# A Calibrated Blackbody Source for Testing Next-Generation Wavefront Actuators

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### Overview

- 1. Project Objectives
- 2. Background (TCS and Adaptive Optics)
- 3. Project design and lab setup
- 4. Theoretical Predictions and Experimental Data
- 5. Validation

# **Project Objectives**

Theoretical incident irradiance profile == experimental results

- -Design and measure a calibrated blackbody source
- -Fit our calibration with data and theoretical calculations (end-to-end validation)
- -Long-term goal
  - 1. Eliminate loss-inducing optical aberrations in test masses
  - 2. Increase resonating laser power and reduce quantum noise floor of aLIGO



Main issues:

- -Static curvature errors
- -Thermally-induced spatial distortions

-Point defects within act as sources of optical error

LIGO-T2200206-v5

### **Test Masses**



### **Current Ring Heaters**

- Fix radius of curvature in center of TM
- Overcompensate further out from center
- More power = more surface deformation closer to the center
- Want to flatten where the ideal gaussian mode hits



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## Adaptive Optics and Wavefront Distortions

Improve the test masses by reducing effects of wavefront distortions

Laser has one mode; an ideal gaussian beam

Parts of laser light scatter and enter higher order modes (HOMs)

Hits point defects in TM

### Wavefront Distortions

- Closer a HOM is to 0-0 mode, the greater the loss
- Eventually, will have a HOM with resonance within the aLIGO arms
- LHO 7<sup>th</sup> order very close to 0-0 resonance

What does this mean for power loss?



Brooks, Vajente, Yamamoto G2000874-v3, 2020

### Power Loss with the Seventh Order Mode

 $Loss_{00,mn} = L_o * Gain_{mn}$ 

- -Single Bounce Scattering
- -Degeneracy between 7<sup>th</sup> order mode and 0-0 mode
- -7<sup>th</sup> OM uses power that should be going towards 0-0 mode
- -Cannot change point defects, must change the optical gain

Comparison of mode sizes on LIGO ITM



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Next Generation Ring heater actuators

-Will address 7<sup>th</sup> OM

0-0 mode has smaller profile, so it will not be affected

-Need to know: transfer of power, confirmation of observations

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### The Setup





### Collimated vs. Reality



### **Initial Calculations**

UNKNOWNS: emissivity, temperature profile

Emissivity  $\varepsilon = 0.57$ 

$$P_{diss} = \varepsilon * A * \sigma_{SB} * (T^4 - T_o^4) = 0.192 \text{ W}$$

T = heater temp (388.15 K)  $T_o$  = atmosphere temp (300.15 K)

A = emitting surface area (4.05e-4 m)  $\sigma_{SB}$  = 5.67e-8 W/m<sup>2</sup>K<sup>4</sup>



Heater when viewed with FLIR



Comsol CAD Geometry

### **Point Source**

### **Cartridge Heater**



## **Power Absorbed Calculations**

Max irradiance  $E_e$  on screen (from Comsol) = 4.64 W/m<sup>2</sup>

Emissivity  $\varepsilon$  = 0.99

$$T = (\frac{E_e}{\varepsilon * \sigma_{SB}} + T_o^4)^{1/4} = 301.32 \text{ K} = 28.3 \text{ C}$$

### Does this match our real data?



IR absorptive screen

### Validation

Running at 1.12 W of input power

Max temperature = 29 °C

Matches temperature of other side!

Clear center hot spot, but no ring shape

#### **Measured Irradiance**



## **Future Applications**

- Testing RH prototypes and spatially complex patterns as soon as parts are fabricated
- Will be able to target single bounce scattering directly
- By 04, will hopefully reduce the effect of point absorbers and move the arm power closer to the design power



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