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Noise requirement for the test mass electro-static driver

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#### 1 Introduction

A low-noise, lower range driver for the test mass electro-static actuator is being designed for use in interferometer low-noise operation (the UK high-voltage driver will continue to be used for lock acquisition). This note specifies the maximum voltage noise for this low-noise driver.

## 2 Force noise per actuator quadrant

The voltage noise in the actuator quadrants will be independent of each other, so I start by defining the force noise per quadrant. The force coefficient for the ETM is still somewhat uncertain. John Miller's FEA model gave 4e-10 N/V<sup>2</sup>, but measurements give factors of 2-4 smaller values (see LHO log entry 12220). It was recently suggested that the ring heater structure could be altering the field lines in a way that reduces the net force. I assume a force coefficient of 2e-10 N/V<sup>2</sup> for the full ETM/ERM electrode pattern, or a force coefficient of  $a = 5e-11 \text{ N/V}^2$  per quadrant. The force noise per quadrant, assuming the bias path is sufficiently low-pass filtered that its noise is negligible, is thus:

$$F_q = 2a \cdot V_b \cdot v_n = 10^{-8} v_n \cdot (V_b/100) N/V$$

#### 3 Force noise for both ETMs

Since the ESD force coefficient for the ITMs is about 30 times smaller than the ETMs, I neglect them in the calculation. The total force noise from the 8 ETM/ERM quadrants is:

$$F_{esd} = \sqrt{8} \times 10^{-8} v_n \cdot (V_b/100) N/V$$

### 4 Maximum allowed force noise from ESD

For the maximum force noise, I use an Advanced LIGO configuration that is good for low frequency noise, namely with 25 W input power (other variable parameters do not significantly impact the noise below 30 Hz). The limiting strain noise in this case is  $1.6e-23 \text{ Hz}^{-1/2}$  at 20 Hz (see LIGO-T1200307, e.g.); the arm differential displacement noise is  $6.5e-20 \text{ m/Hz}^{1/2}$  at 20 Hz (this frequency is chosen because a  $1/f^2$  line is tangent with the strain noise spectrum at about 20 Hz).

The maximum displacement noise from ESD noise is 10 times smaller than this value, which gives a maximum (total differential) ESD force noise of:

$$F_{max} = 40 \; kg \; \cdot (2\pi \cdot 20 \; Hz)^2 \cdot 6.5 \times 10^{-21} \; m/\sqrt{Hz} = \; 4.1 \times 10^{-15} \; N/\sqrt{Hz}$$

# 5 ESD signal path voltage noise

The maximum voltage noise on each ESD quadrant signal path comes from the previous two equations:

$$v_n(f \geq 20Hz) \leq \frac{4.1 \times 10^{-15} \, N/\sqrt{Hz}}{\sqrt{8} \times 10^{-8} \cdot (V_b/100) N/V} = 150 \, nV/\sqrt{Hz} \cdot \left(\frac{100 \, V}{V_b}\right)$$

Between 10-20 Hz the interferometer strain noise falls a bit faster than  $f^{-2}$ , so the noise at 10 Hz can be a bit higher; I set  $v_n(10 \text{ Hz}) < 250 \text{ nV/Hz}^{1/2}$ .