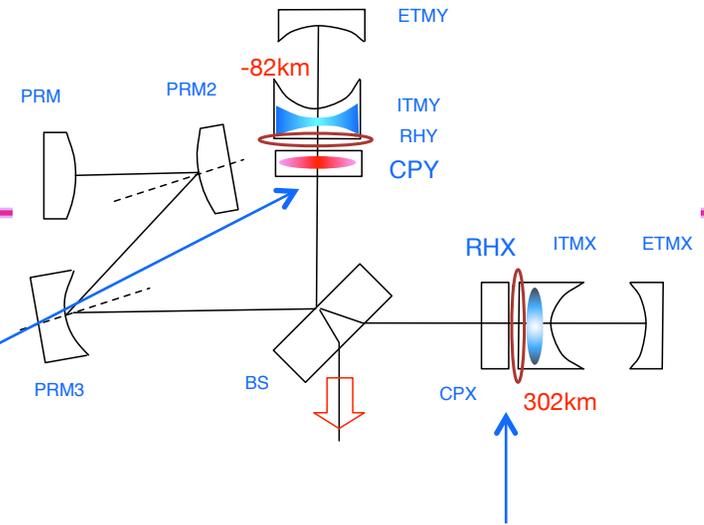
- Recycling cavity mode is defined by RM HR reflection and ITM reflection,  $E_{in}$  to  $E_{out}$ , not  $E_{in}$  to  $E_{ref}$ , just the same as length DOF case
- Optimal coupling is  $mode(E_{ref}) = mode(E_{leak})$ , which makes  $mode(CR \text{ in } RC) = mode(SB \text{ in } RC)$
- When thermal lens changes,  $mode(CR \text{ in } RC)$  does not change in the first order, but the  $mode(SB \text{ in } RC)$  changes in the first order



# TCS corrections for LLO PRMI

RH optimal lens =  $n(\text{SiO}_2) \times 82\text{km} = 1/0.84 \times 10^{-5}$

CP optimal lens =  $82\text{km} = 1/1.22 \times 10^{-5}$

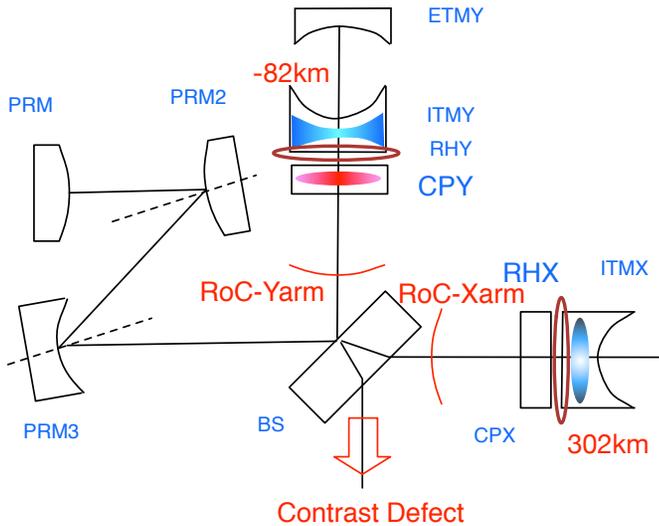
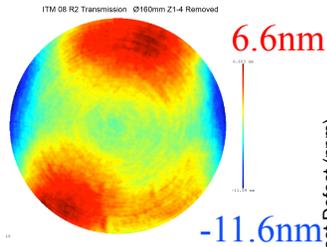


log11140 CD~400ppm, PRG~45

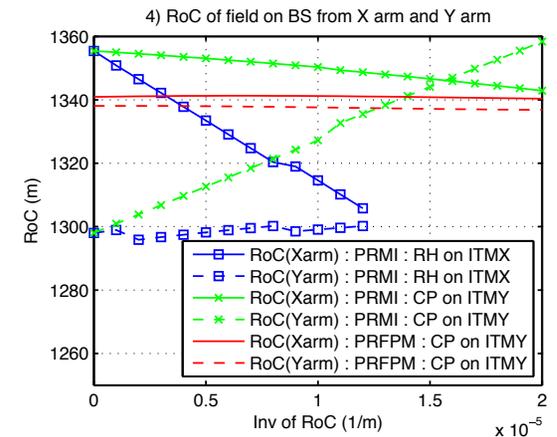
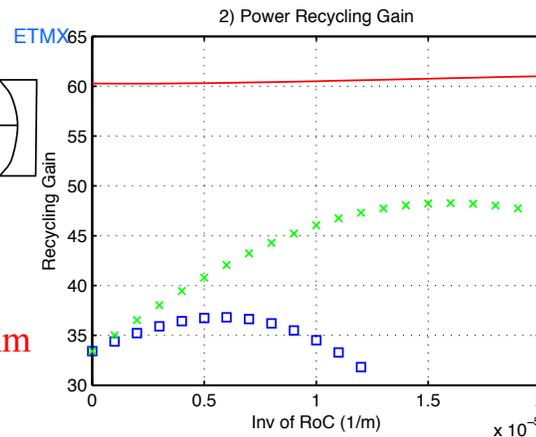
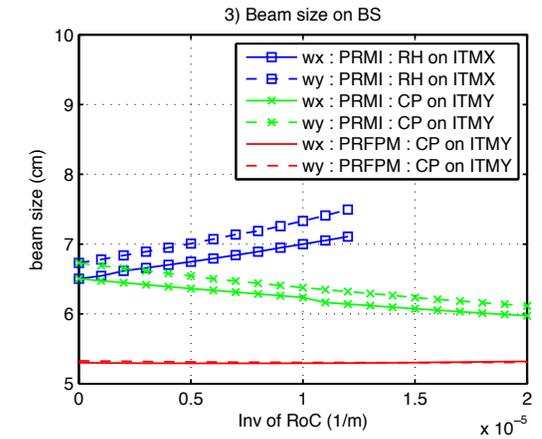
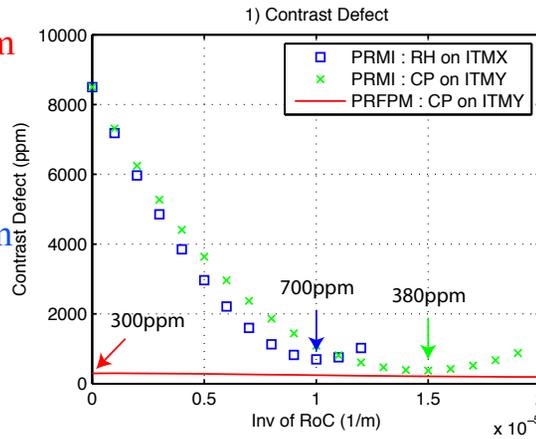
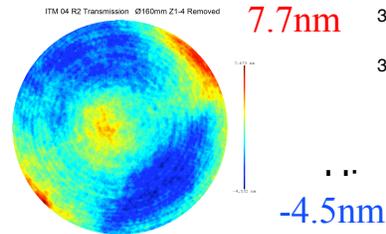
log#9733 CD~600ppm, PRG~35

# (In)Sensitivity on ITM SPTWE + CP lens

ITM08 / ITMY  
transmission  
map in 160mm  
w/o power



ITM04 / ITMX



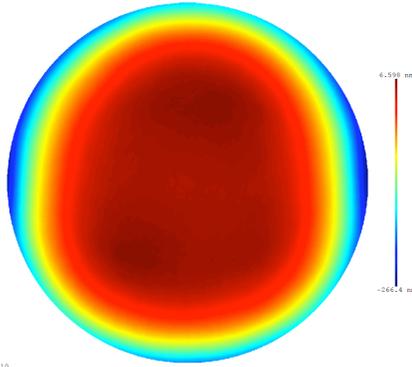


# ITM transmission maps not the large lens effect imbalance

### ITM08 / ITMY

ITM 08 R2 Transmission Ø300mm Z1-4 Removed Fit Over Ø160mm

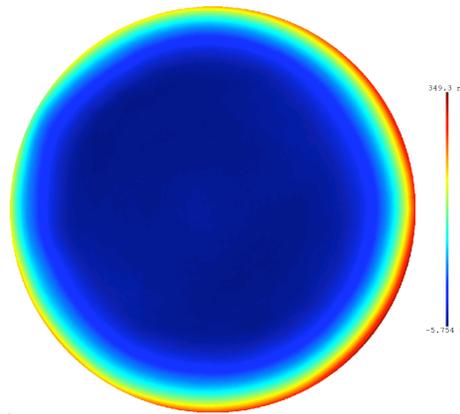
$\phi=300\text{mm}$



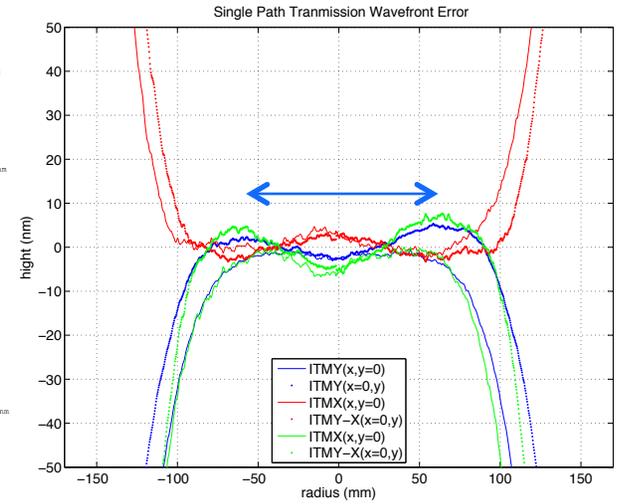
1010

### ITM04 / ITMX

ITM 04 R2 Transmission Ø300mm Z1-4 Removed Fit Over Ø160mm

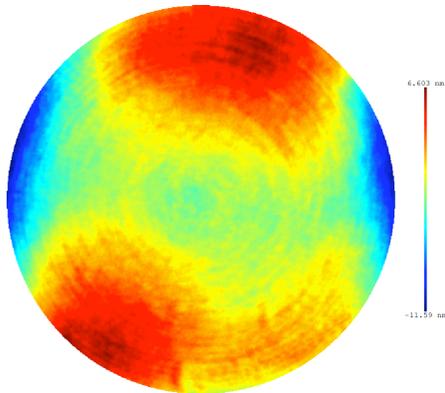


2010



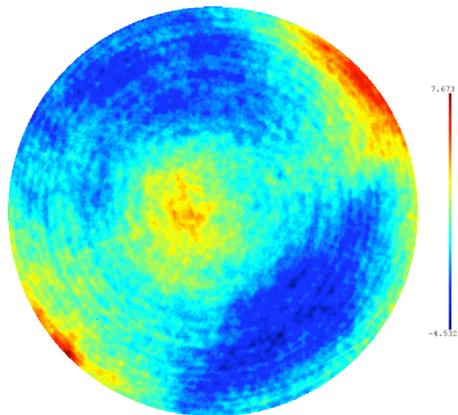
ITM 08 R2 Transmission Ø160mm Z1-4 Removed

$\phi=160\text{mm}$



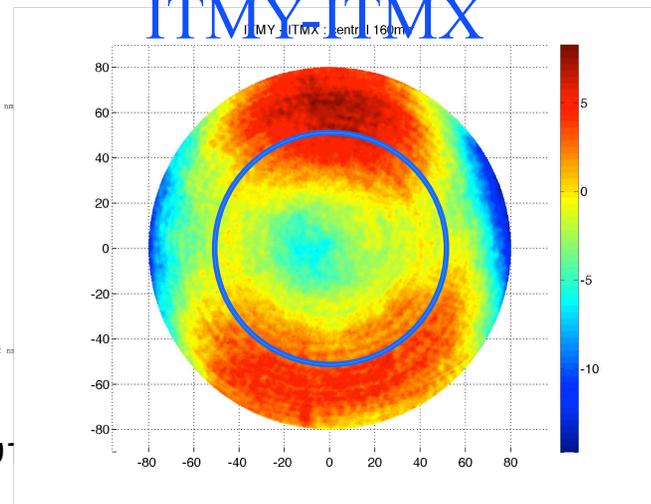
10

ITM 04 R2 Transmission Ø160mm Z1-4 Removed



010

### ITMY-ITMX

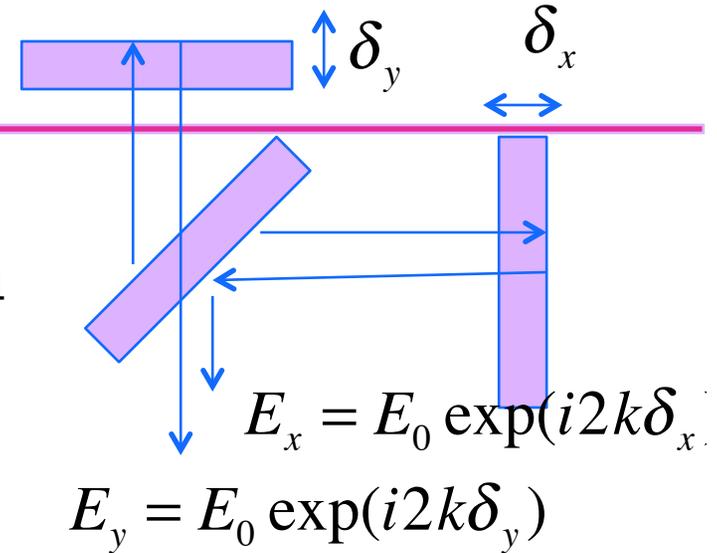




# Back of the envelope vs FFT

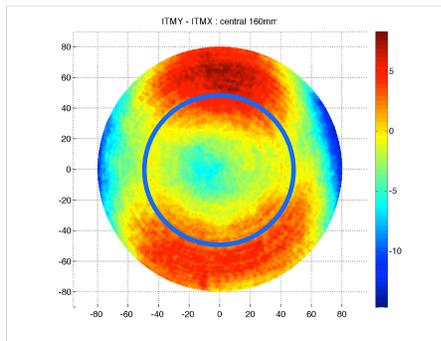
$$CD = Power(E_x - E_y) / Power(E_x + E_y)$$

$$= \int dx dy (2k)^2 \frac{2}{\pi w^2} \exp(-2 \frac{r^2}{w^2}) (\delta_x(x,y) - \delta_y(x,y))^2 / 4$$



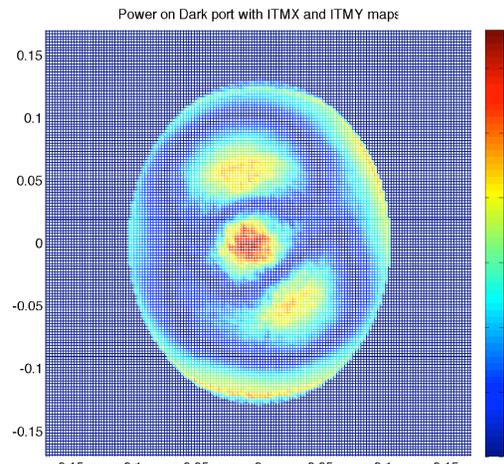
	W=7cm ITMX	W=7cm ITMY	W=7cm ITMX&Y	W=5.3 ITMX&Y
simple	1200	1900	5500	440
<del>FFT</del>	<del>320 ppm</del>	<del>570</del>	<del>1370</del>	<del>120</del>

$\delta_y - \delta_x$

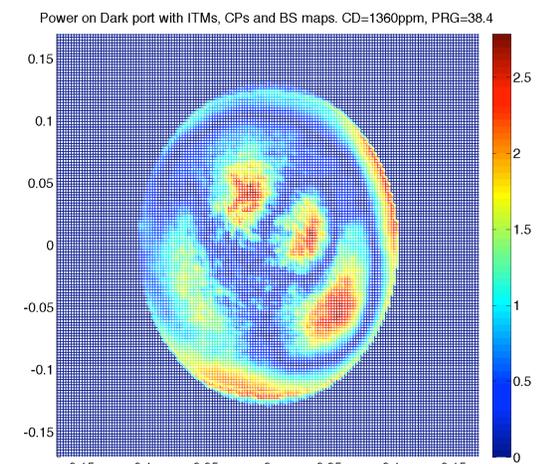


LIGO-G1400162

FFT w/ ITMx/y maps

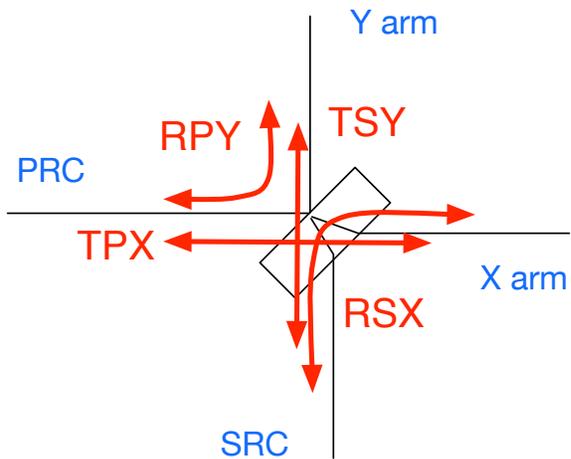


FFT with all maps (1300ppm)

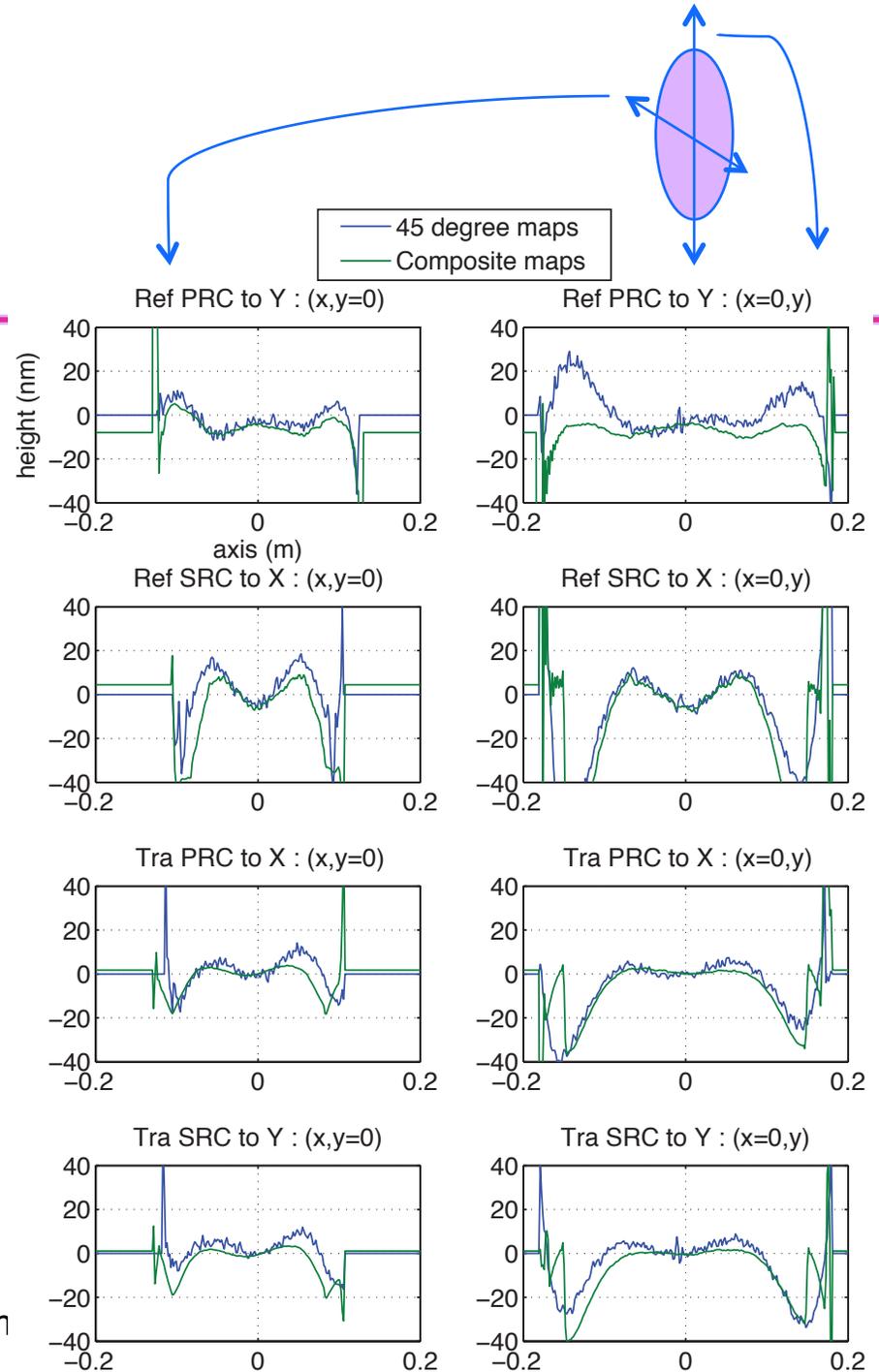
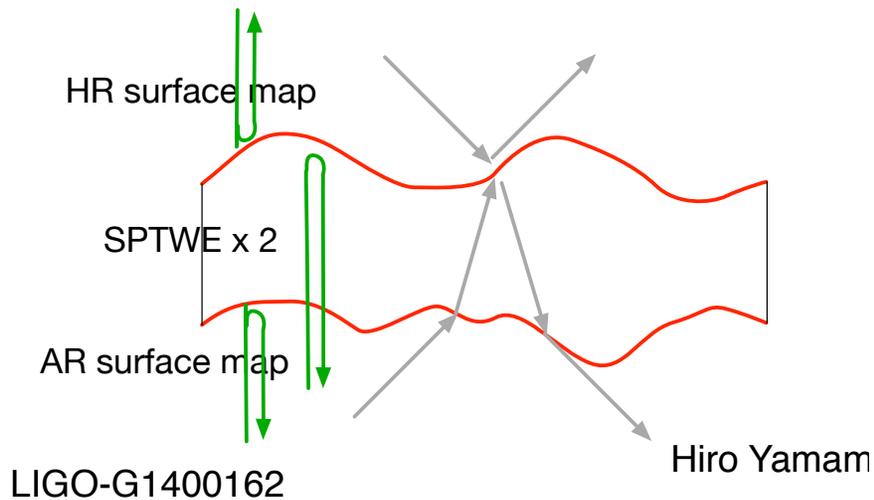




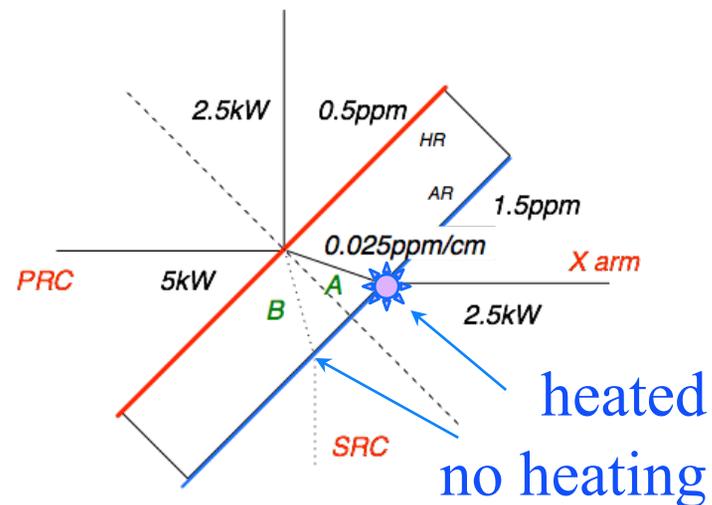
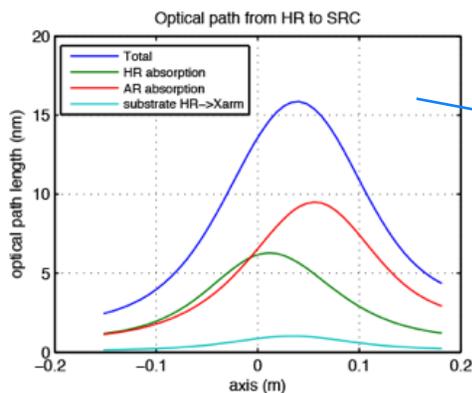
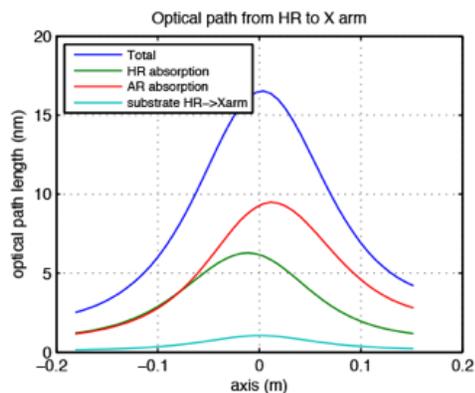
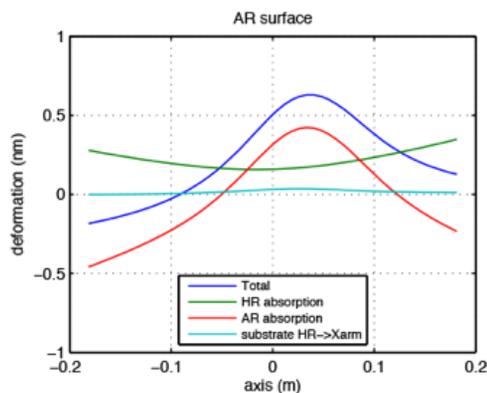
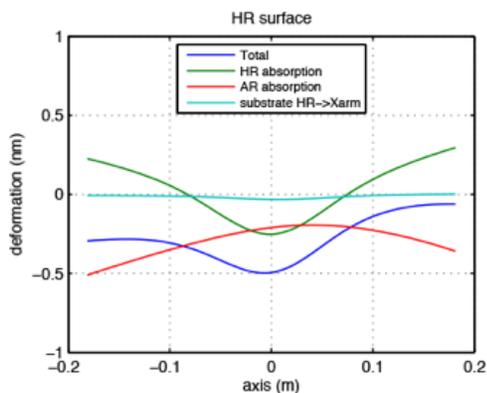
# LIGO BS, not quite well measured



## Composite map



# BS Thermal distortion



$$\frac{1}{R_{BS}} = \frac{\epsilon_{HR}}{R_{HR}} + \frac{\epsilon_{AR}}{R_{AR}}$$

$\epsilon$  : absorption of coating in ppm  
 red for  $\epsilon_{HR}=0.5\text{ppm}$ ,  $\epsilon_{AR}=1.5\text{ppm}$   
 blue for  $\epsilon_{HR}=0.5\text{ppm}$ ,  $\epsilon_{AR}=1.8\text{ppm}$

	$R_{HR}$	$R_{AR}$	$R_{BS}$
horizontal	500km	1000km	400km
vertical	420km	870km	340km

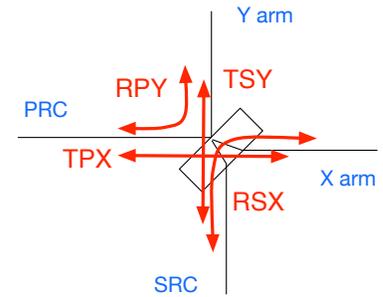
  

	$R_{HR}$	$R_{AR}$	$R_{BS}$
horizontal	500km	5000km	770km
vertical	440km	1530km	470km

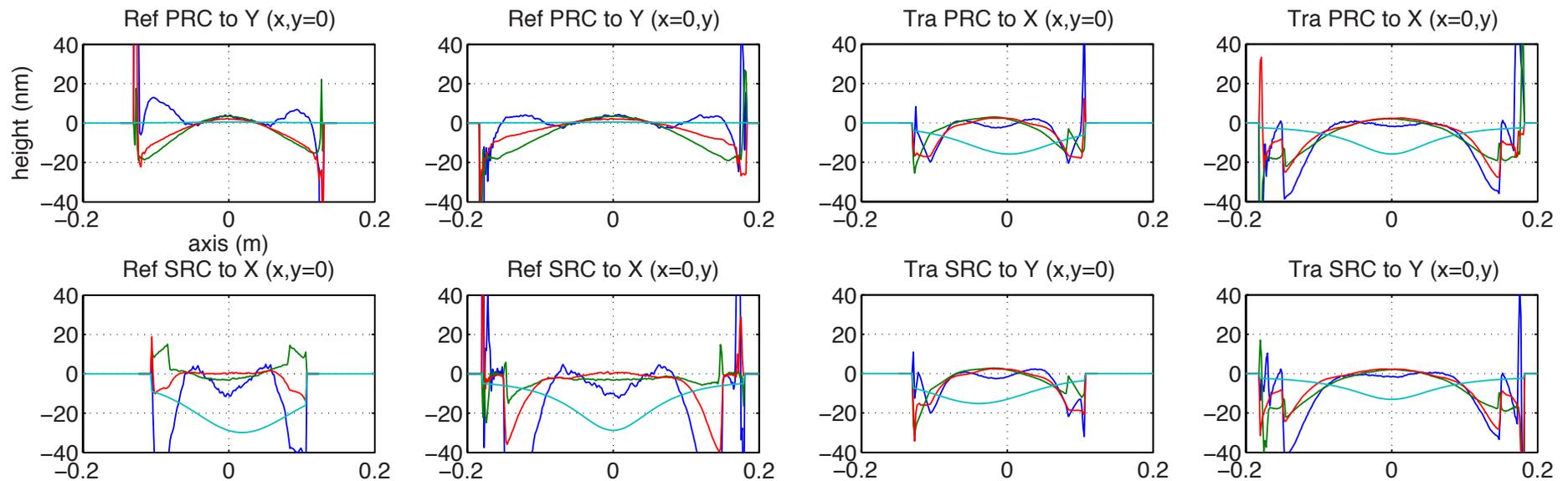
$\theta(\text{nrad})=26 \epsilon_{HR} + 38 \epsilon_{AR}$   
**70 nrad**



# BS : Three maps and Thermal distortion



— BS02 LLO now    — BS05 LLO    — BS06 LHO    — BS Thermal



Reflections

Transmissions



# Summary

abs(ITMX)-abs(ETMX) with maps, BS and thermal  
 abs(ITMY)-abs(ETMY)

		PRC				X arm			Y arm		
		CD ppm	PRG	HOM (BS)	Refl	Power	HOM (ppm)	Round trip loss	Power	HOM (ppm)	Round trip loss
H1	BS06	190	63	1390	0.14	8860	97	33	8680	115	37
	No BS	139	63	1380	0.14	8870	97	33	8690	115	37
	BS thermal	147	63	1460	0.14	8860	97	33	8670	114	37
	0.3-0.3 0.4-0.4	7	61.7	2400	0.14	8730	81	37	8550	137	37
	0.3-0.3 0.3-0.5	23	58.7	2900	0.11	8300	81	37	8110	151	45
L1	BS05	112	61	1165	0.15	8090	98	41	8090	111	38
	No BS	64	61	980	0.15	8120	98	41	8100	110	38

With miracle TCS



# Coating + Thermal = flat

770kW in LLO X arm, 0.3ppm absorption

