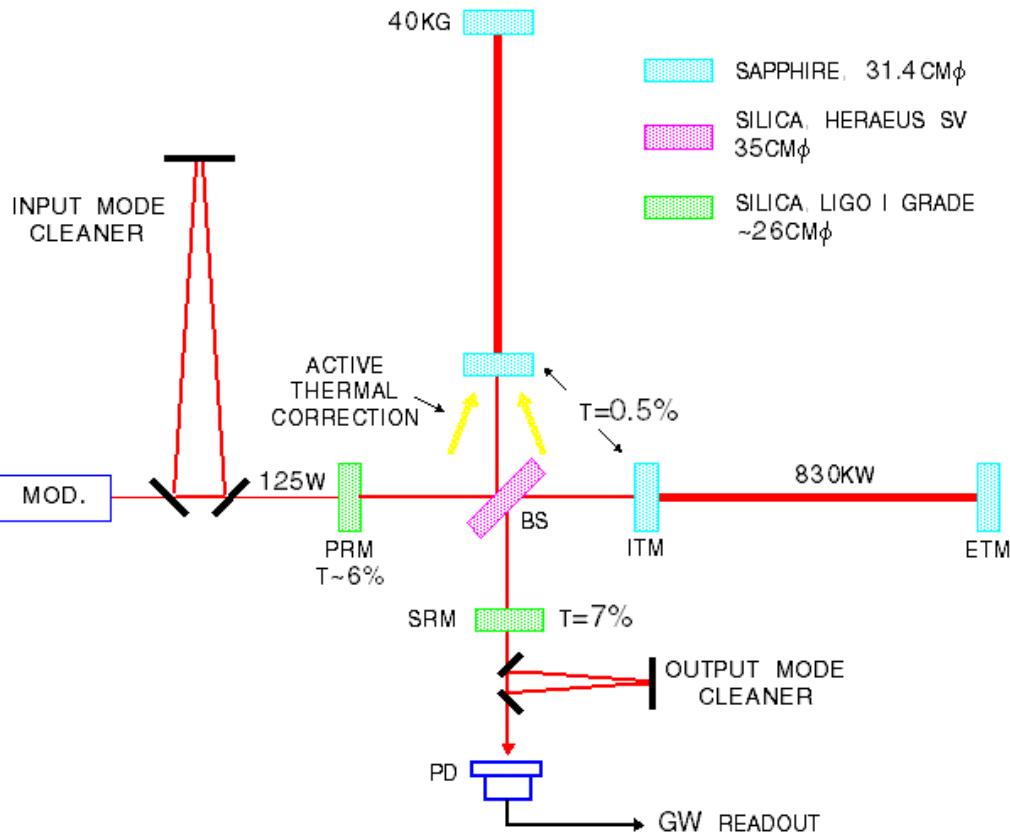
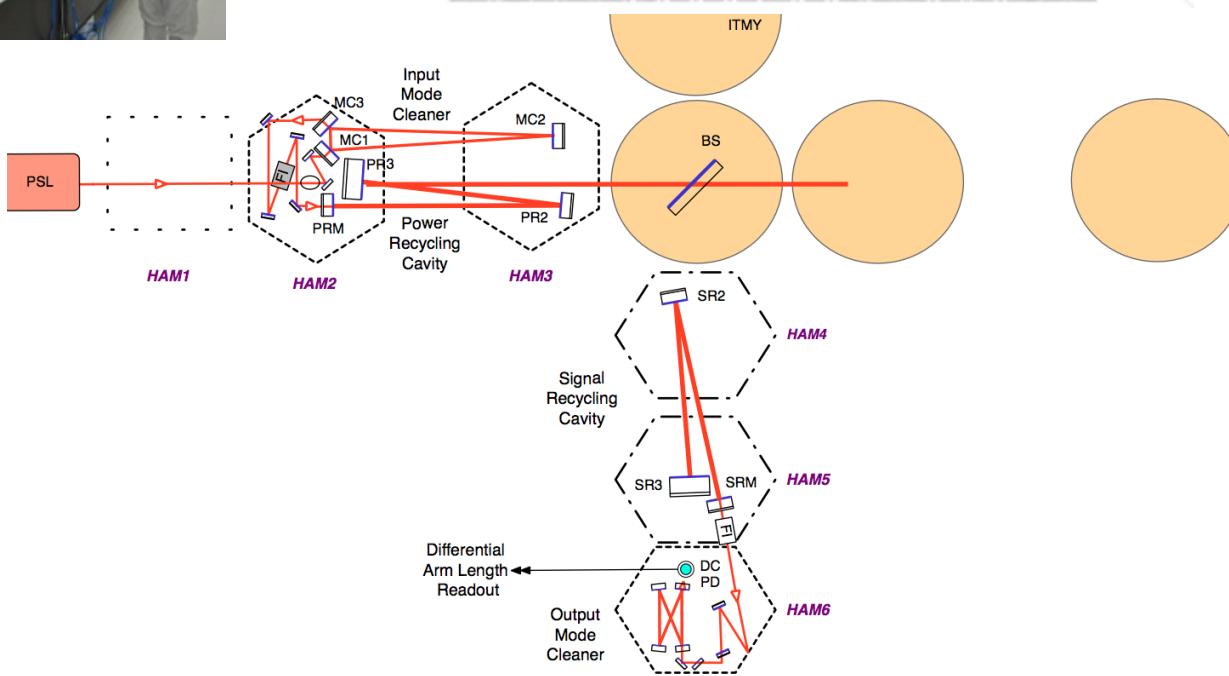
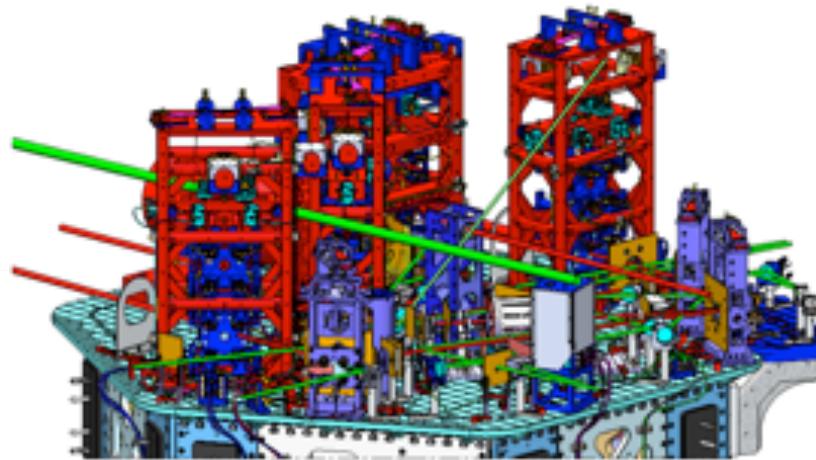

“IO”

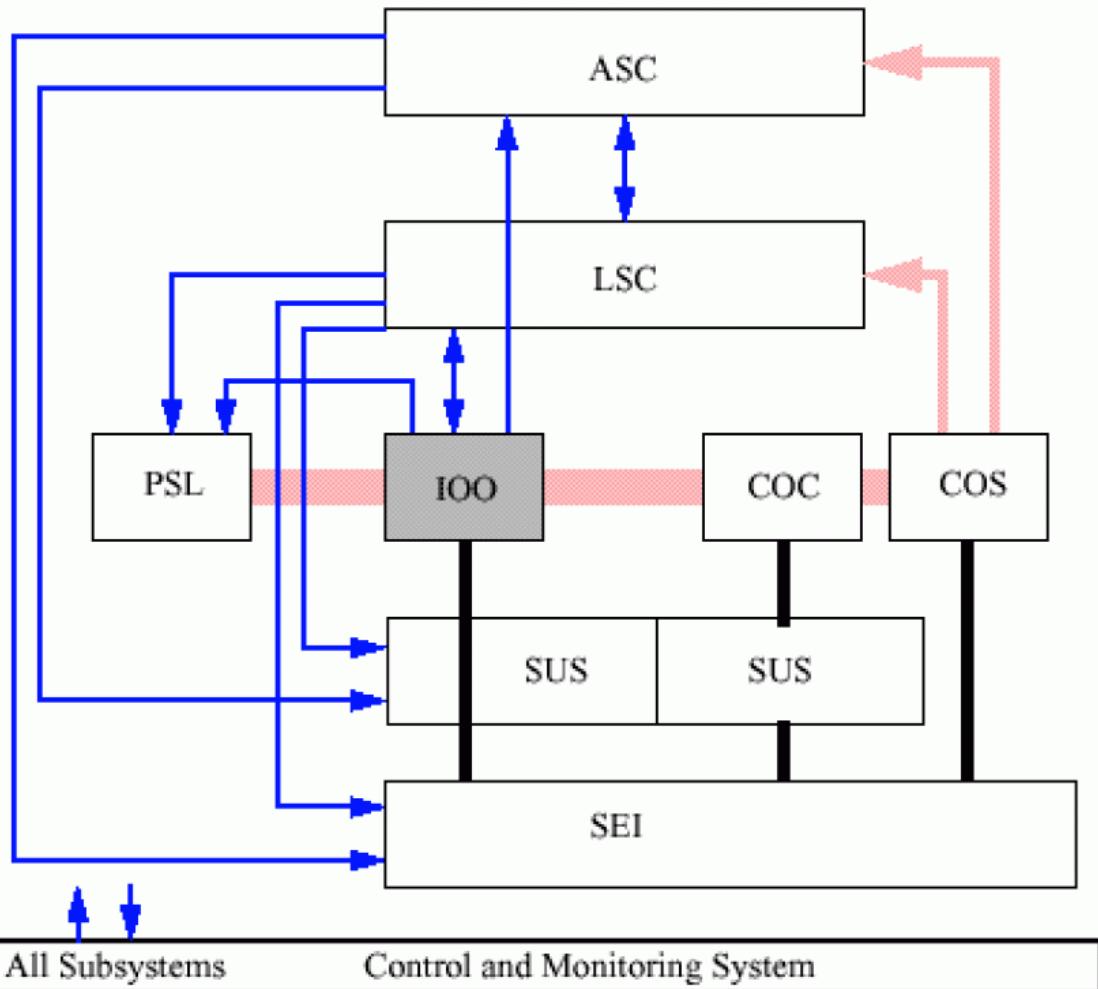
1. Input optics
2. EOM
3. Mode cleaner
4. Faraday
5. Other components



New features:

- » Signal recycling
- » 200-watt laser
- » 40 kg test masses
- » Larger beam size
- » Higher arm finesse
- » Moderate recycling factor
- » Active thermal correction
- » Better isolation from the ground
- » Output mode cleaner

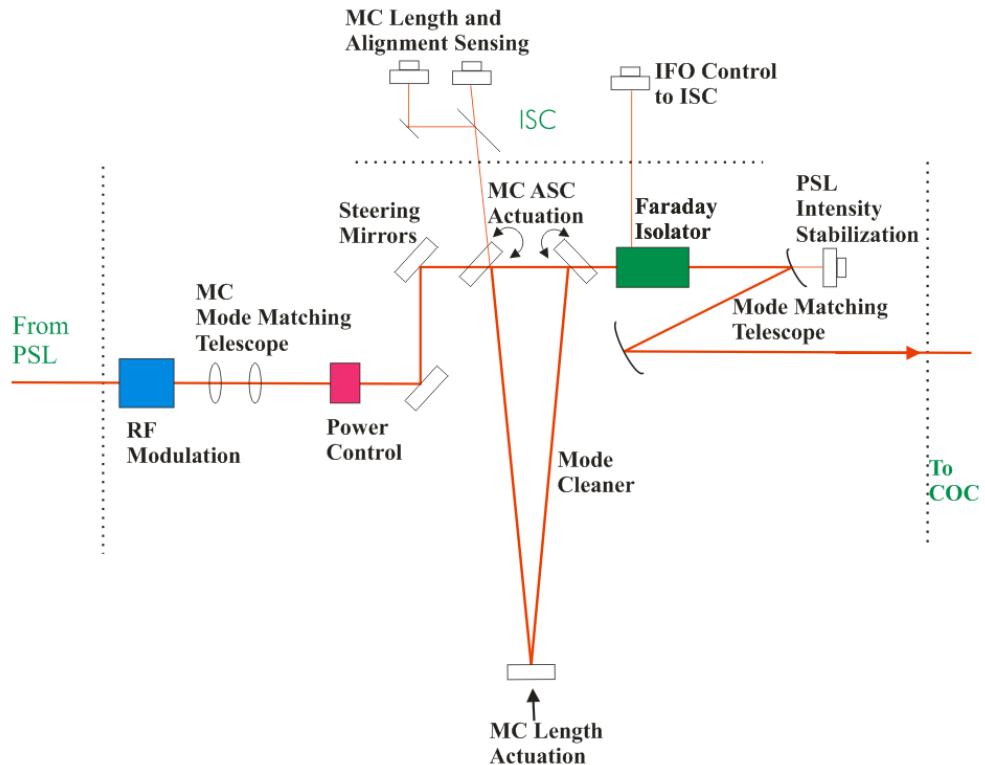




The input optics (IO) conditions the PSL laser light and delivers it to the interferometer.

It provides:

- RF modulation for length and alignment control functions
- Power control
- Laser mode cleaning and frequency stabilization
- Isolation of laser from interferometer reflected light
- Optical signal distribution to length and alignment control
- Mode matching to recycling and arm cavities
- Design and fabrication of small PRMs and SRMs



PSL = pre-stabilized laser

COC = core optical components

IMC = input mode cleaner

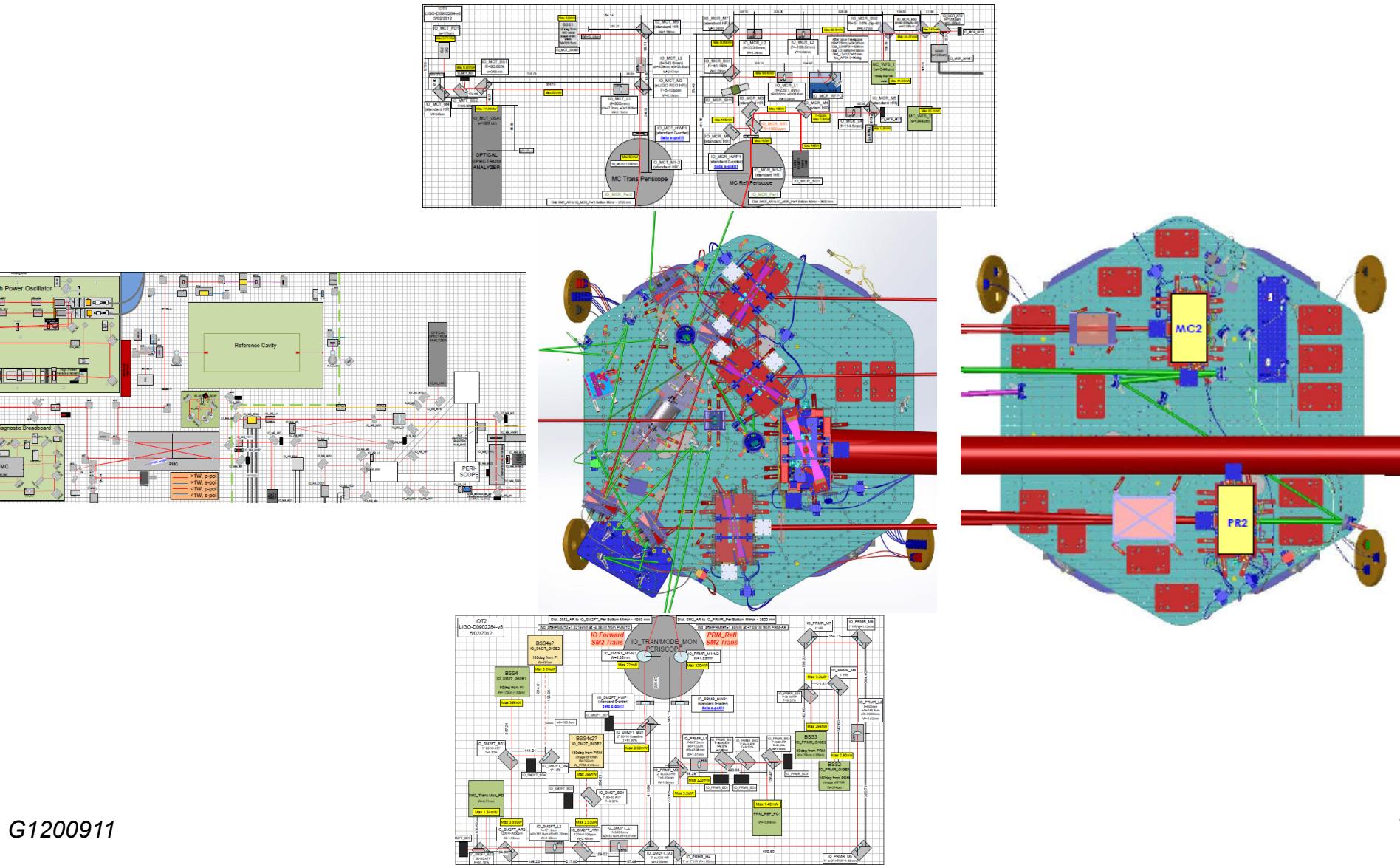
ISC = interferometer sensing and control

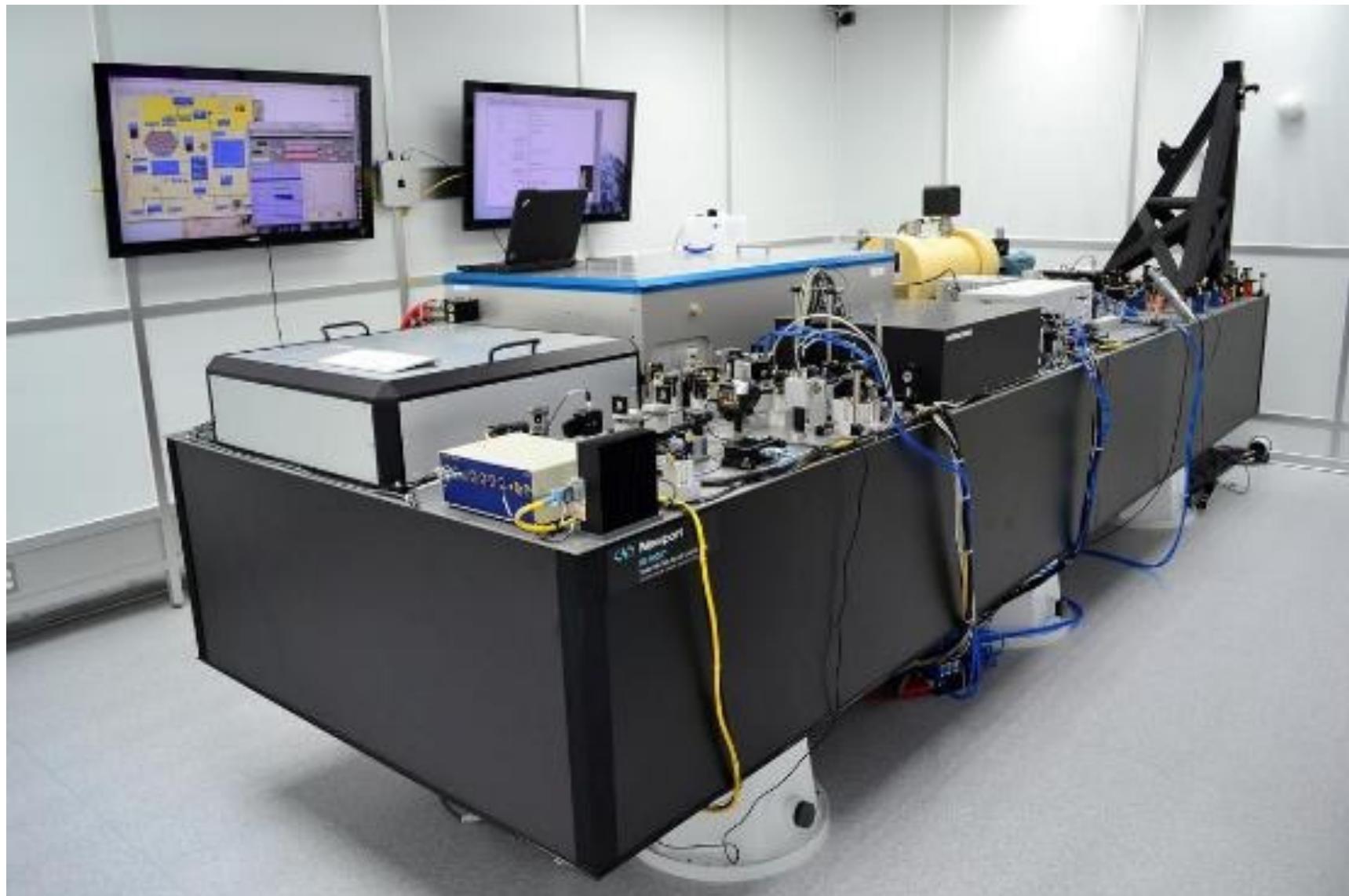
PRM = power recycling mirror

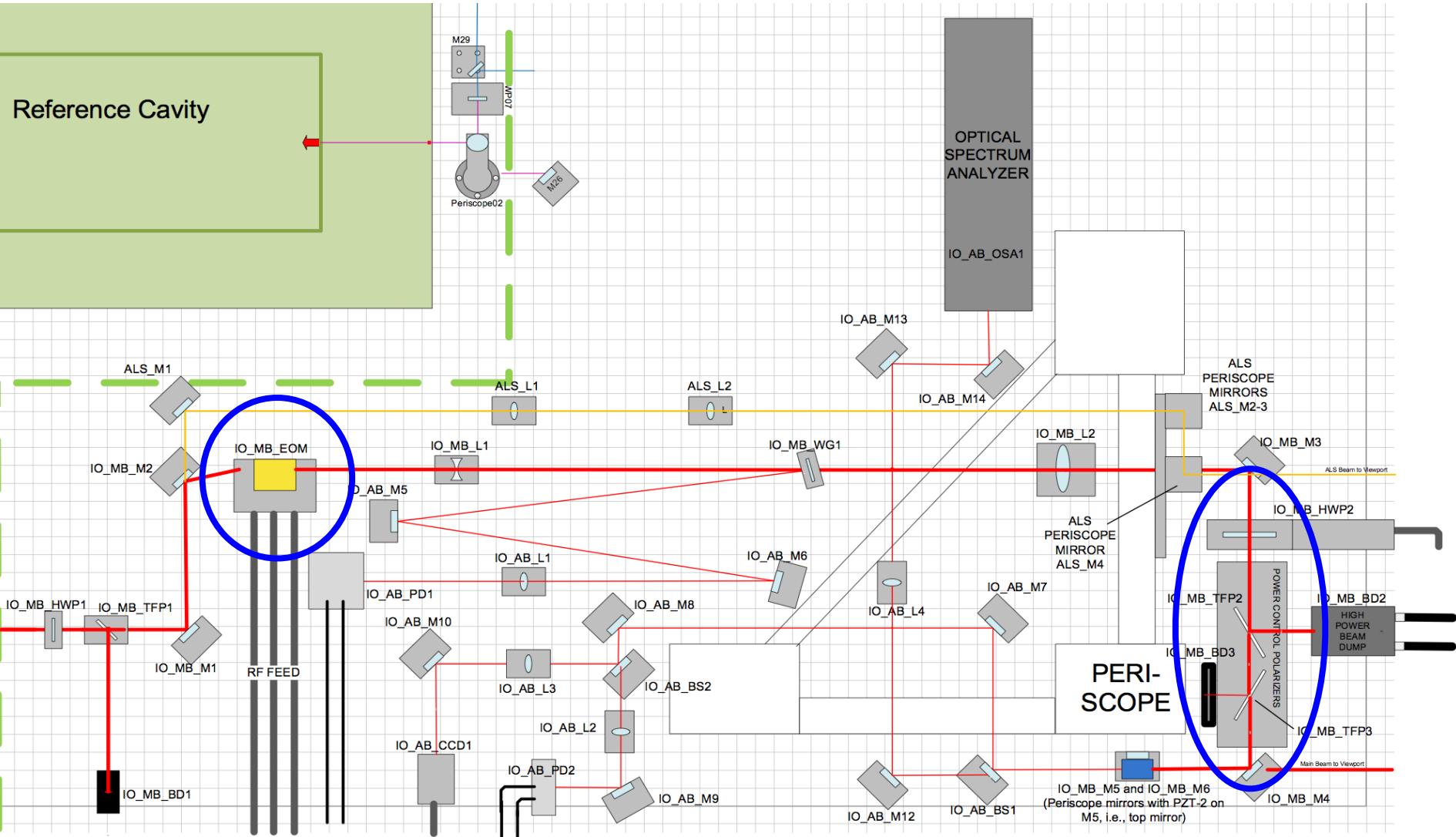
SRM = signal recycling mirror

Activity Name	Start	Finish	FY2008	FY2009	FY2010	FY2011	FY2012	FY2013	FY2014	FY2015	-Y2016
LIGO LIGO Lab Program - AdvL Current	21-Aug-00 A	03-Apr-12									
LIGO.3 Advanced LIGO Development	21-Aug-00 A	15-Apr-11									
LIGO.3.05 Input Optics (IO)	21-Aug-00 A	15-Apr-11									
LIGO.3.05.1 IO Management	21-Aug-00 A	23-Feb-10 A									
LIGO.3.05.1.1 IO Development Management	21-Aug-00 A	23-Feb-10 A									
LIGO.3.05.3 IO Design	21-Aug-00 A	15-Apr-11									
LIGO.3.05.3.1 IO Conceptual Design/Requirements	21-Aug-00 A	07-May-02 A									
LIGO.3.05.3.2 IO Preliminary Design	07-May-02 A	21-Aug-07 A									
LIGO.3.05.3.3 IO Final Design	07-Apr-06 A	15-Apr-11									
LIGO.4 Advanced LIGO Project	02-Sep-08 A	03-Apr-12									
LIGO.4.05 Input Optics (IO)	02-Sep-08 A	03-Apr-12									
LIGO.4.05.1 IO Management	02-Sep-08 A	03-Apr-12									
LIGO.4.05.1.2 IO Fabrication Management	02-Sep-08 A	03-Apr-12									
LIGO.4.05.4 IO Fabrication	02-Sep-08 A	03-Apr-12									
LIGO.4.05.4.1 IO Modulation System	17-Feb-09 A	28-Sep-11									
LIGO.4.05.4.2 IO Mode Cleaner and MMT Assemblies	02-Sep-08 A	03-Apr-12									
LIGO.4.05.4.3 IO Optical Isolation	15-Feb-10 A	28-Sep-11									
LIGO.4.05.4.4 IO Baffles	03-May-10 A	10-Feb-12									

- Overall IO Final Design substantially completed in Feb 2010
 - May 2011 is for baffles (additional scope), installation
- IO Project phase began in Sept 08
 - Optics procurement (input mode cleaner, recycling mirrors, steering and mode-matching mirrors) is largest component of the project
 - Well underway; on track to meet installation schedule







IO on the PSL table

Electro-optic modulator

Mode matching telescope

RFAM photodiode

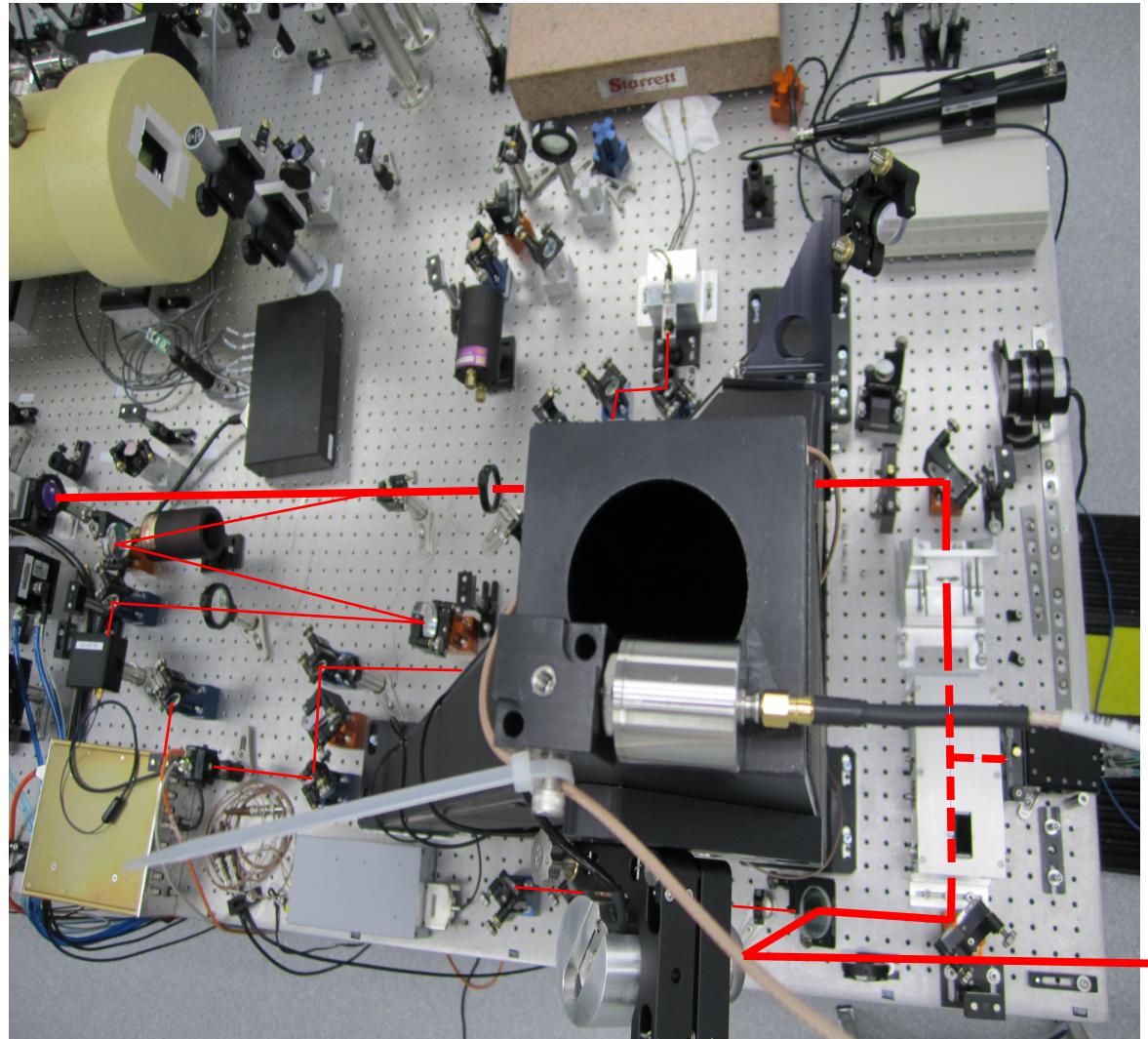
-

Power control

Beam positioning piezo

Optical Spectrum Analyzer

Beam viewing camera



Electric field emerging from the PM:

$$\mathbf{E} = \mathbf{E}_0 e^{i(kL - \omega t)}$$

with $k = \omega n/c = 2\pi n/\lambda \equiv k_0 n$ and $n = \sqrt{\epsilon}$.

Suppose

$$n = n_0 + \Delta n \sin(\Omega t)$$

then phase will be modulated at Ω

$$\mathbf{E} = \mathbf{E}_0 e^{i(k_0 n_0 L - \omega t + k_o L \Delta n \sin(\Omega t))} = \mathbf{E}_0 e^{i(k_0 n_0 L - \omega t)} e^{iA \sin(\Omega t)}$$

with $A = k_o L \Delta n$. If A is small

$$e^{iA \sin(\Omega t)} = 1 + iA \sin(\Omega t) + \dots = 1 + \frac{A}{2} [e^{i\Omega t} - e^{-i\Omega t}] + \dots$$

making

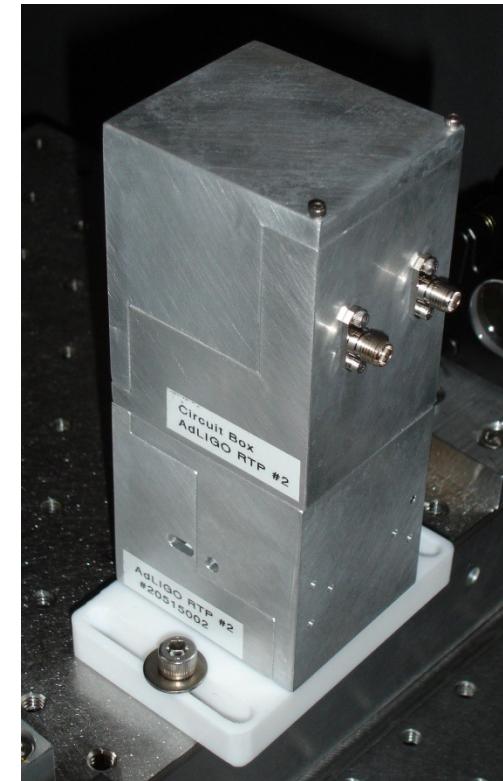
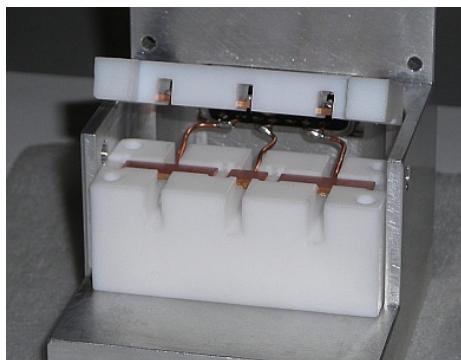
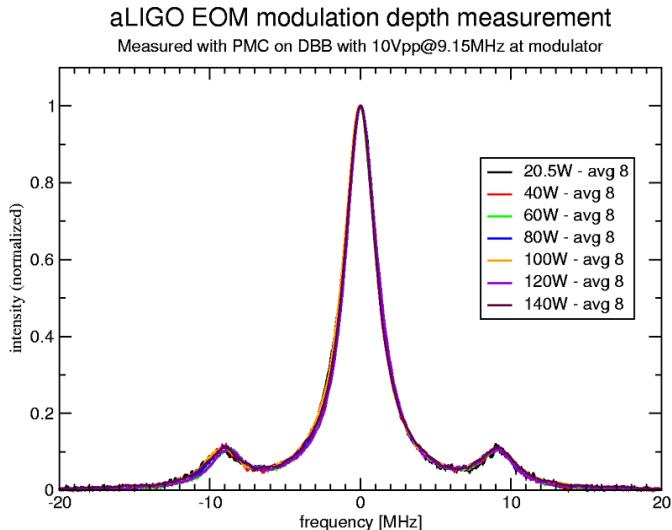
$$\mathbf{E} = \mathbf{E}_0 e^{i k_0 n_0 L} \cdot \left\{ e^{-i\omega t} + \frac{A}{2} e^{-i(\omega - \Omega t)} - \frac{A}{2} e^{-i(\omega + \Omega t)} \right\} + \dots$$

The frequency spectrum contains the carrier at ω , sidebands at $\omega \pm \Omega$, plus ...

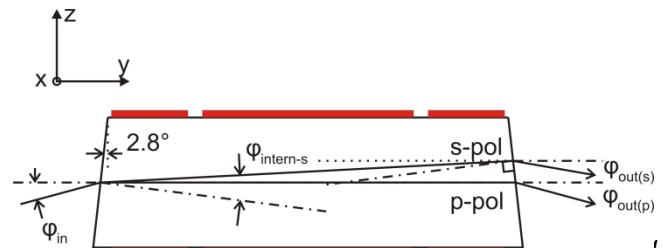
Note: The intensity in all of these is not time varying:

$$I \equiv \mathbf{E} \cdot \mathbf{E}^* = E_0^2$$

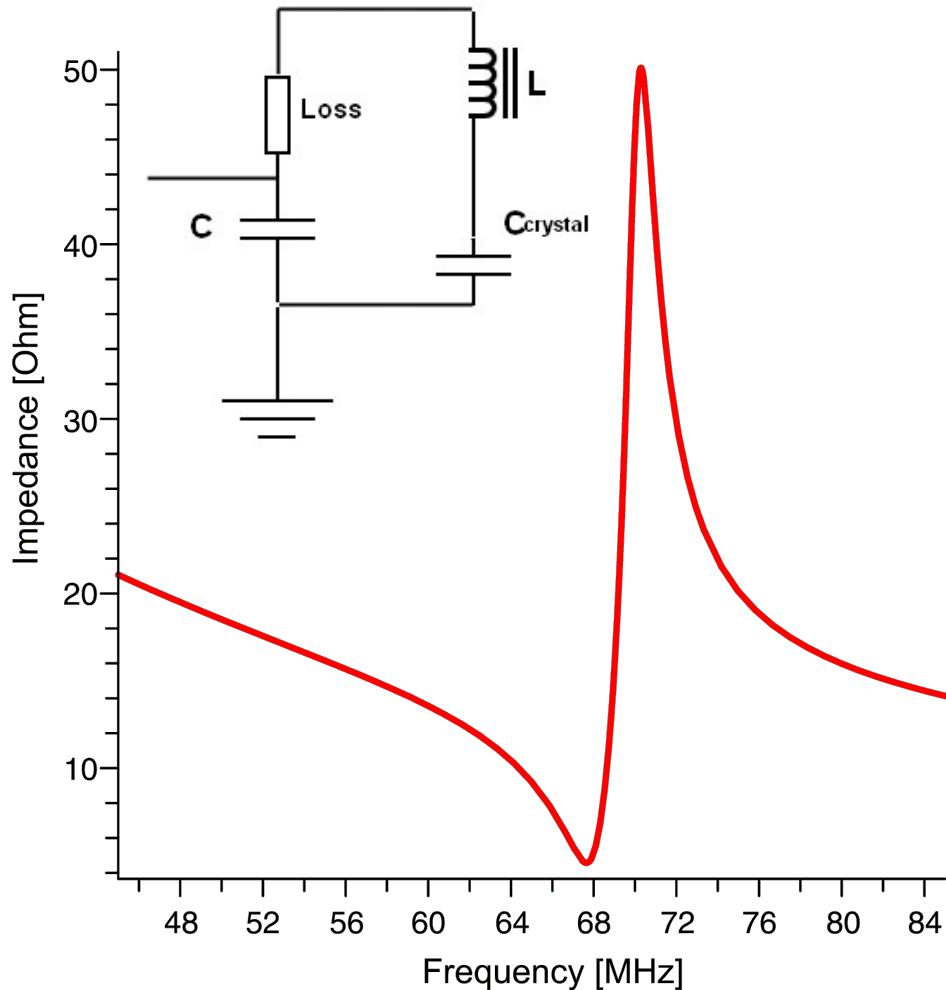
- Modulators use rubidium titanyl phosphate (RTP)
 - » Electro-optic response similar to LiNbO_3
 - » low absorption => low thermal lensing



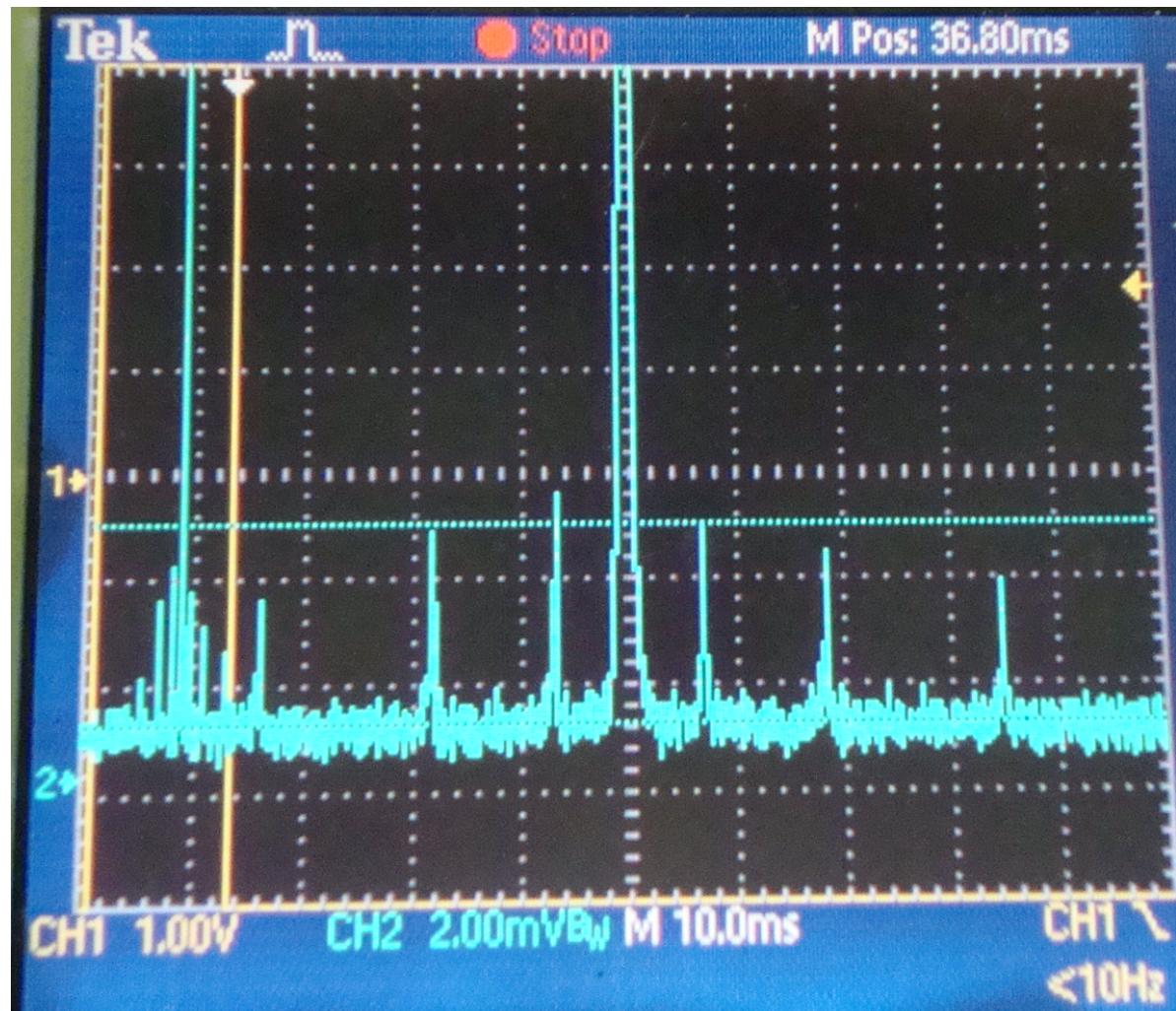
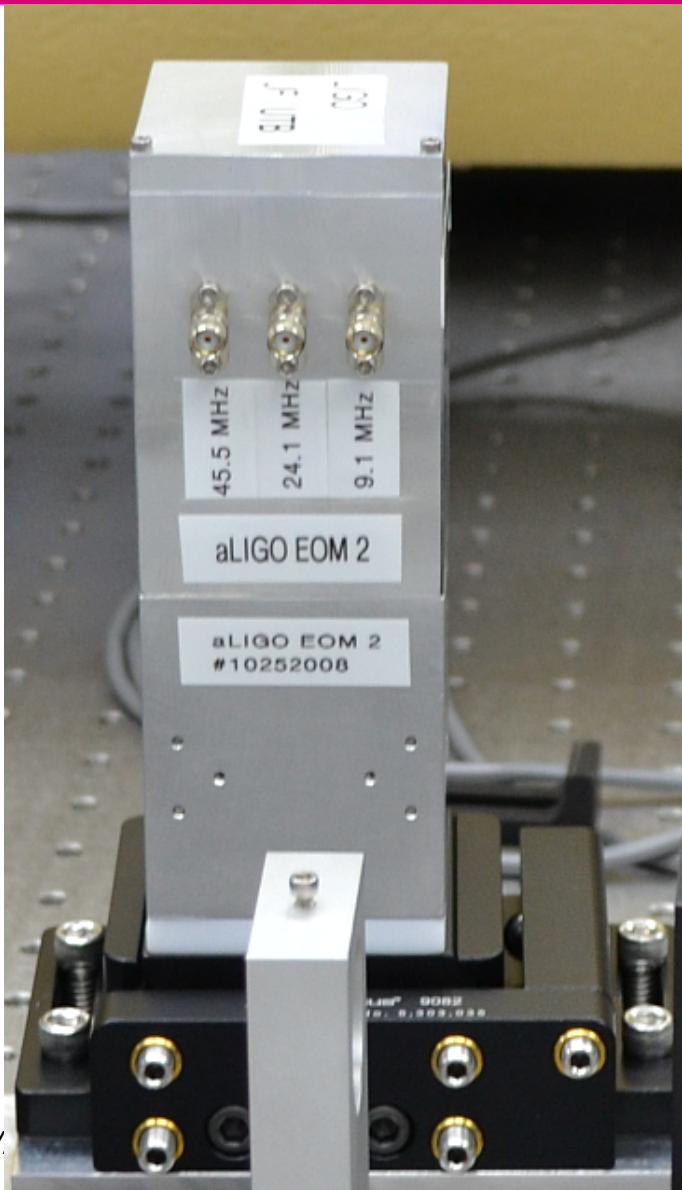
- Multiple electrode configuration
- Wedge, to reduce RFAM from polarization impurity
- RF matching circuit in separate housing
- Installed in enhanced LIGO at both sites



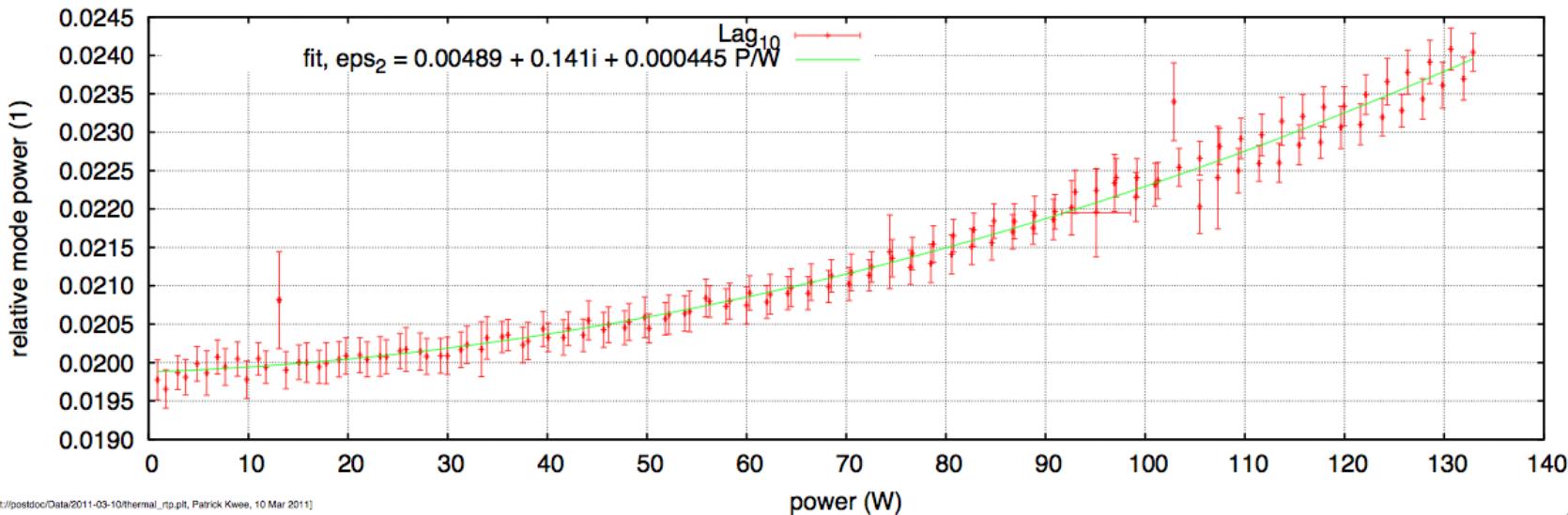
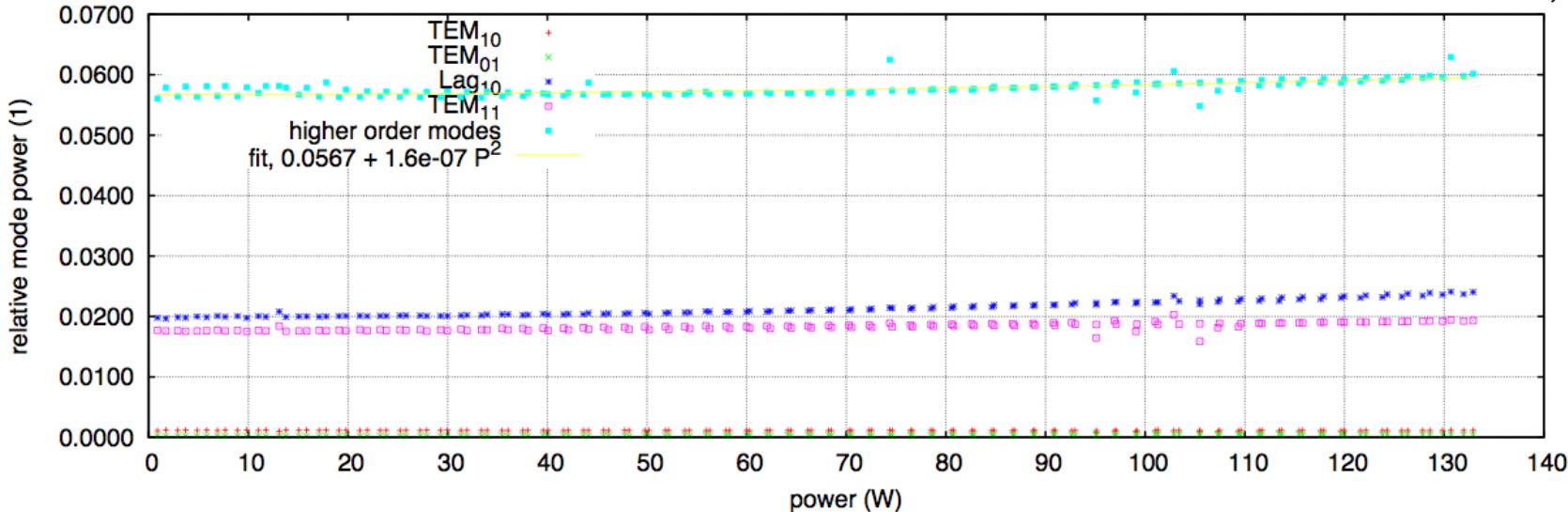
- Impedance matching circuit in separate housing.
- Resonant circuit with $50\ \Omega$ input impedance.
- Three resonant circuits:
 - » 24.5 / 33.0 / 61.2 MHz

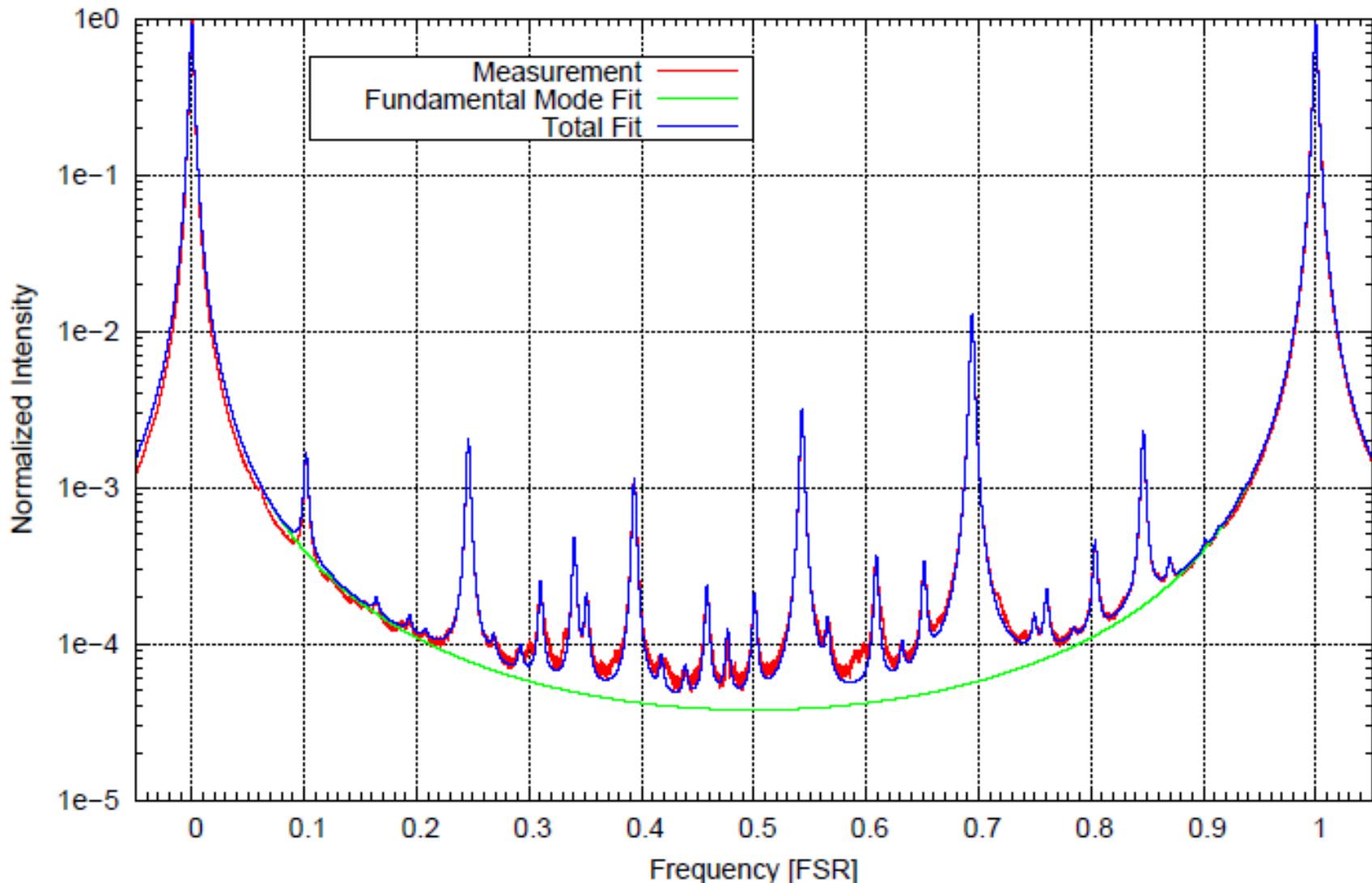


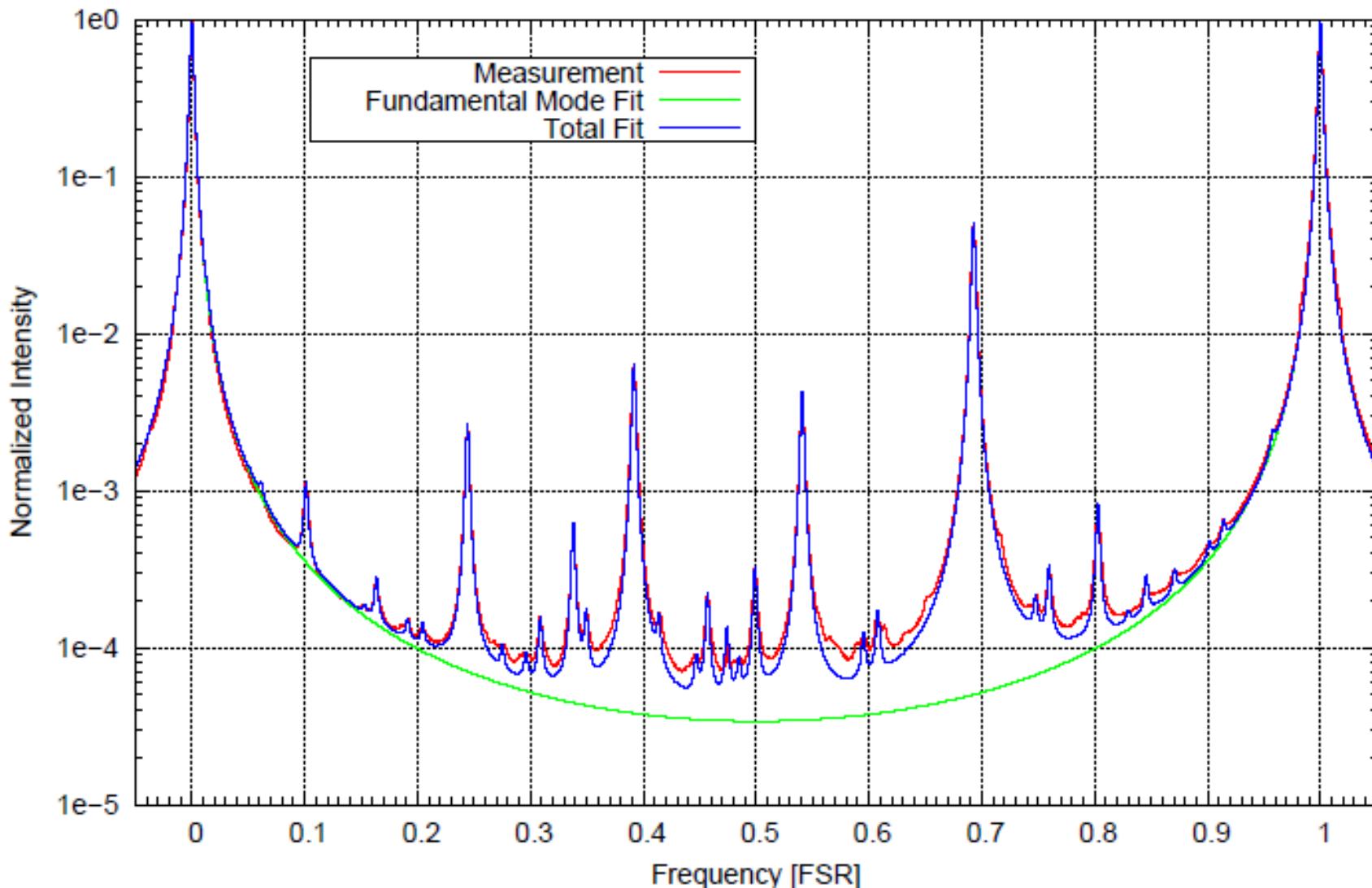
LIGO 3 RF modulators in one box



Data from Patrick Kwee, AEI

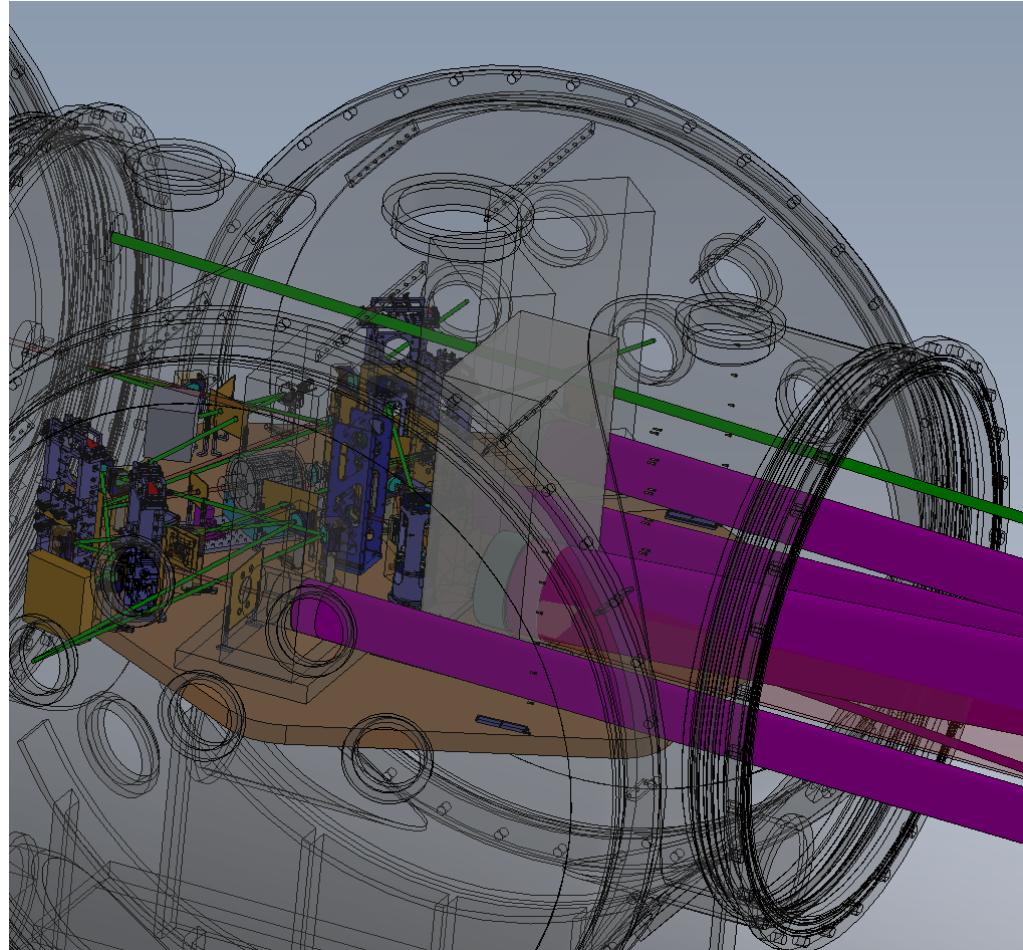


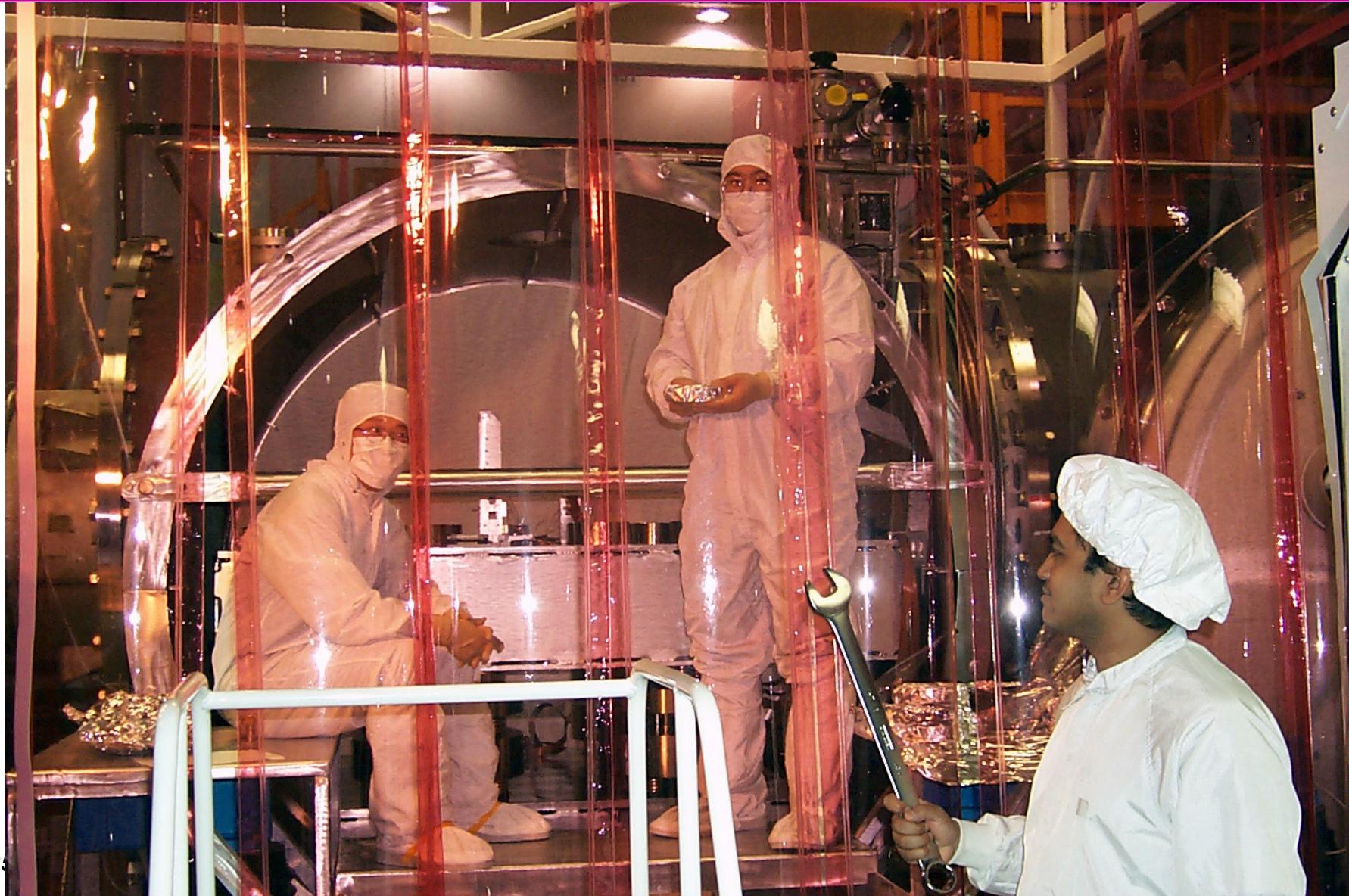


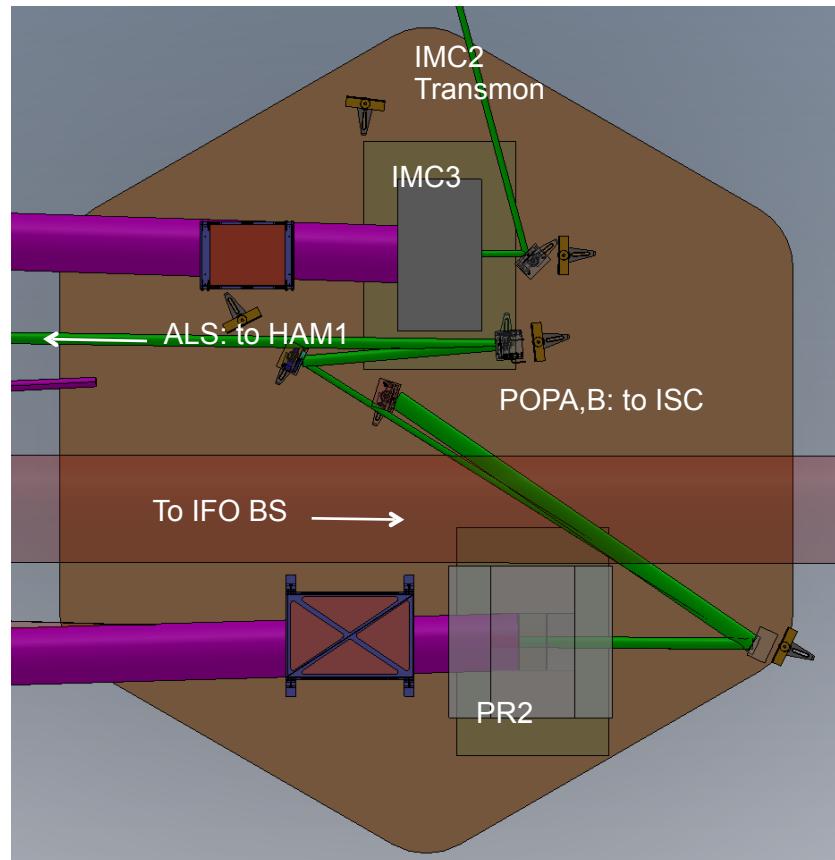
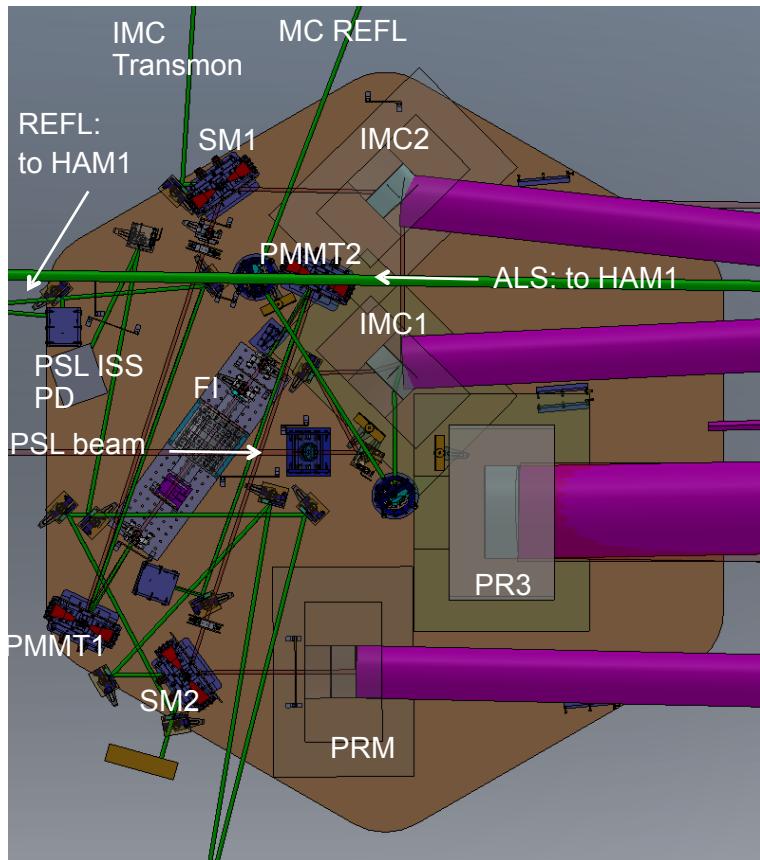


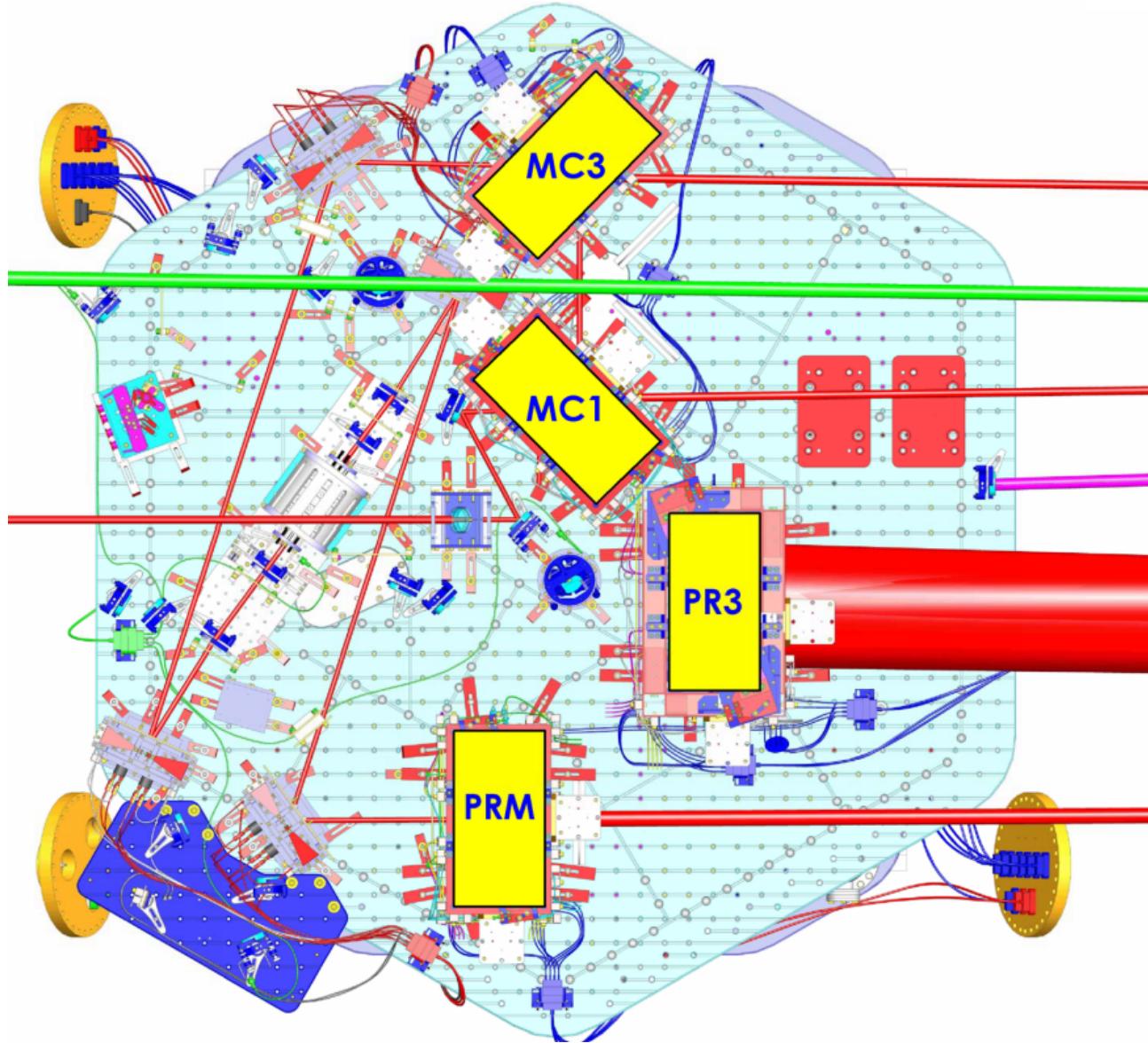
☒ Most of the IO is located in HAMs 2 and 3

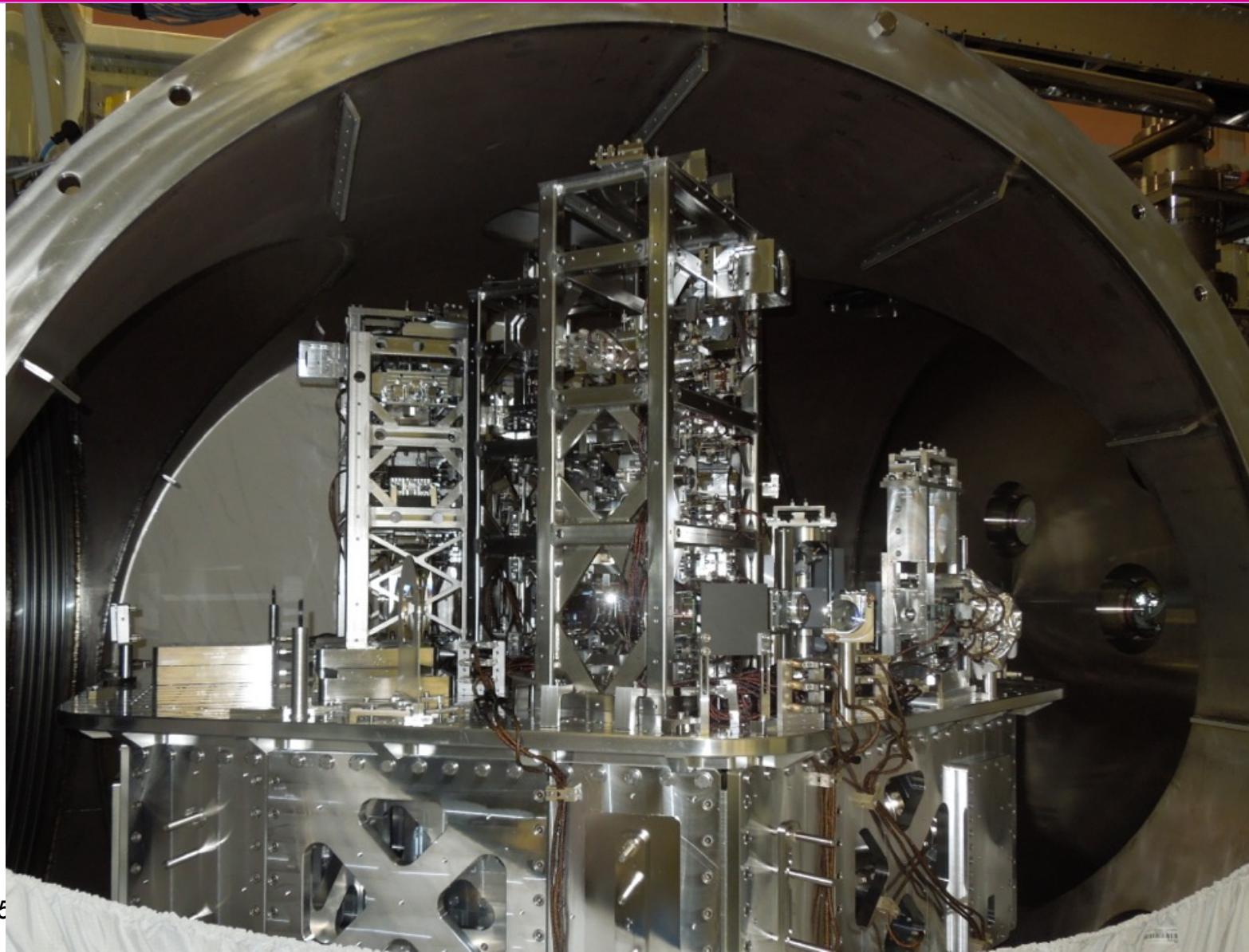
☒ In-vacuum layout is dense and complex, especially in HAM 2



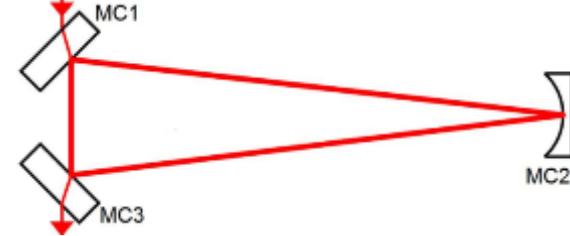
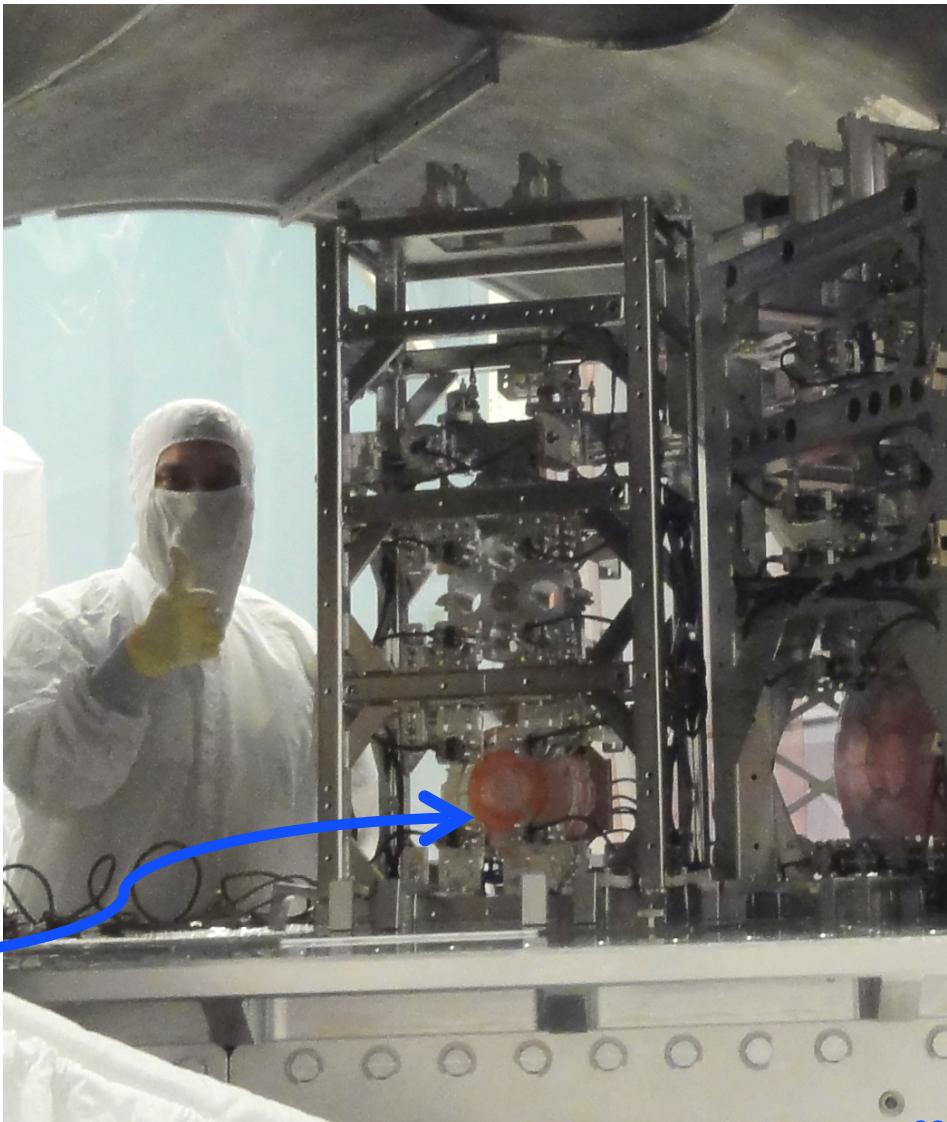
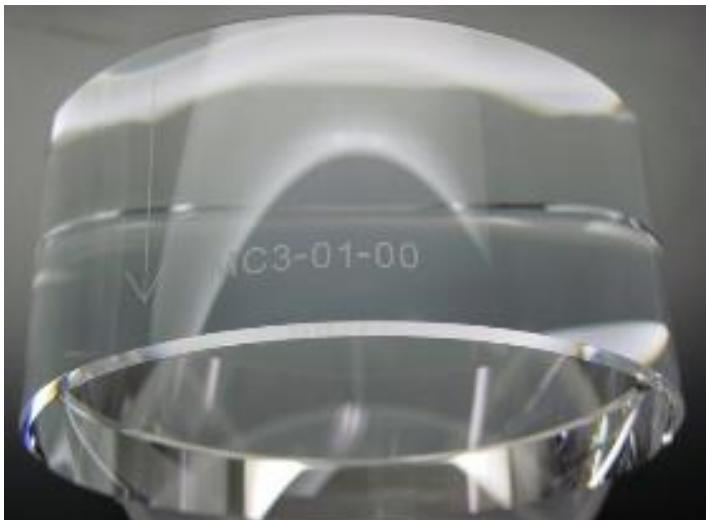


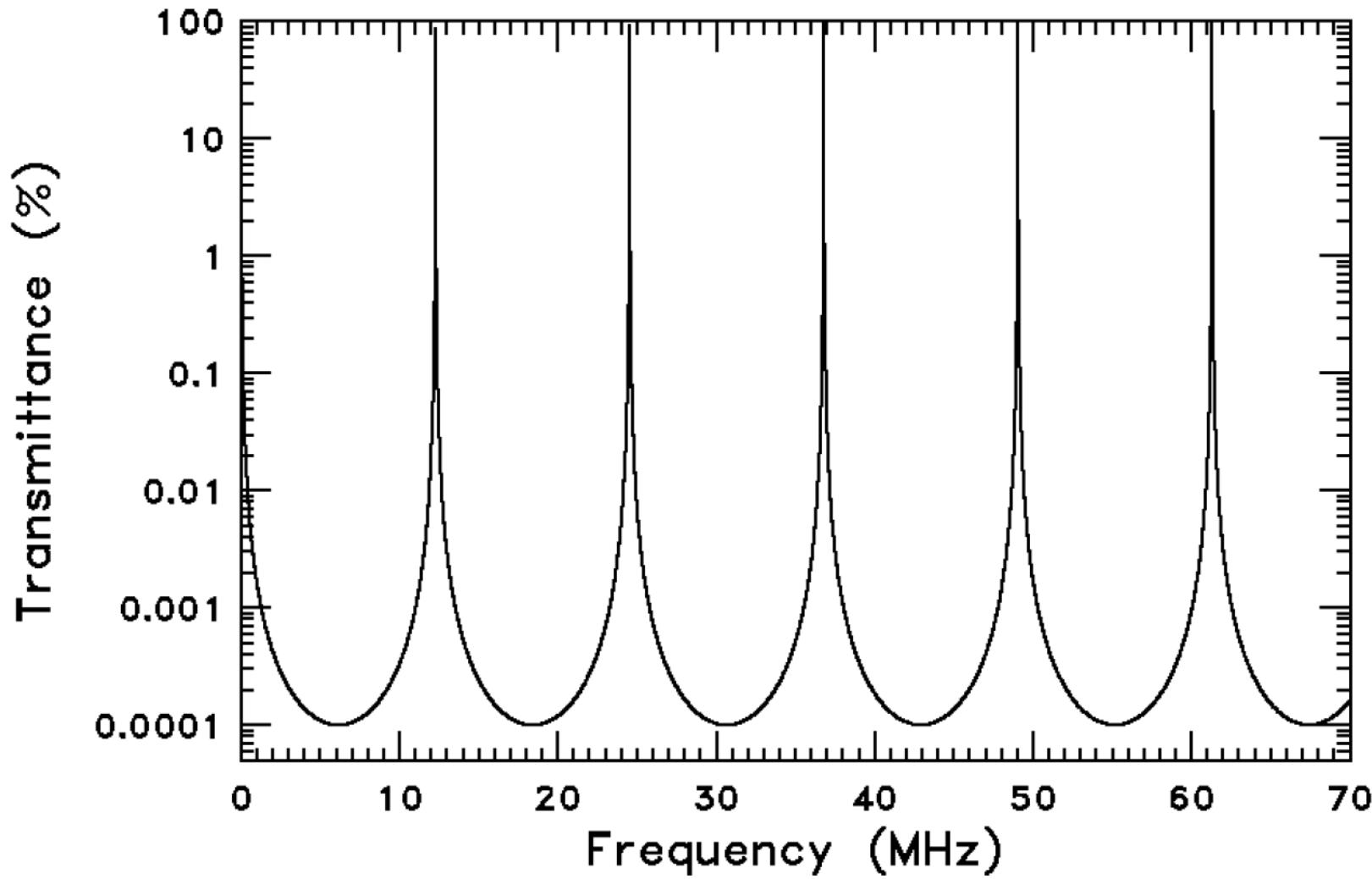


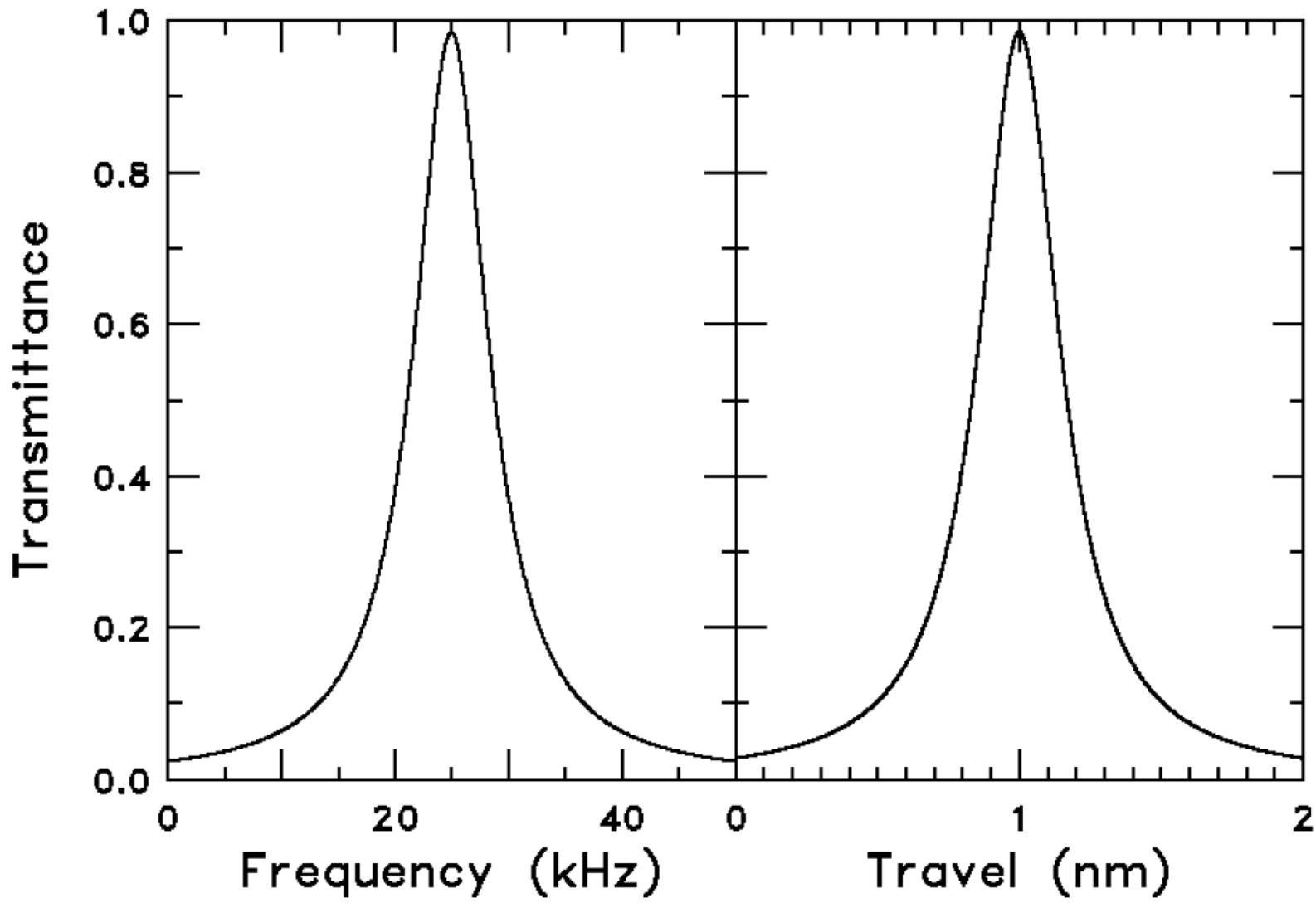




- Triangular ring cavity
- Stabilize pointing
- Frequency reference
- $L/2 = 16.5 \text{ m}$; Finesse = 520







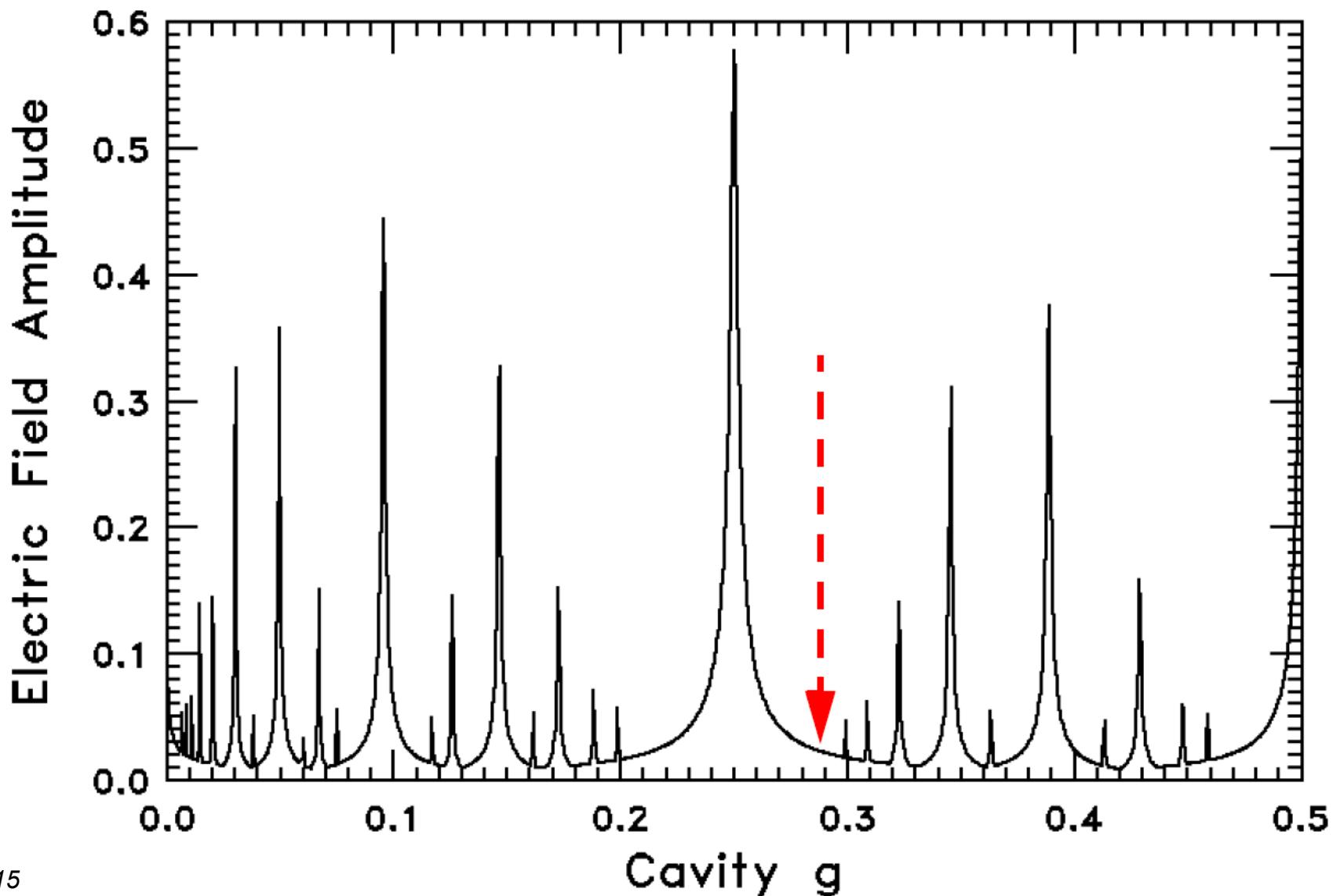
For TEM_{lm} Gaussian modes, the resonances occur at frequencies

$$v_{lm} = \frac{c}{2L} \left[n - \frac{1}{2} + \frac{l+m+1}{\pi} \arccos(\sqrt{g}) \right]$$

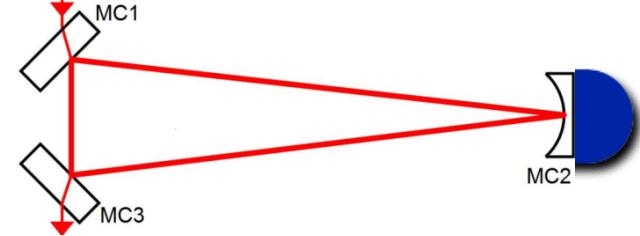
where $g = L/R$ with R the radius of curvature of the curved mirror. The resonator is adjusted for resonance with the TEM_{00} mode; this sets the value of n (of order 10^7). The radius of curvature (and hence g) is chosen so that the resonance condition is not satisfied for $l \neq 0$ and $m \neq 0$ for any $\{n,l,m\}$. The condition is

$$\frac{l+m}{\pi} \arccos \sqrt{g} \neq \text{integer} + \epsilon$$

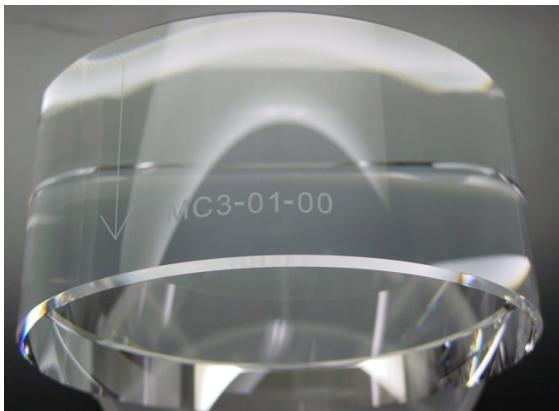
where ϵ specifies the amount the higher-order mode avoids being resonant.

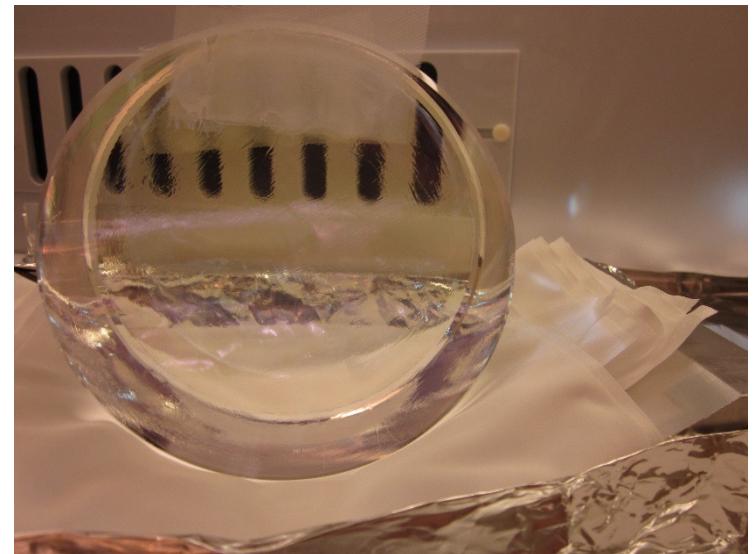
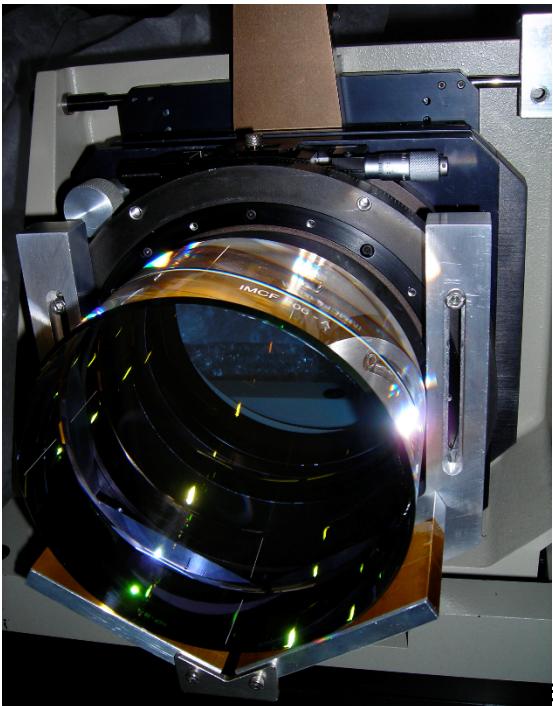
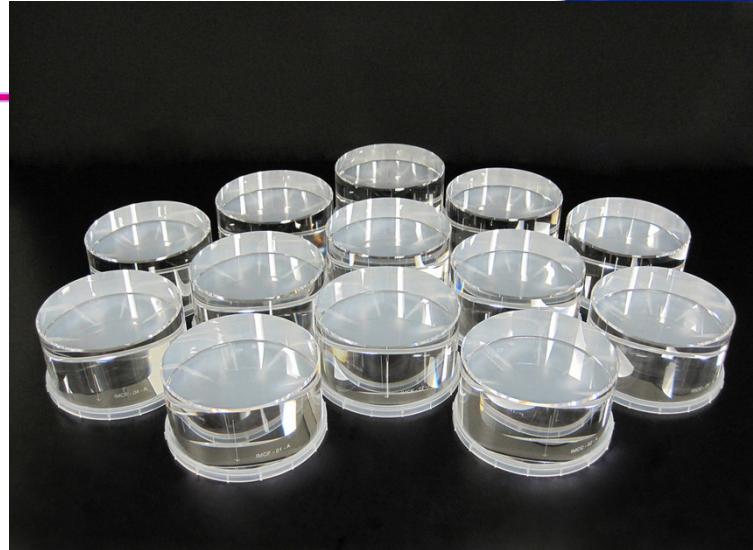


HAM triples

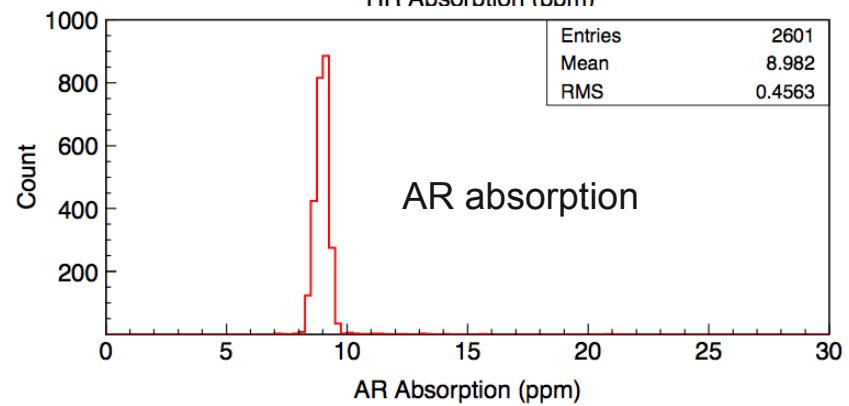
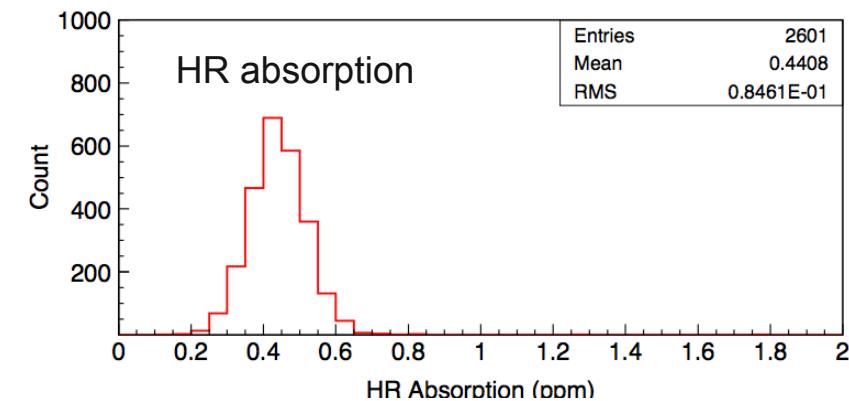
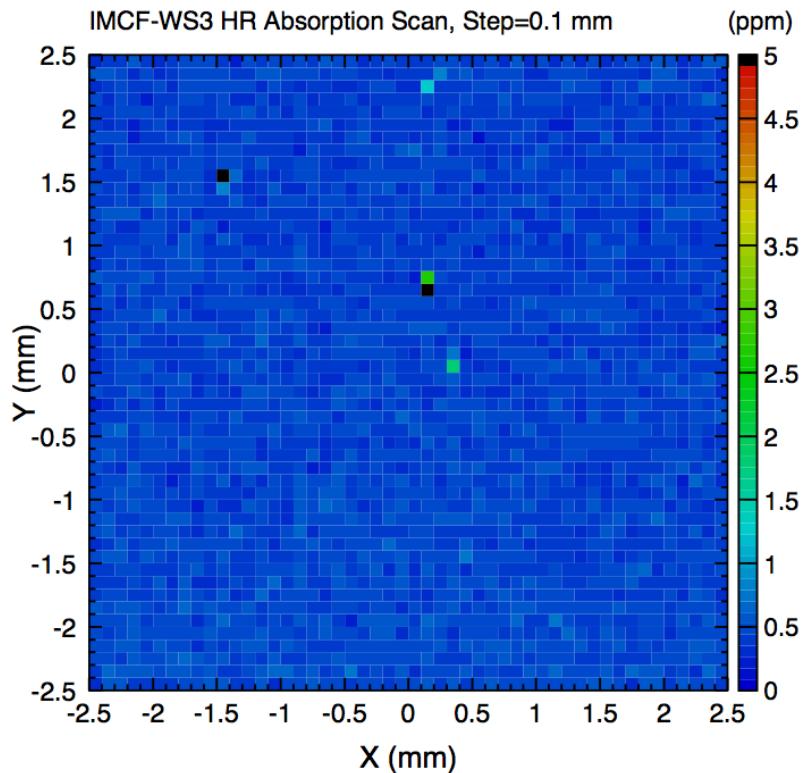


- ☒ Mirrors suspended as 3 pendulums in series for seismic isolation, control
- ☒ Mirrors 15 cm diameter x 7.5 cm thick -- 3 kg
- ☒ 12x heavier than iLIGO, to limit radiation pressure noise





MCF-WS3 witness sample absorption scan



IMC mirror phase maps

Measurement Parameters

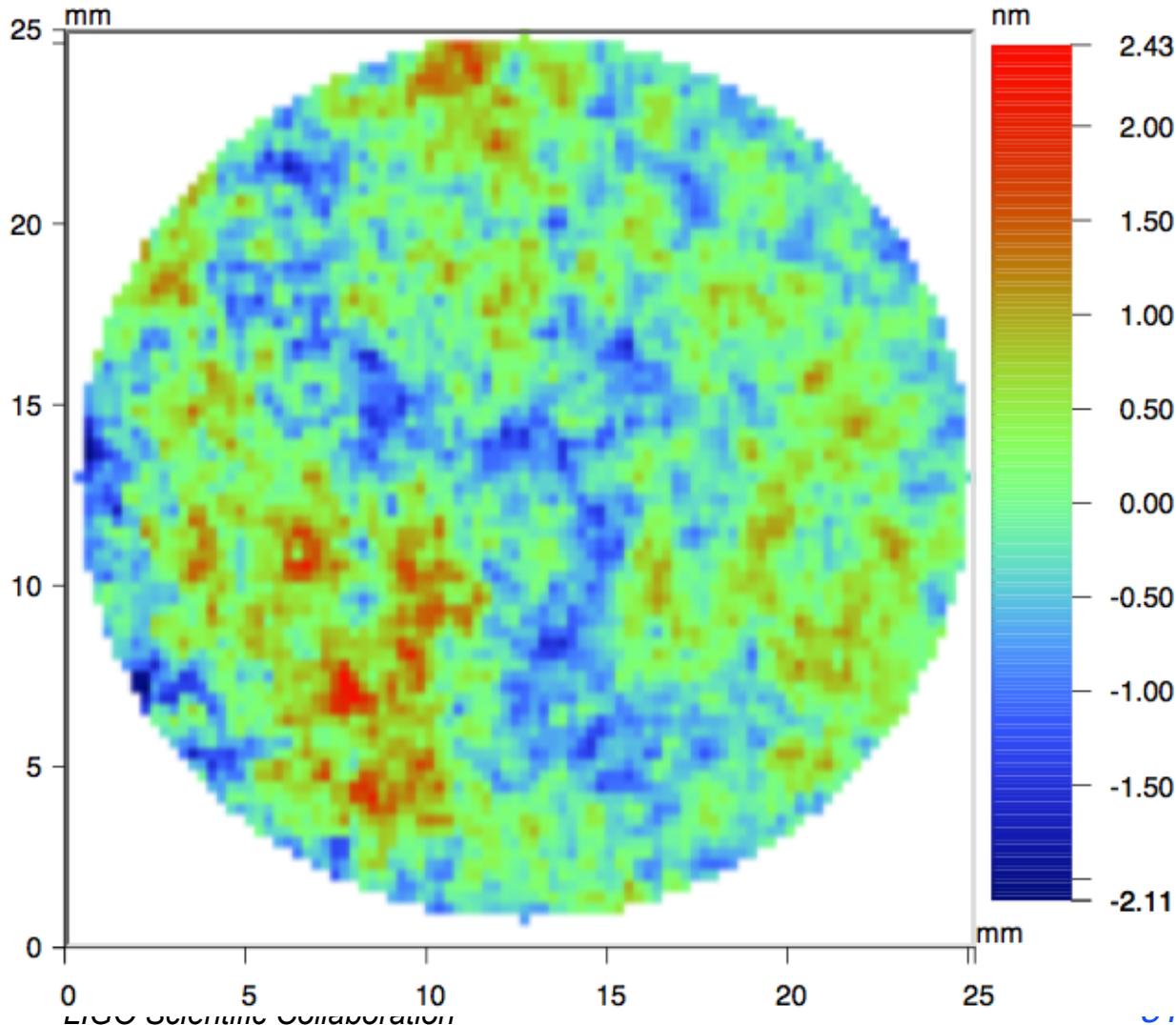
File:	WYK36
Wavelength	1.06 um
Wedge	0.50
X/YSize	96 X 83
Pixel size	265.05 um
Date	09/22/2010
Time	13:40:08
Averages	16

Analysis Results

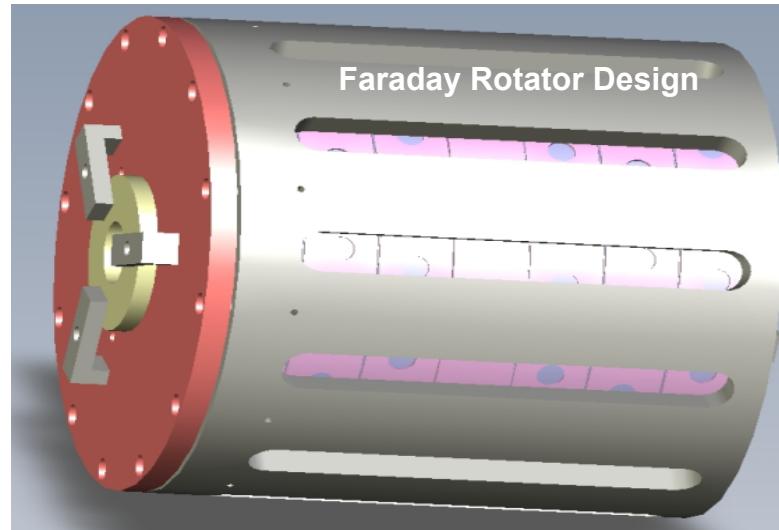
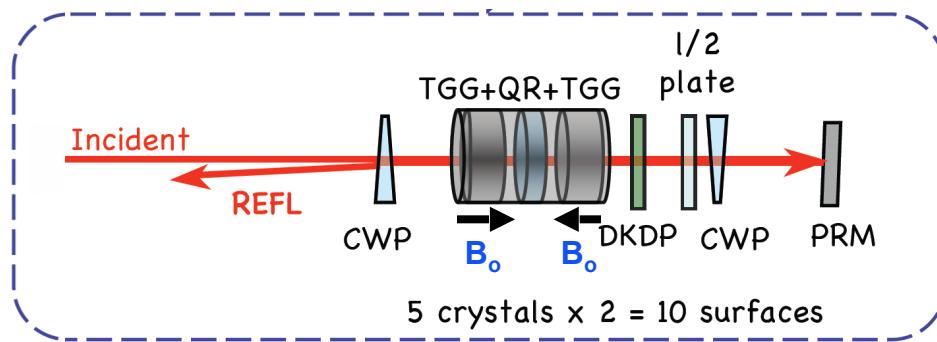
Ra	0.457 nm
Rms	0.574 nm
20 Pt. PV	3.431 nm
2 Pt. PV	4.54 nm

Analysis Parameters

Terms	Tilt Power Astig
Masks:	Det Anl Trm Masks
Filtering	DBP (0.04/2/mm)
Data Restore	Yes
Valid Points	5895



- IAP/UF design and construction
- Passively compensated (for depolarization and thermal lensing)
- Consists of 2x calcite polarizers, 2x TGG crystals, quartz rotator, $\lambda/2$ plate and $-dn/dT$ DKDP thermal compensator
- Observed >50 dB isolation (in lab)
- Faraday installed in enhanced LIGO
- 25 dB isolation, 1-18 W.
- 20 μ rad REFL drift.

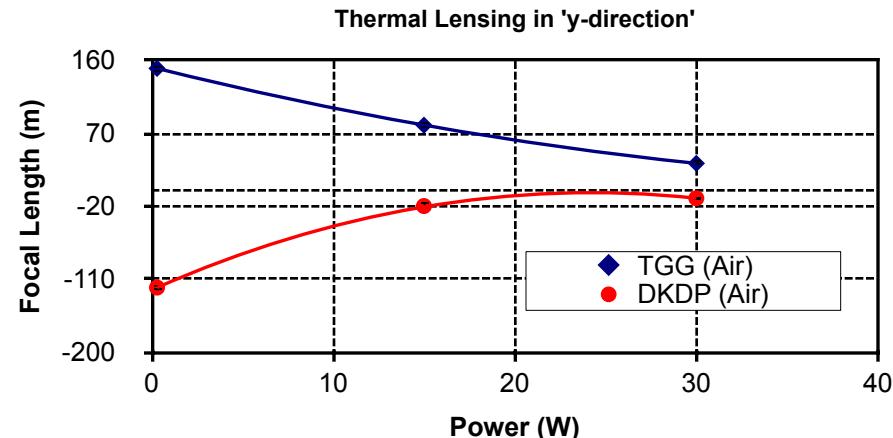
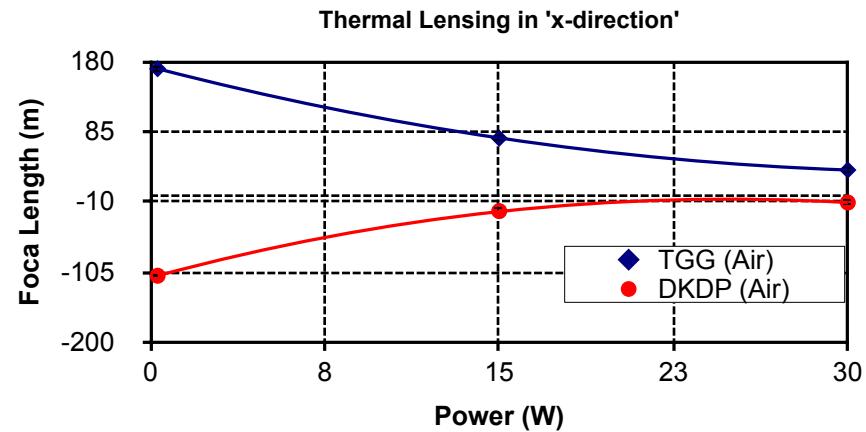
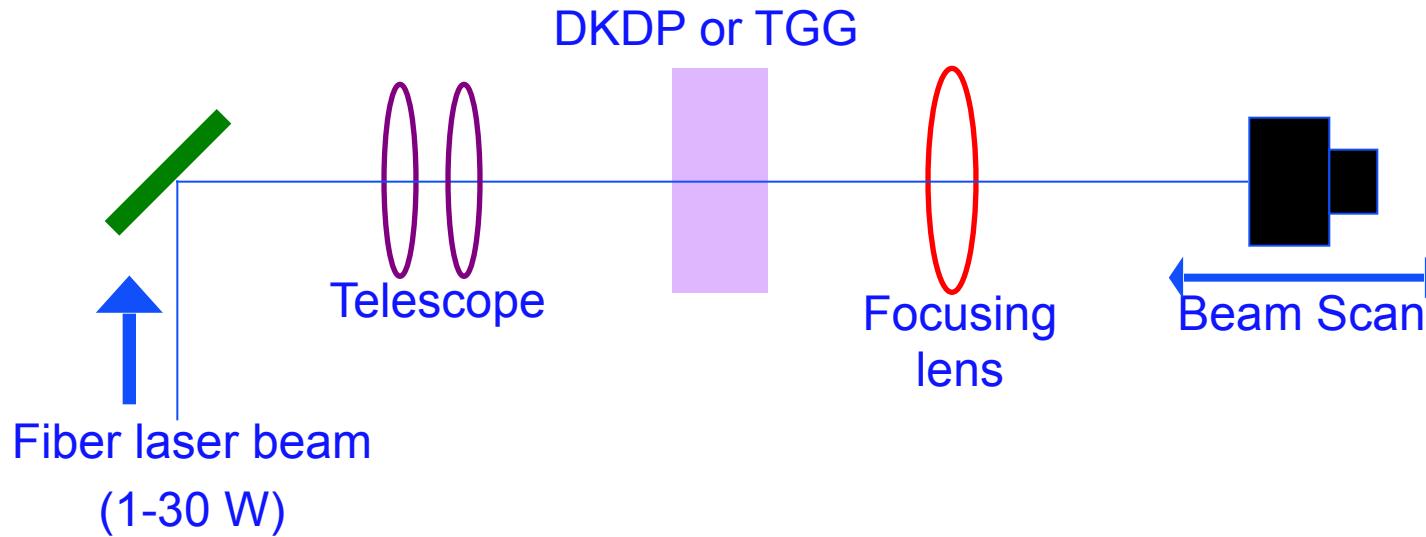


IAP = Institute of Applied Physics, Nizhny Novgorod

TGG = terbium-gallium garnet

DKDP = deuterated potassium dihydrogen phosphate, KD_2PO_4

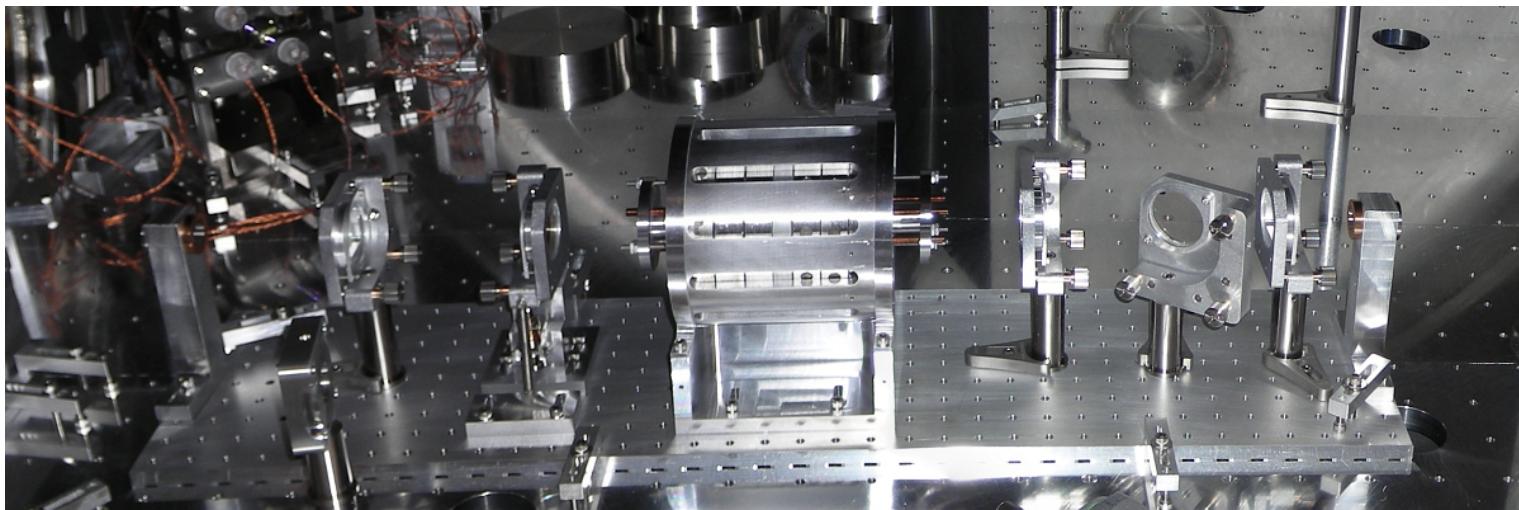
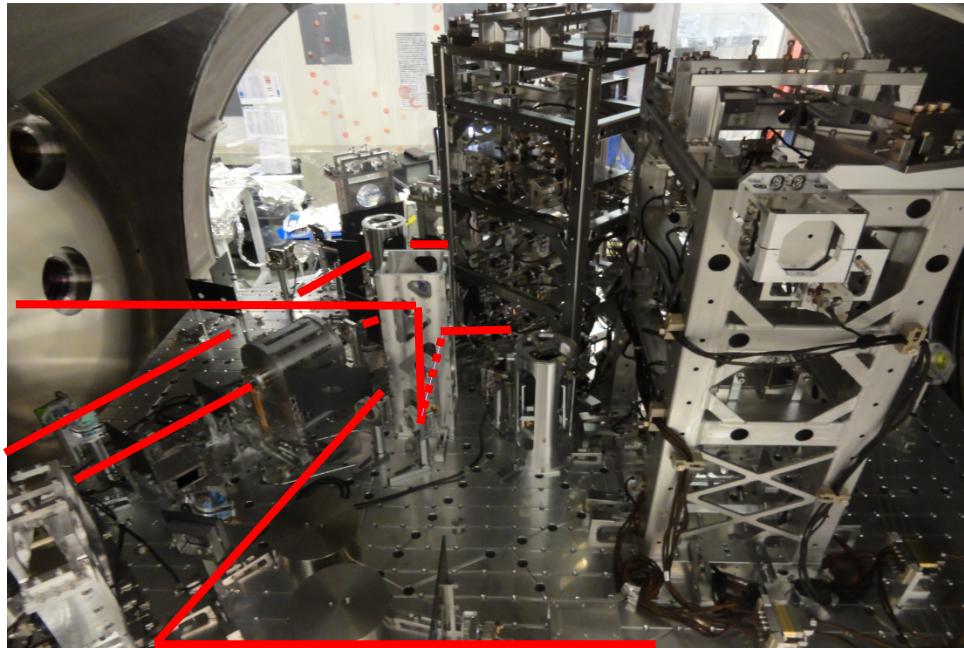
Thermal lens created by TGG and DKDP



Faraday isolator

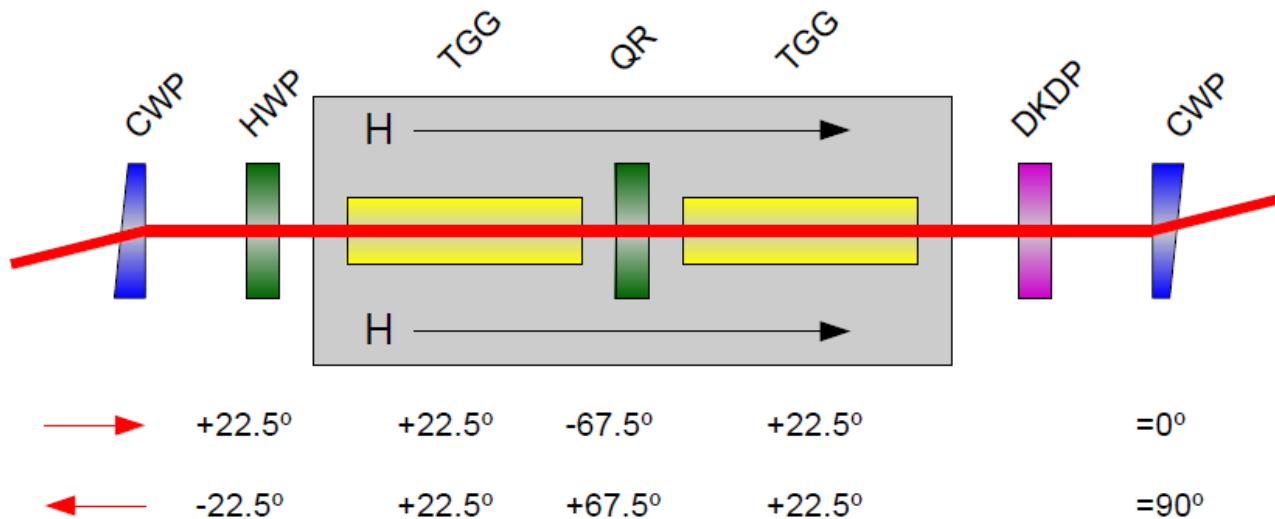


Palashov et al JOSA B (2012)

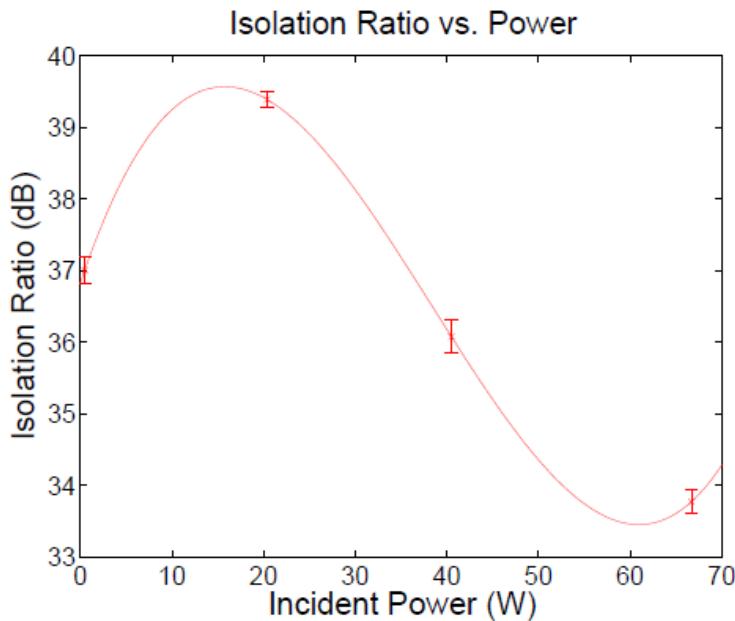


Faraday design

- Same as eLIGO except for removal of the thin film polarizer.
- Calcite wedge polarizers for low loss and high isolation.
- Double TGG with quartz rotator design for thermal depolarization compensation.
- DKDP (negative dn/dT) for thermal lens compensation.
- Half wave plate is adjustable from the control room.



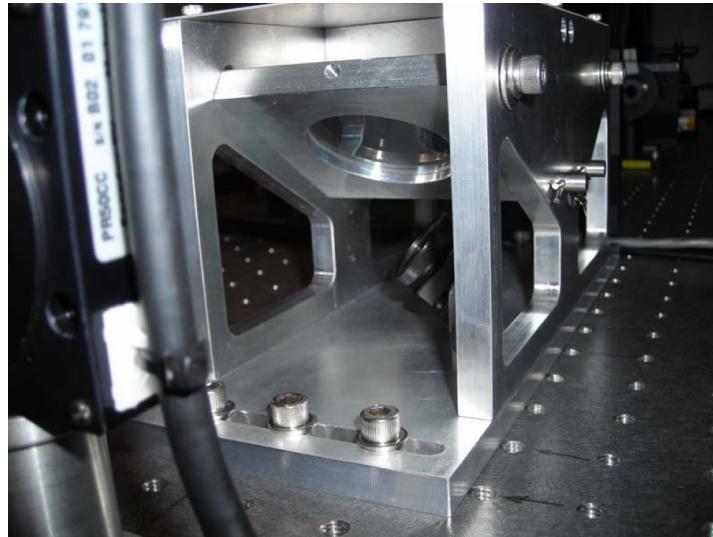
- Stress induced linear birefringence is the strongest effect with temperature
- The beam is rotated with a quartz rotator between the two TGG crystals to compensate partially for the linear birefringence.
- The FI is optimized for isolation at 20 W.



iLIGO[5]	26 dB
eLIGO[5]	35 dB

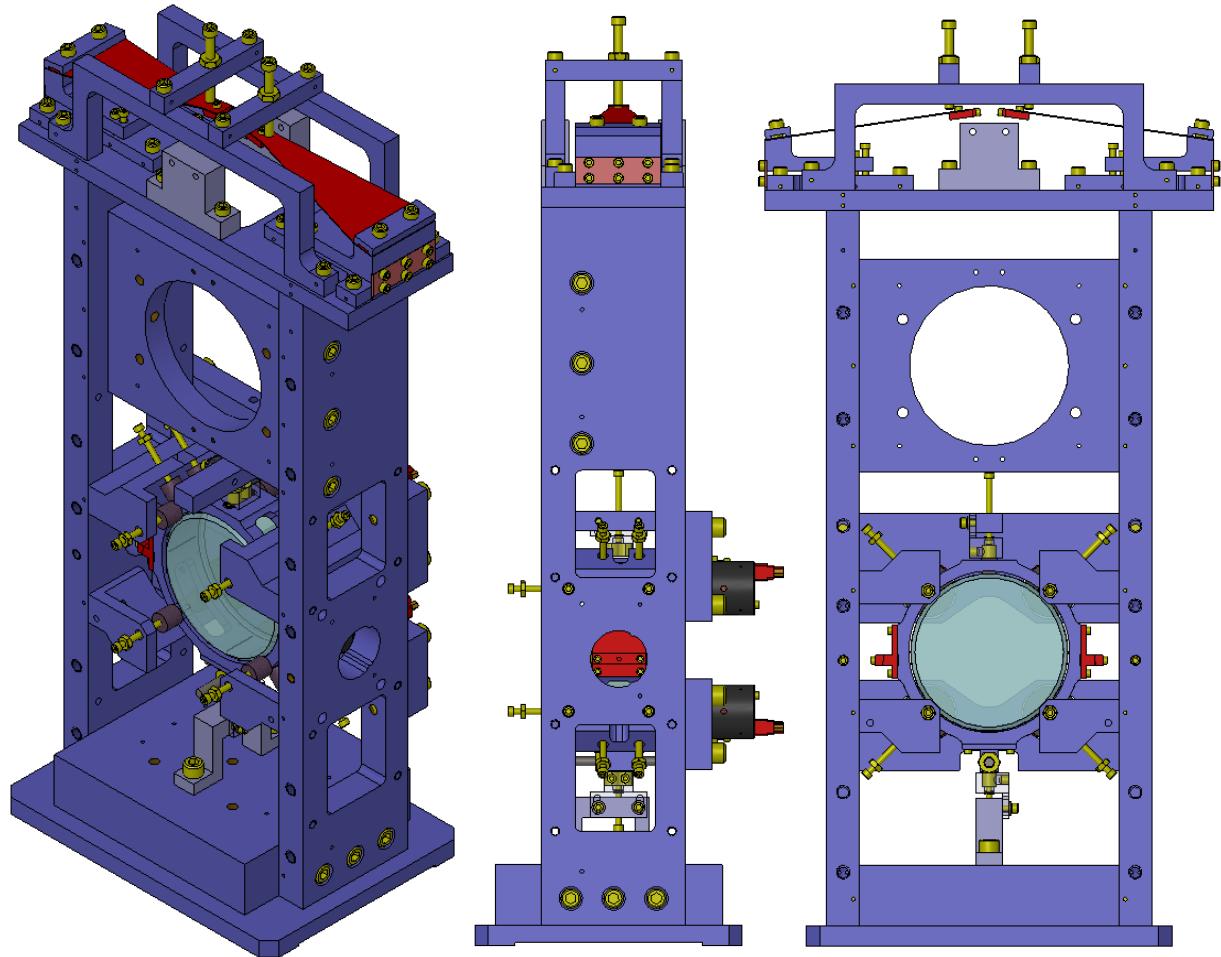
Other items

- Power control: motorized waveplate and 2x thin-film polarizers on PSL table, behind EOMs. $T \sim 98\%$. Extinction ratio 140,000:1
- Mode-matching to IMC: 2 lens telescope on PSL table
- Periscope: Oil derrick
- HAM Aux
-

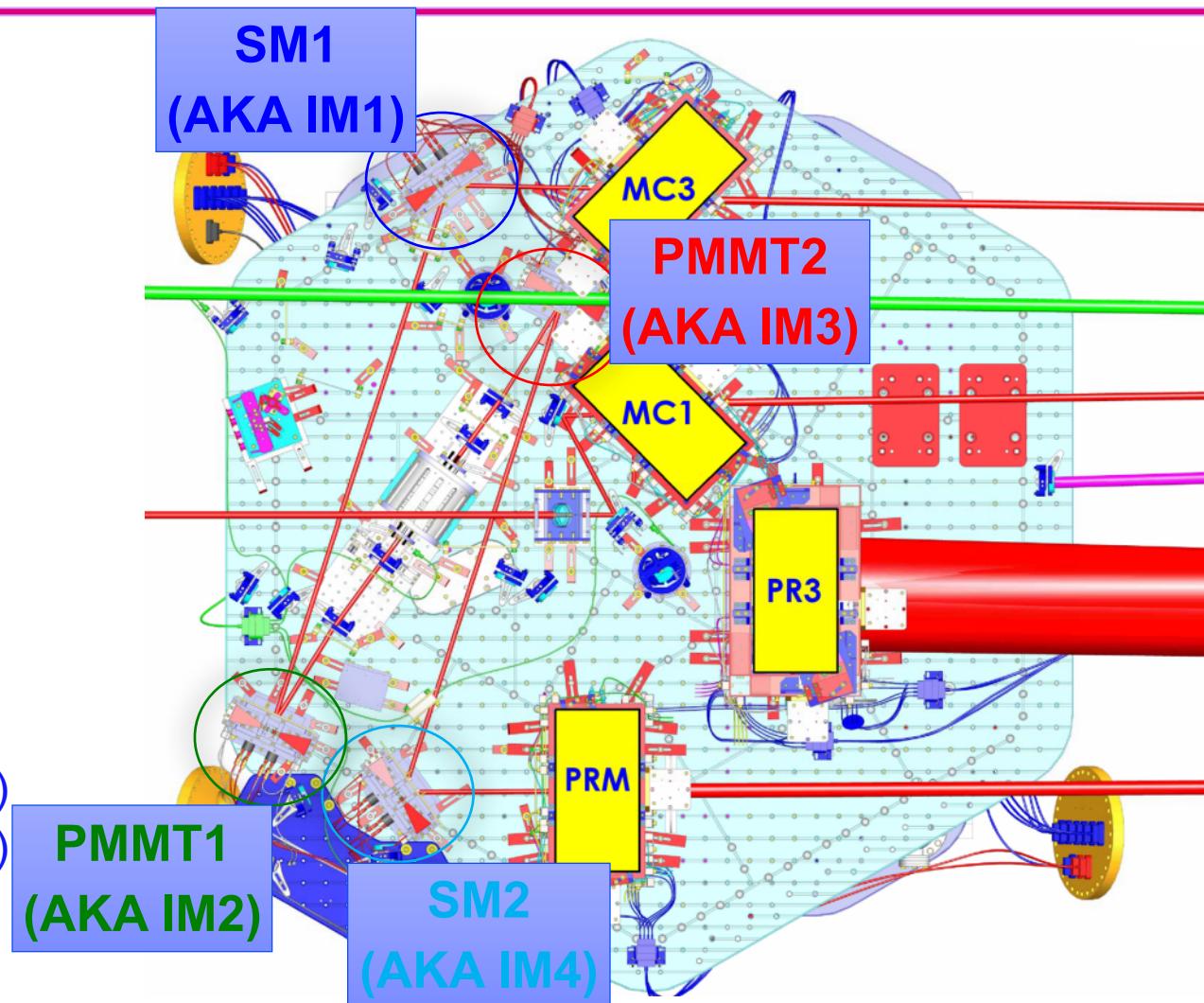


PSL = pre-stabilized laser;
EOM = electro-optic modulator
IMC = input mode cleaner
HAM = vacuum chamber

- Single stage (outgrowth of SOS)
- 4 OSEMs
- 3 inch optic in an aluminum optic holder
- Blades for vertical isolation
- Eddy current dampers



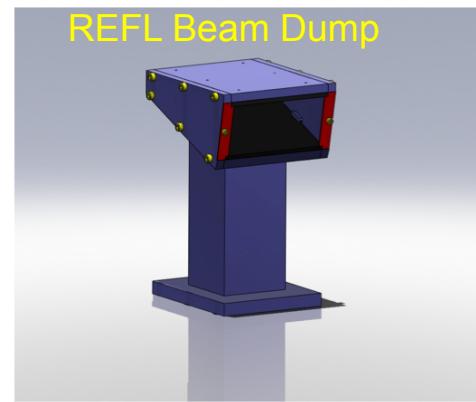
- 4 per IFO, all in HAM2
- They suspend steering and pre-mode-matching mirrors in the IO chain:
 - » SM1 (now IM1)
 - » PMMT1 (now IM2)
 - » PMMT2 (now IM3)
 - » SM2 (now IM4)



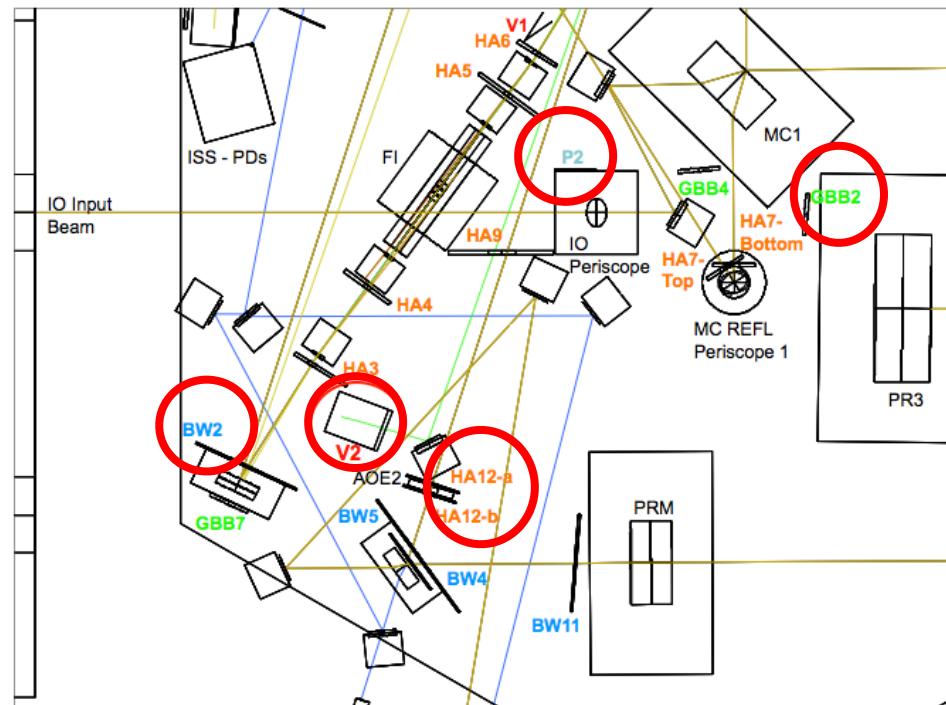
T0900486-v5

- The IO has a high density of high power lasers beams in a very confined space.
 - » It's a very dangerous place...
- The IO baffles serve two purposes:
 - » To prevent scattered light from entering sensing the interferometer and sensing photodiodes
 - » To protect the in-vacuum components from laser damage
- IO Baffle types:
 1. Beam dumps - for parking and dumping high power beams
 2. Suspension baffles - for protecting suspension components
 3. Hard apertures and plates - for protecting other components
 4. Scraper baffles - for collecting small angle scattered light
 5. Ghost beam baffles - for blocking specular reflections from AR coatings and other low power

- Different materials for different power levels
 - » High power absorbing beam dumps: superpolished SiC @ Brewster angle
 - » High power ‘protectors’: unpolished SiC
 - » Low/medium power (< 5 W): porcelain-coated stainless steel
 - » Very low power (< 500 mW): absorbing black glass



Baffles in HAM2



Some key sources for IO:

- *P1500076*
- *E1201013*
- *G1200911*
- *G060185*
- *G070680*

