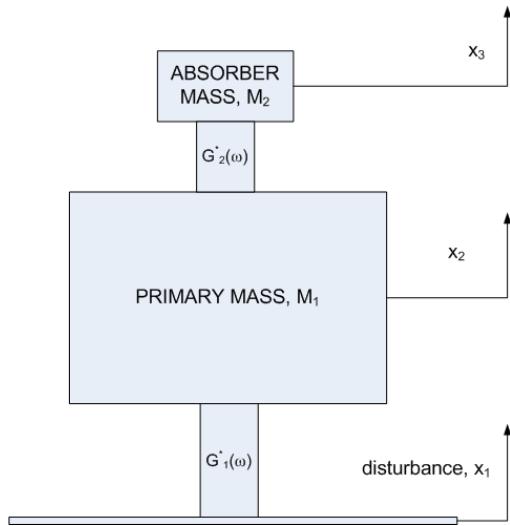


NMBD Dynamic Vibration Absorber

Derived from appendix T080194, and applied to the Non-Magnetic Blade-spring Damper (NMBD) for the Quad UIM internal blade-spring mode



coupled two-mass oscillator derivation

following J.C. Snowdon, Vibration and Shock in Damped Mechanical Systems, John Wiley & Sons, cr 1968, section 4.2, pp. 80-83.

derivation

The derivation below corrects Snowdon's equations. Snowdon's formulation for the amplitude of the transfer function from ground to primary mass motion is correct, but his real and imaginary terms are incorrect.

```
(Debug) In[1]:= eqn1[t_] := M1 x2''[t] - k1 G1[\omega] (x1[t] - x2[t]) + k2 G2[\omega] (x2[t] - x3[t]);  
  
(Debug) In[2]:= eqn3 = LaplaceTransform[eqn1[t], t, s] /.  
  {x1'[0] \rightarrow 0, x1[0] \rightarrow 0, LaplaceTransform[x1[t], t, s] \rightarrow \bar{x1}[s],  
   x2'[0] \rightarrow 0, x2[0] \rightarrow 0, LaplaceTransform[x2[t], t, s] \rightarrow \bar{x2}[s],  
   x3'[0] \rightarrow 0, x3[0] \rightarrow 0, LaplaceTransform[x3[t], t, s] \rightarrow \bar{x3}[s]}  
  
(Debug) Out[2]= s^2 M1 \bar{x2}[s] - k1 \bar{x1}[s] G1[\omega] + k1 \bar{x2}[s] G1[\omega] + k2 \bar{x2}[s] G2[\omega] - k2 \bar{x3}[s] G2[\omega]  
  
(Debug) In[3]:= eqn2[t_] := M2 x3''[t] - k2 G2[\omega] (x2[t] - x3[t]);
```

```
(Debug) In[4]:= eqn4 = LaplaceTransform[eqn2[t], t, s] /.
  {x1'[0] → 0, x1[0] → ξ, LaplaceTransform[x1[t], t, s] → x̄1[s],
   x2'[0] → 0, x2[0] → 0, LaplaceTransform[x2[t], t, s] → x̄2[s],
   x3'[0] → 0, x3[0] → 0, LaplaceTransform[x3[t], t, s] → x̄3[s]}

(Debug) Out[4]= s^2 M2 x̄3[s] - k2 x̄2[s] G2[ω] + k2 x̄3[s] G2[ω]

(Debug) In[5]:= soln = Solve[{eqn3 == 0, eqn4 == 0}, {x̄2[s], x̄3[s]}]
(Debug) Out[5]= { {x̄2[s] → -((k1 x̄1[s] G1[ω] (s^2 M2 + k2 G2[ω])) /
  (k2^2 G2[ω]^2 - (s^2 M2 + k2 G2[ω]) (s^2 M1 + k1 G1[ω] + k2 G2[ω])), x̄3[s] → ((k1 k2 x̄1[s] G1[ω] G2[ω]) / (s^4 M1 M2 + s^2 k1 M2 G1[ω] +
  s^2 k2 M1 G2[ω] + s^2 k2 M2 G2[ω] + k1 k2 G1[ω] G2[ω]) )} }
```

(Debug) In[6]:= T[ω_] := Simplify[x̄2[s] / x̄1[s] /. soln /. s → I ω]

Snowdon's equation 4.7:

```
(Debug) In[7]:= T[ω]
(Debug) Out[7]= { -((k1 G1[ω] (-ω^2 M2 + k2 G2[ω])) /
  (k2^2 G2[ω]^2 - (-ω^2 M2 + k2 G2[ω]) (-ω^2 M1 + k1 G1[ω] + k2 G2[ω]))) }
```

Using the following substitutions / defintions

$$\mu = \frac{M_1}{M_1 + M_2};$$

$$n = \frac{\omega_a}{\omega_0};$$

$$\omega_0 = \sqrt{\frac{k_1 Y_1[\omega_{00}]}{M_1 + M_2}};$$

$$\omega_a = \sqrt{\frac{k_2 Y_2[\omega_{00}]}{M_2}};$$

$$\Omega = \frac{\omega}{\omega_0};$$

and the following notation for the complex modulus :

```
(Debug) In[8]:= G1[ω_] := Y1(1 + I δ1);
G2[ω_] := Y2(1 + I δ2);
```

The expression for the transfer function is as follows:

(Debug) In[10]:= T[ω]

```
(Debug) Out[10]= { (k1 Y1(-I + δ1) (ω^2 M2 + k2 Y2(-1 - I δ2))) / (k1 Y1(-I + δ1) (ω^2 M2 + k2 Y2(-1 - I δ2)) +
  ω^2 k2 M2 Y2(-I + δ2) + ω^2 M1(I ω^2 M2 + k2 Y2(-I + δ2))) }
```

Transfer function,: Real Numerator Term

```
(Debug) In[11]:= R_N = FullSimplify[Re[Expand[T[w][[1, {1, 2, 3, 4}]]]],
{k1, k2, Y1, Y2, δ1, δ2, μ, w0, wa, Ω, ω, M1, M2} ∈ Reals]
(Debug) Out[11]=  $k_1 Y_1 (\omega^2 M_2 \delta_1 - k_2 Y_2 (\delta_1 + \delta_2))$ 

(Debug) In[12]:= c = -n^2 / (k1 k2 Y1 Y2)
(Debug) Out[12]=  $-\frac{n^2}{k_1 k_2 Y_1 Y_2}$ 

(Debug) In[13]:= Simplify[c R_N]
(Debug) Out[13]=  $n^2 \left( \left( 1 - \frac{\omega^2 M_2}{k_2 Y_2} \right) \delta_1 + \delta_2 \right)$ 

(Debug) In[14]:= Simplify[Expand[c R_N] //. ω^2 n^2 M2 / (k2 Y2) → Ω^2 (Y_a / Y2)]
(Debug) Out[14]=  $\left( n^2 - \frac{\Omega^2 Y_a}{Y_2} \right) \delta_1 + n^2 \delta_2$ 
```

This is the same as Snowdon's Equation 4.13 for I_N

Transfer function,: Imaginary Numerator Term

```
(Debug) In[15]:= I_N = FullSimplify[Im[Expand[T[w][[1, {1, 2, 3, 4}]]]],
{k1, k2, Y1, Y2, δ1, δ2, μ, w0, wa, Ω, ω, M1, M2} ∈ Reals]
(Debug) Out[15]=  $-k_1 Y_1 (\omega^2 M_2 + k_2 Y_2 (-1 + \delta_1 \delta_2))$ 

(Debug) In[16]:= Simplify[c I_N]
(Debug) Out[16]=  $n^2 \left( -1 + \frac{\omega^2 M_2}{k_2 Y_2} + \delta_1 \delta_2 \right)$ 

(Debug) In[17]:= Simplify[Expand[c I_N] //. ω^2 n^2 M2 / (k2 Y2) → Ω^2 (Y_a / Y2)]
(Debug) Out[17]=  $\frac{\Omega^2 Y_a}{Y_2} + n^2 (-1 + \delta_1 \delta_2)$ 
```

This is the negative of Snowdon's Equation 4.12 for R_N

Transfer function,: Real Denominator Term

```
(Debug) In[18]:= R_D = FullSimplify[Re[1/T[w][[1, 5]]],
{k1, k2, Y1, Y2, δ1, δ2, μ, w0, wa, Ω, ω, M1, M2} ∈ Reals]
(Debug) Out[18]=  $\omega^2 k_2 (M_1 + M_2) Y_2 \delta_2 + k_1 Y_1 (\omega^2 M_2 \delta_1 - k_2 Y_2 (\delta_1 + \delta_2))$ 

(Debug) In[19]:= Simplify[c R_D]
(Debug) Out[19]=  $-\left( \left( n^2 (\omega^2 k_2 (M_1 + M_2) Y_2 \delta_2 + k_1 Y_1 (\omega^2 M_2 \delta_1 - k_2 Y_2 (\delta_1 + \delta_2))) \right) / (k_1 k_2 Y_1 Y_2) \right)$ 
```

```
(Debug) In[20]:= FullSimplify[Expand[Expand[c RD] //.
{ω^2 (M1 + M2) → (k1 Y1) Ω^2 (Y0 / Y1), ω^2 n^2 M2 / (k2 Y2) → Ω^2 (Ya / Y2)}]] //.
{ω^2 (M1 + M2) → (k1 Y1) Ω^2 (Y0 / Y1), ω^2 n^2 M2 / (k2 Y2) → Ω^2 (Ya / Y2)}]
(Debug) Out[20]= 
$$\left(n^2 - \frac{\Omega^2 Y_a}{Y_2}\right) \delta_1 + \frac{n^2 \left(-\Omega^2 Y_0 + Y_1\right) \delta_2}{Y_1}$$

```

This is the Snowdon's Equation 4.15 for I_D

Transfer function,: Imaginary Denominator Term

```
(Debug) In[21]:= ID = FullSimplify[Im[1/T[ω][[1, 5]]], {k1, k2, Y1, Y2, δ1, δ2, μ, w0, wa, Ω, ω, M1, M2} ∈ Reals]
(Debug) Out[21]= -ω2 k2 M2 Y2 + M1 (w4 M2 - ω2 k2 Y2) - k1 Y1 (ω2 M2 + k2 Y2 (-1 + δ1 δ2))

(Debug) In[22]:= Collect[Expand[c ID] //.
{ω^2 M1 / (k1 Y1) + ω^2 M2 / (k1 Y1) → Ω^2 (Y0 / Y1), ω^2 n^2 M2 / (k2 Y2) → Ω^2 (Ya / Y2),
n^2 ω^4 M1 M2 / (k1 k2 Y1 Y2) → μ Ω^4 (Y0 / Y1) (Ya / Y2)}, n] //.
{ω^2 M1 / (k1 Y1) + ω^2 M2 / (k1 Y1) → Ω^2 (Y0 / Y1)}
(Debug) Out[22]= 
$$\frac{\Omega^2 Y_a}{Y_2} - \frac{\mu \Omega^4 Y_0 Y_a}{Y_1 Y_2} + n^2 \left(-1 + \frac{\Omega^2 Y_0}{Y_1} + \delta_1 \delta_2\right)$$

```

This is the negative of Snowdon's Equation 4.14 for R_D

coupled two-mass oscillator formulation

Same formulation as above but restated without subscripts.

general transmissibility equation

The UIM blade spring (D060237) has a mass of .367 kgm. I'll assume ~1/2 of this mass is involved in the 1st resonance.

The mass of the NMBD involved in its 1st elastic mode is ~2 x the mass of the dumb-bells (D1400296)
= 2 x 17 = 34 gm

See NMBD damping results in T1600046

```
(Debug) In[50]:= .055 / M1
(Debug) Out[50]= 0.299728

(Debug) In[23]:= n = wa / w0;
M1 = .367 / 2;
M2 = eps M1;
μ = M1 / (M1 + M2);
```

```
(Debug) In[27]:= d1[w_] := 1/720;
d2[w_] := d;
Y1[w_] := w0^2 (M1 + M2);
Y2[w_] := wa^2 M2;
```

Variables:

d = loss factor

eps = damping mass to primary mass ratio, M2/M1

wa = natural frequency of the damping element by itself, rad/sec

w0 = natural frequency of the primary mass without the damping element added, rad/sec

The total mass of the NMBD = 55 gm. However the mass of the dumb-bells involved in its 1st mode is ~34gm

So eps = .034/M1 = 0.185

wa was estimated in T1500237 to be ~120 Hz (indirectly by fitting to some data)

However using viton elastic stiffness, the cross-sectional area of the viton spring and the dumbbell mass, one gets wa = 344 Hz

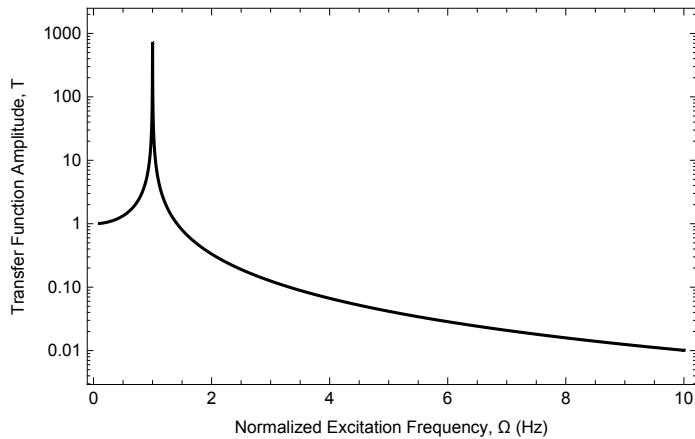
From T1600046, w0 = 110 Hz and d1 = 1/720

```
(Debug) In[31]:= IN[w_] := (w/w0)^2 (Y2[wa]/Y2[w]) - n^2 (1 - d1[w] d2[w]);
RN[w_] := - (w/w0)^2 (Y2[wa]/Y2[w]) d1[w] + n^2 (d1[w] + d2[w]);
ID[w_] := -mu (w/w0)^4 (Y1[w0]/Y1[w]) (Y2[wa]/Y2[w]) +
(w/w0)^2 (n^2 (Y1[w0]/Y1[w]) + (Y2[wa]/Y2[w])) - n^2 (1 - d1[w] d2[w]);
RD[w_] := - (w/w0)^2 (n^2 (Y1[w0]/Y1[w]) d2[w] + (Y2[wa]/Y2[w]) d1[w]) +
n^2 (d1[w] + d2[w]);
T[w_] := (RN[w] + I IN[w]) / (RD[w] + I ID[w]);
```

NMBD application

case I: UIM blade spring, no damper

```
(Debug) In[74]:= plt1 = LogPlot[Abs[T[\!\(\omega\)]], {w0 -> 2 Pi 110, wa -> 2 Pi 344, d -> 0, eps -> 0}, {Omega, .1, 10}, PlotRange -> All, PlotPoints -> 10000, MaxRecursion -> 15, PlotStyle -> {Black}, Frame -> True, FrameLabel -> {"Normalized Excitation Frequency, \!\(\omega\) (Hz)", "Transfer Function Amplitude, T"}]
```



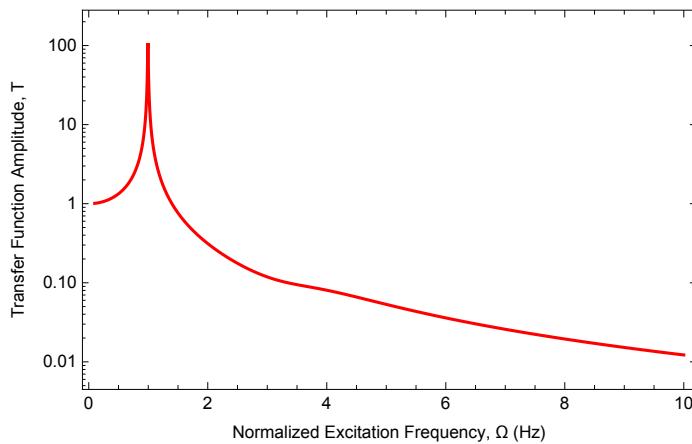
```
(Debug) Out[74]=
```

```
(Debug) In[75]:= FindMaximum[Abs[T[\!\(\omega\)]], {w0 -> 2 Pi 110, wa -> 2 Pi 344, d -> 0, eps -> 0}, {\omega, 10, 500}]
```

```
(Debug) Out[75]= {720.001, {\omega -> 691.15}}
```

case 2: NMBD, wa >> w0, 75 F (23.8 C)

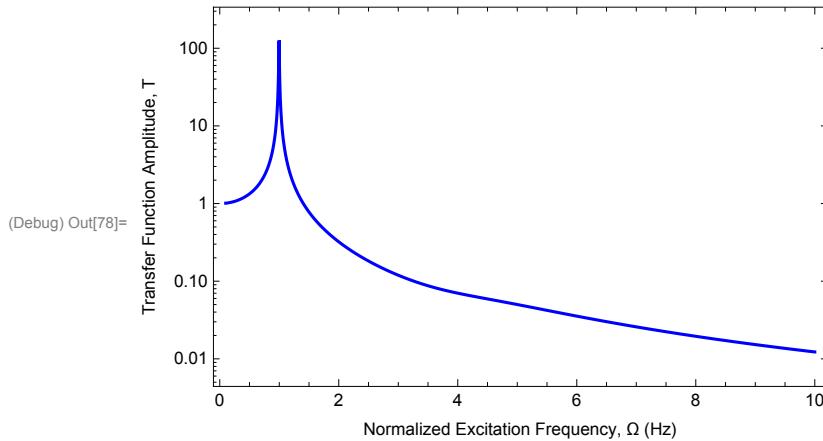
```
(Debug) In[76]:= plt2 =
  LogPlot[Abs[T[\!\(\omega\)]], {w0 -> 2 Pi 110, wa -> 2 Pi 344, d -> .68, eps -> .185},
  {\!\(\omega\), .1, 10}, PlotRange -> All, PlotPoints -> 10000,
  MaxRecursion -> 15, PlotStyle -> {Red}, Frame -> True,
  FrameLabel -> {"Normalized Excitation Frequency, \!\(\omega\) (Hz)",
  "Transfer Function Amplitude, T"}]
```



```
(Debug) Out[76]=
(Debug) In[77]:= FindMaximum[
  Abs[T[\!\(\omega\)]], {w0 -> 2 Pi 110, wa -> 2 Pi 344, d -> 0.68, eps -> 0.185}, {\!\(\omega\), 10, 500}]
(Debug) Out[77]= {102.624, {\!\(\omega\), 687.264}}
```

case 3: NMBD, wa >> w0, 65 F (18.3 C)

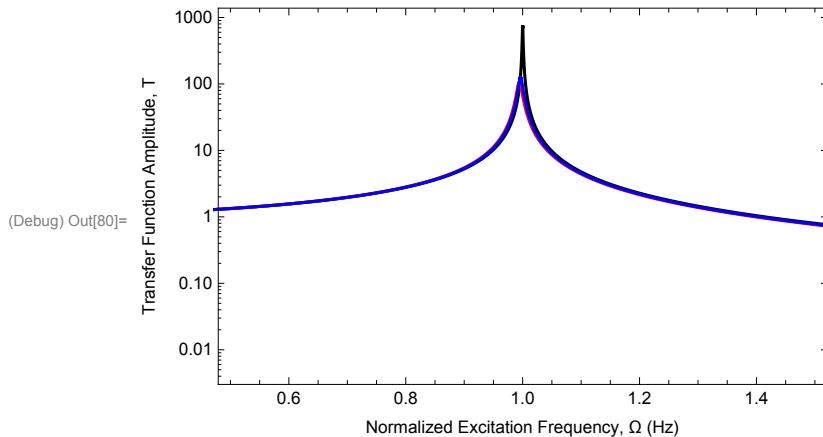
```
(Debug) In[78]:= plt3 = LogPlot[
  Abs[T[\Omega w0]] /. {w0 -> 2 Pi 110, wa -> 2 Pi 344 \ 1.119, d -> .9, eps -> .185},
  {\Omega, .1, 10}, PlotRange -> All, PlotPoints -> 10000,
  MaxRecursion -> 15, PlotStyle -> {Blue}, Frame -> True,
  FrameLabel -> {"Normalized Excitation Frequency, \Omega (Hz)",
  "Transfer Function Amplitude, T"}]
```



```
(Debug) In[79]:= FindMaximum[
  Abs[T[\omega]] /. {w0 \rightarrow 2 Pi 110, wa \rightarrow 2 Pi 344 \ 1.119, d \rightarrow 0.9, eps \rightarrow 0.185}, {\omega, 10, 500}]
(Debug) Out[79]= {121.554, {\omega \rightarrow 688.693}}
```

compare NMBD cases 1,2,3

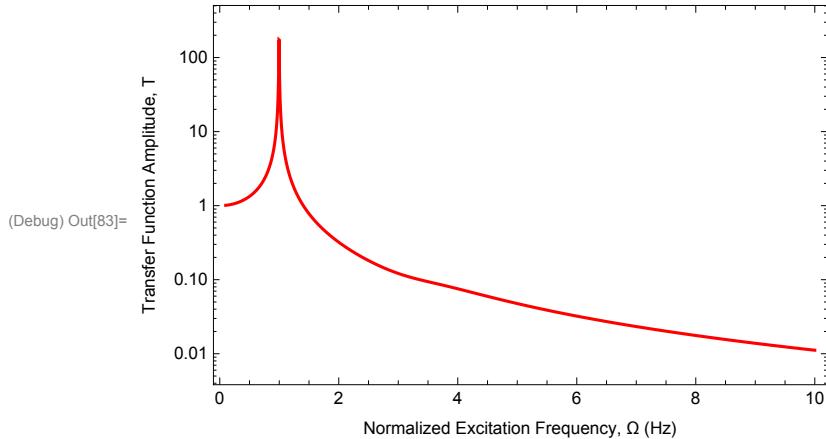
```
(Debug) In[80]:= Show[plt1, plt2, plt3, PlotRange -> {{.5, 1.5}, All}]
```



case 4: NMBD, wa >> w0, 75 F (23.8 C), d & M2 set to match T1600046-v2

Qdamped

```
(Debug) In[83]:= plt4 = LogPlot[
  Abs[T[\Omega w0]] /. {w0 -> 2 Pi 110, wa -> 2 Pi 344, d -> .6, eps -> .185/2},
  {\Omega, .1, 10}, PlotRange -> All, PlotPoints -> 10000,
  MaxRecursion -> 15, PlotStyle -> {Red}, Frame -> True,
  FrameLabel -> {"Normalized Excitation Frequency, \Omega (Hz)",
  "Transfer Function Amplitude, T"}]
```



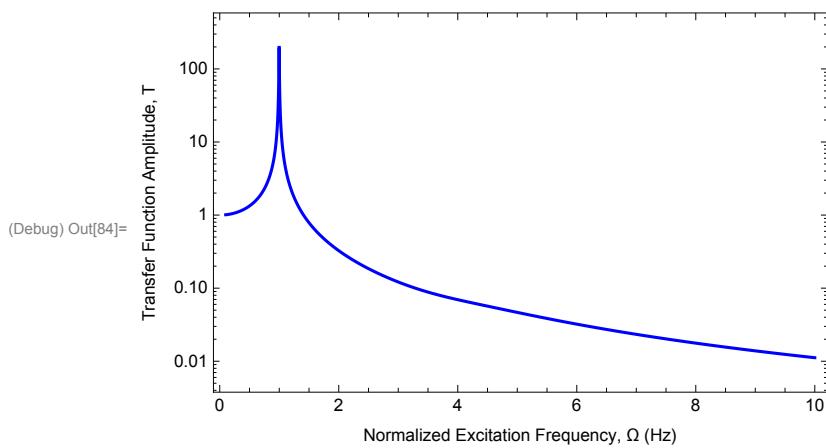
```
(Debug) In[82]:= FindMaximum[
  Abs[T[\omega]] /. {w0 -> 2 Pi 110, wa -> 2 Pi 344, d -> 0.6, eps -> 0.185/2}, {\omega, 10, 500}]
(Debug) Out[82]= {172.987, {\omega -> 688.855}}
```

case 5: NMBD, wa >> w0, 65 F (23.8 C), d & M2 set to match T1600046-v2

Qdamped

Using d & M2 that match T160046-v2 Qdamped at 75F, but then estimating effect of temperature of 65 F, by increasing d by 1.32 factor and increasing wa frequency by 1.119 factor, predicted from Viton-B complex modulus variation with temperature

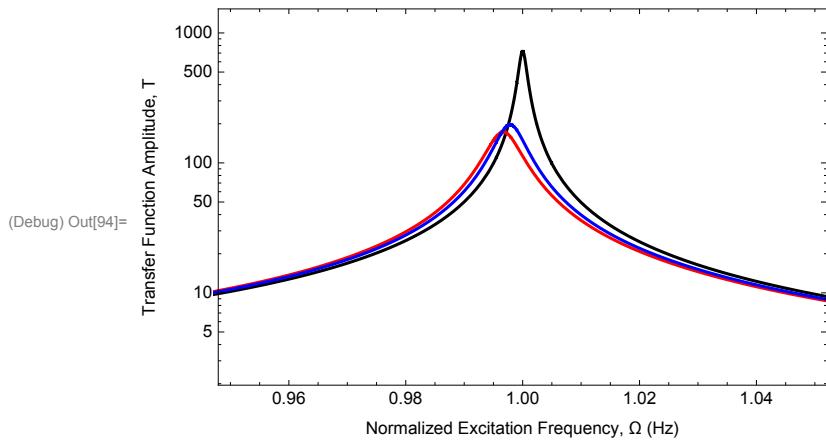
```
(Debug) In[84]:= plt5 = LogPlot[Abs[T[\Omega w0]] /.
  {w0 -> 2 Pi 110, wa -> 2 Pi 344 \ 1.119, d -> .6 \ 1.32, eps -> .185 / 2},
  {\Omega, .1, 10}, PlotRange -> All, PlotPoints -> 10000,
  MaxRecursion -> 15, PlotStyle -> {Blue}, Frame -> True,
  FrameLabel -> {"Normalized Excitation Frequency, \Omega (Hz)",
  "Transfer Function Amplitude, T"}]
```



```
(Debug) In[85]:= FindMaximum[Abs[T[\omega]] /.
  {w0 \rightarrow 2 Pi 110, wa \rightarrow 2 Pi 344 \ 1.119, d \rightarrow 0.6 \ 1.32, eps \rightarrow 0.185 / 2}, {\omega, 10, 500}]
(Debug) Out[85]= {196.895, {\omega \rightarrow 689.656}}
```

compare NMBD cases 1,4,5

```
(Debug) In[94]:= Show[plt1, plt4, plt5, PlotRange -> {{.95, 1.05}, {1, 7}}]
```



```
(Debug) In[96]:= 197 / 173 // N
```

```
(Debug) Out[96]= 1.13873
```

If the NMBD were assembled at 75