

The LIGO logo consists of several concentric, curved lines in the top-left corner, resembling a ripple or a stylized 'L'.

LIGO

Post-O5 Thermal Modeling A# TCS requirements

[G2300624](#)

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A# realistic limits: 1000kW and 4% MM SQZ Loss

Realistic limit of configurations explored so far

We're yet to find a robust TCS solution that supports ASharp target performance

Better with Super-TCS, requiring significant improvements in sensing & actuation

A# performance estimates (Preliminary)

Coating Absorption	0.5ppm	1ppm	1.5ppm
SQZ Loss	~4%	7%	7.2%
Arm Power	~1000kW	680kW	450kW

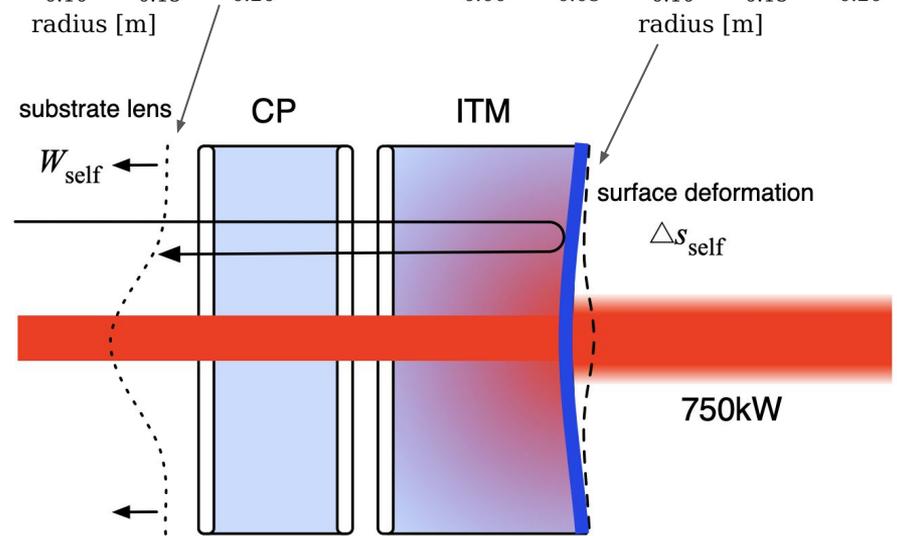
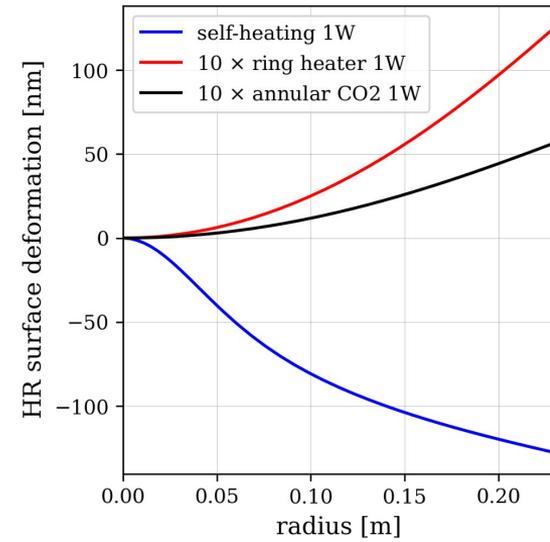
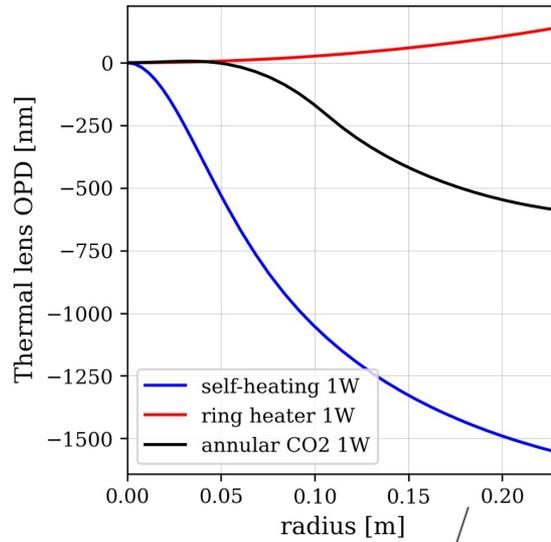
85% TCS correction (6.7x reduction in distortion)
200W of input laser power

Thermal Model

Steady state finite element models for thermo-optic deformations made

Test mass optics assumptions:

- Test mass scaled up from A+ \rightarrow A# proportionally to meet 100 kg
- Compensation plate (CP) diameter scaled up to match test mass, same thickness & separation distance
- 170 mm radius aperture is assumed (no coating outside)
- 2D-axisymmetric thermal equilibrium optical profile used

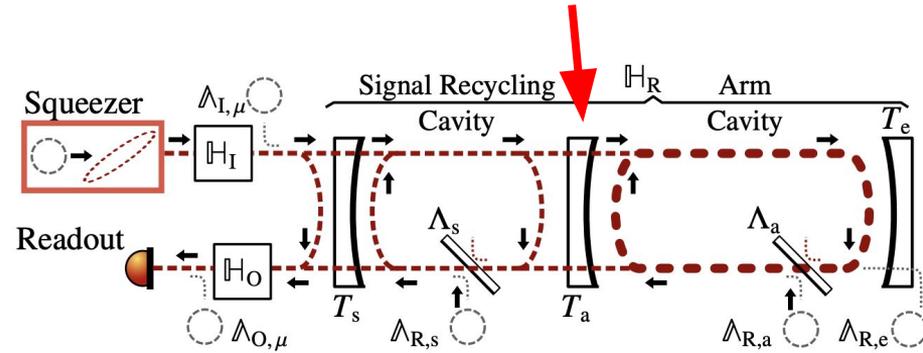
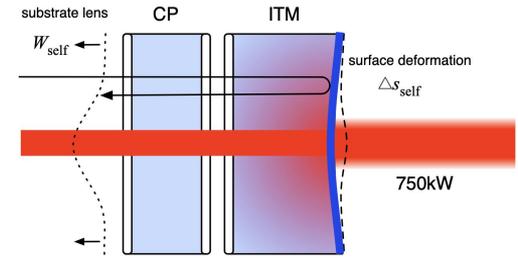


Thermal + Optical model

Full interferometer model is hard to interpret so we start the study with looking at the **PRC+ARM** and **SRC+ARM** separately and ask

How do we optimise TCS for:

- Maximum power buildups (CARM)
 - Power recycling gain (PRG)
 - Arm cavity gain
- Minimise squeezing losses (DARM)
 - Reduce higher order mode losses
 - Mis-rotation of the squeezed state



$$\theta(\Omega) = (\arg(\mathfrak{h}(+\Omega)) + \arg(\mathfrak{h}(-\Omega)))/2, \quad (52)$$

$$\eta(\Omega) = (|\mathfrak{h}(+\Omega)|^2 + |\mathfrak{h}(-\Omega)|^2)/2, \quad (53)$$

$$\Xi(\Omega) = (|\mathfrak{h}(+\Omega)| - |\mathfrak{h}(-\Omega)|)^2/4\eta. \quad (54)$$

Model the upper and lower sideband transfer functions in FINESSE/SIS to get the squeezed state response

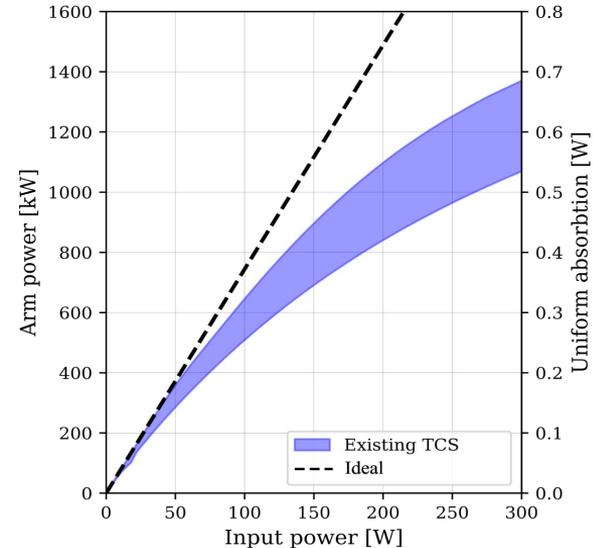
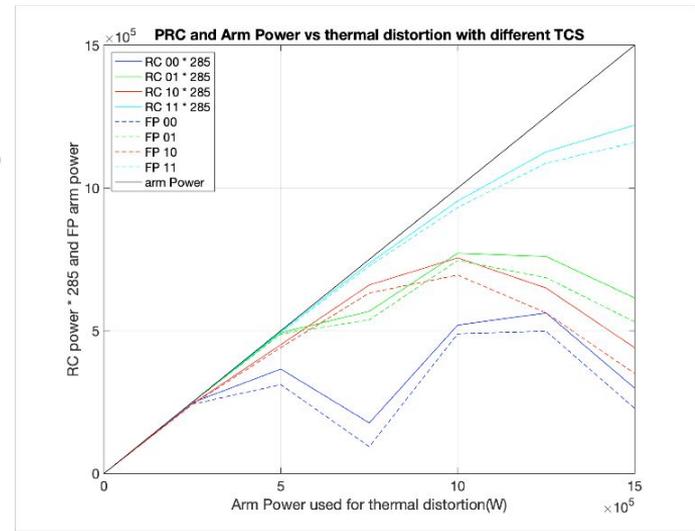
See paper *LIGO's quantum response to squeezed states*

Initial findings: Power build-up

Optimising for maximum power buildup and minimised squeezing losses is not always the same TCS settings.

- **Power buildups sensitive to spot-size weighted thermal-lens and surface deformations in PRC+ARM**
- But, squeezing losses sensitive to full aperture distortions due to higher order modes resonating in the SRC

Overall we need to reduce wavefront distortion across the full aperture! A challenging TCS problem...

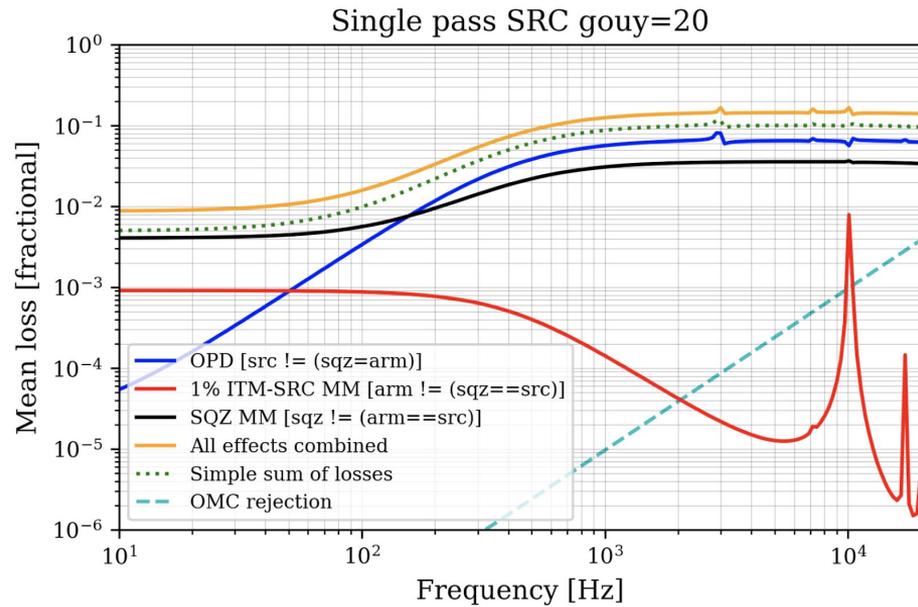


Initial findings: SRC loss

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SRC-ARM mismatch (coupling to HOM2) is not a big issue

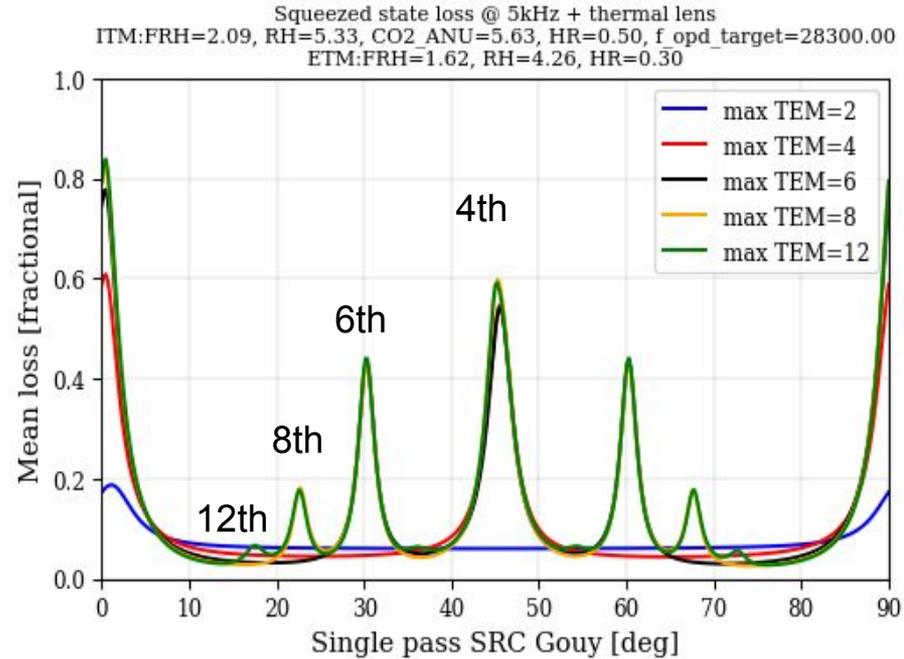
Higher order mode substrate scatter has the biggest effect on squeezing at high frequencies

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SRC gouy phase determines which HOM resonates and give high frequency losses

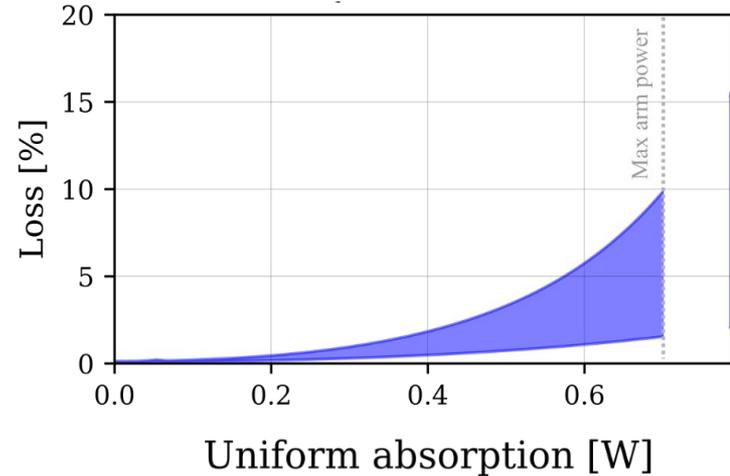
aLIGO SRC is around 20 degrees, which can change with thermal lensing state

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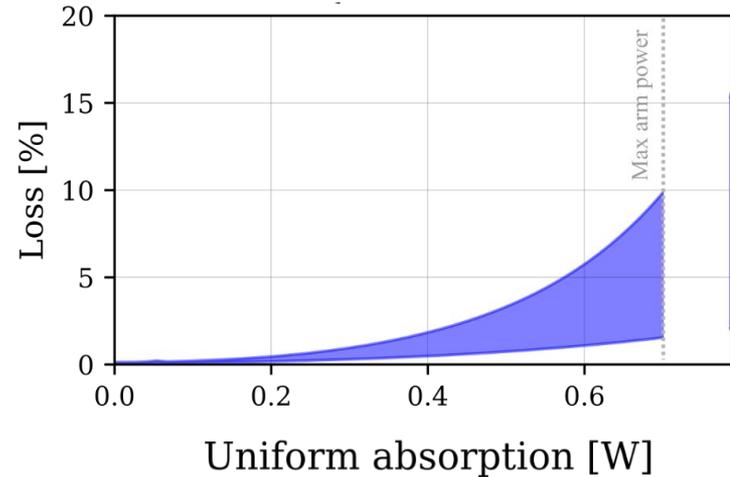
- **SQZ loss** at 500 Hz can range between 2% - 10% depending initial cold state static lens
- **Misrotation**: maximum ~ 1.5 degree @ 500 Hz
- **Dephasing**: 0.04 mrad @ 500 Hz
→ small misrotation and dephasing

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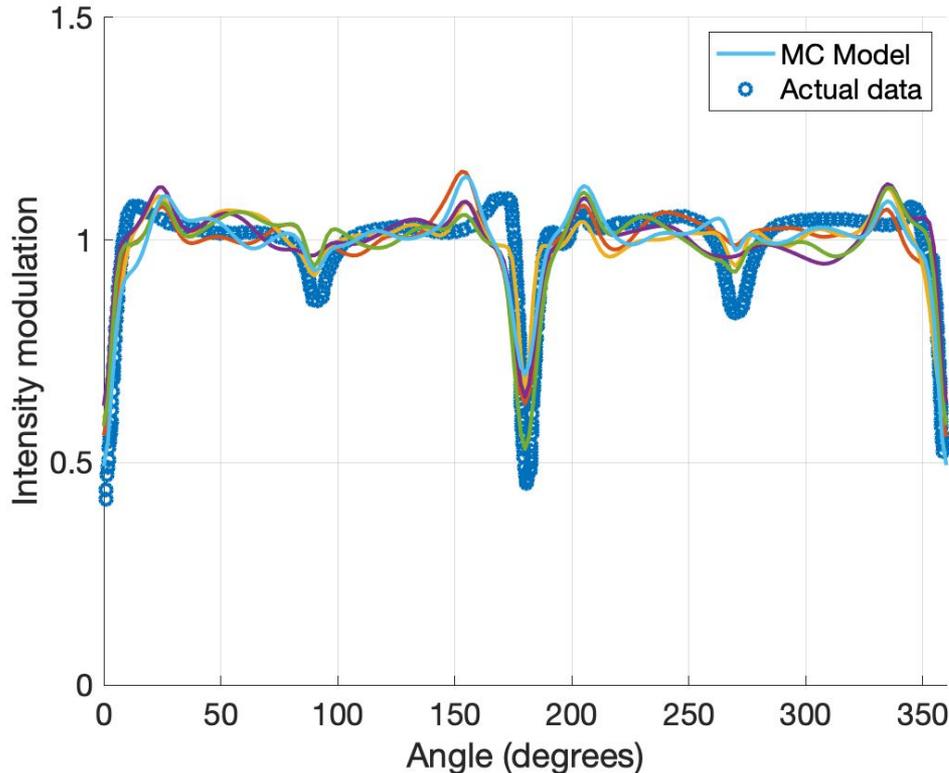
**Overall we need to reduce both thermal lens and surface distortion across the full aperture!
A challenging TCS problem...**



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Adding TCS variations (based upon real systems)

Ring Heater axial variations



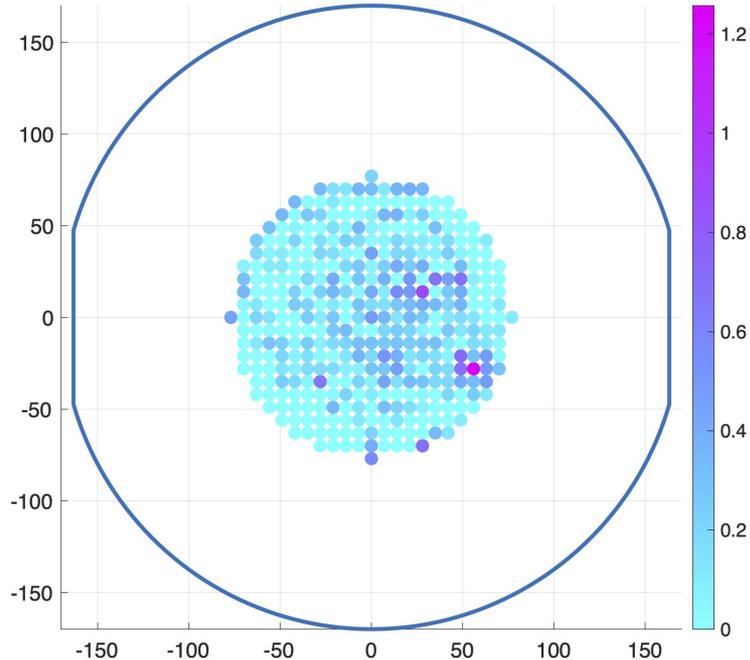
CO2 Laser (approximations)

Parameter	Variation
Alignment to mask*	$\pm 3\text{mm}$
Beam size	$\pm 5\%$
Magnification	$\pm 5\%$
Alignment to CP	$\pm 4\text{mm}$

* Referenced to full-size heating beam at CP

Adding TCS variations (based upon real systems)

H1ITMX: t0 = 1333923804. Cool down fit. Total power absorbed = 52.1mW

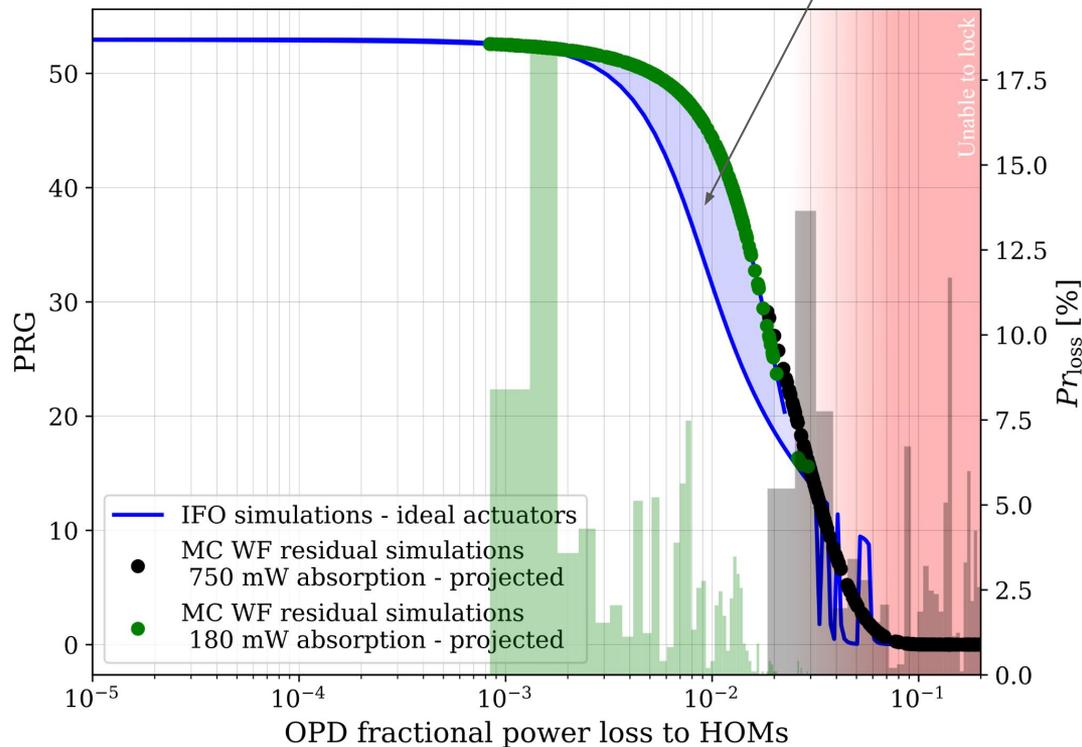


- Non-uniformity observed in recorded in Hartmann wavefront sensor
 - Non-uniform absorption on larger spatial wavelength scale (> 2 cm)
 - Uncertainty in sensor
- **MC data set include variation in absorption point-to-point:**
 - 68%: 0.5 ± 0.05 ppm
 - 27%: 0.5 ± 0.15 ppm
 - 5% : 0.5 ± 0.5 ppm

Preliminary results: Monte Carlo simulation

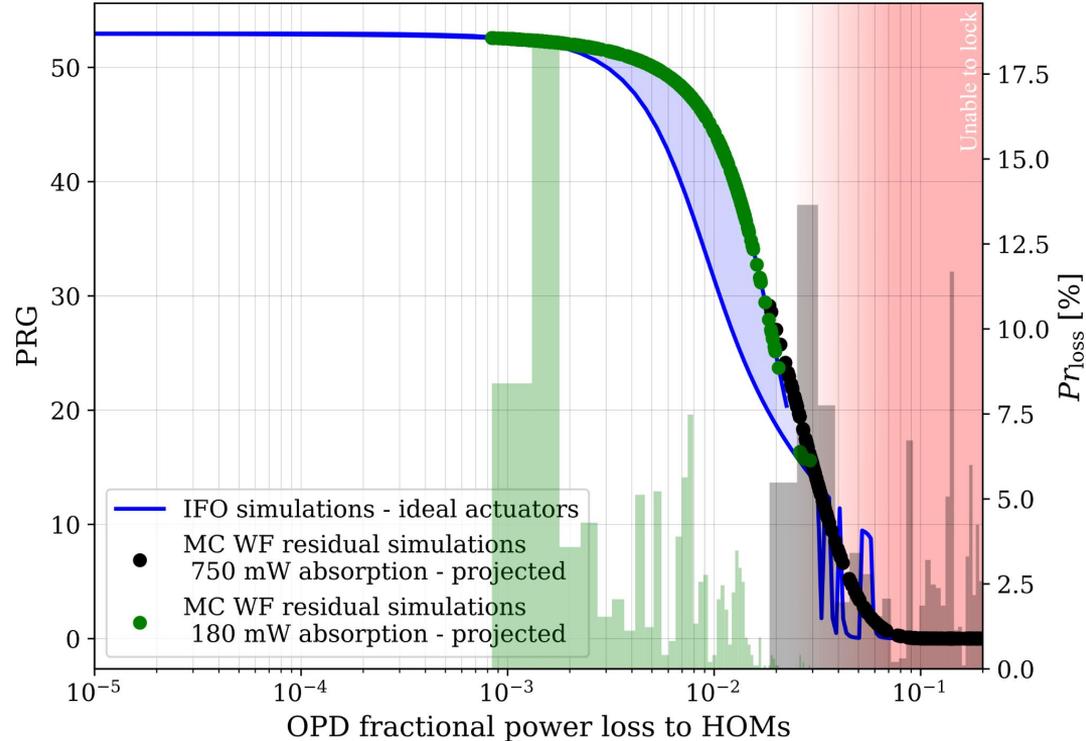
Variations dependent on TCS configurations, i.e. residual spatial structure

- For each optimised map: compute fractional power loss to HOMs
- Plot PRG as a function fractional power loss
- Compute optimised maps and their fractional power loss from Monte-Carlo dataset
- **Project MC data to the trend obtained from IFO simulation**



Preliminary results: Monte Carlo simulation

- At 750 mW HR absorption distortion, HOM loss from OPD is most likely 2-5%
→ **PRG drops to 5 - 10**
- **Couldn't find operating point to lock in many cases**



Preliminary results: Monte Carlo simulation

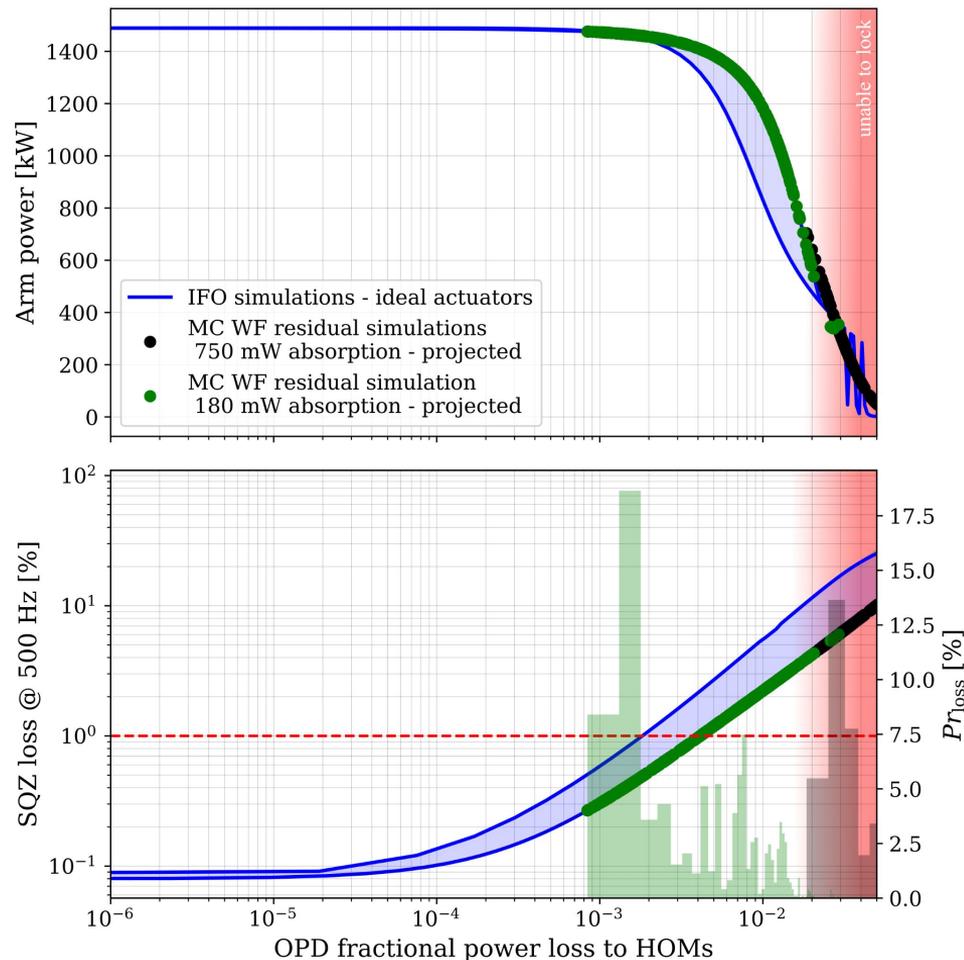
At 750 mW absorption:

- **SQZ loss @ 500 Hz > 5% in all cases**
- No self-consistent solution that results in 750 mW absorption

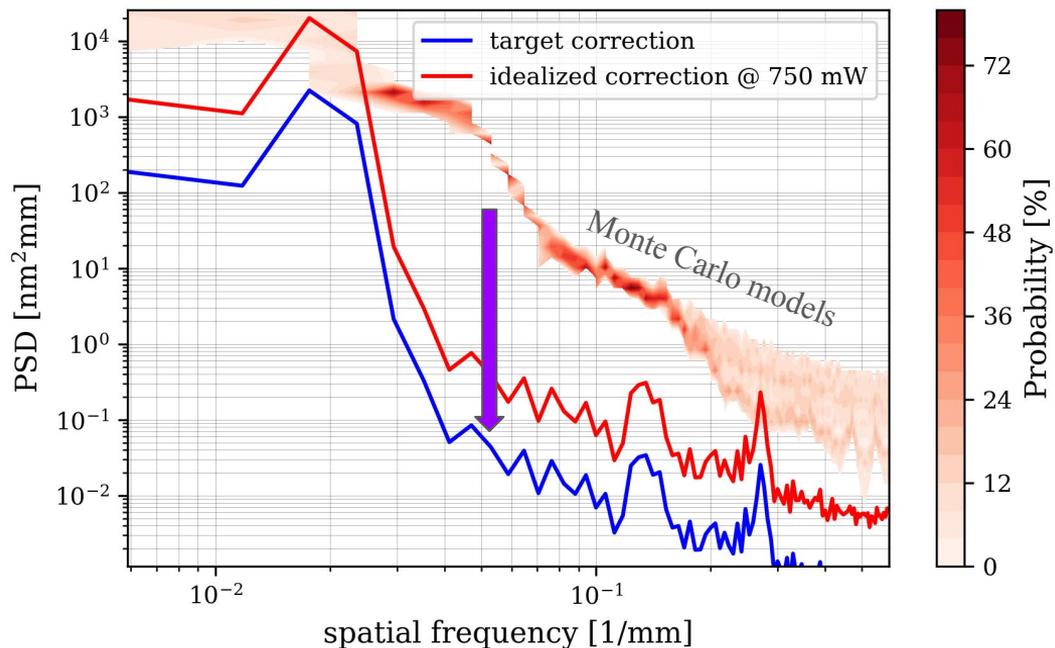
Require a self-consistent solution where the arm power achieved can generate the right residual lens that allows such arm power (sufficient PRG and arm gain)

* Preliminary results (for 200 W injection)

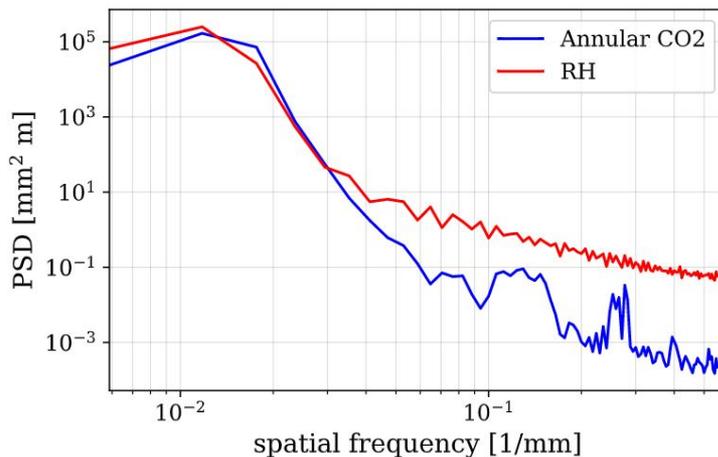
Absorption	0.5ppm	1ppm	1.5ppm
SQZ Loss	~4%	7%	7.2%
Arm Power	~1000kW	680kW	450kW



What is our cancellation capability?



- Errors in actuators result in excess of distortion in spatial wavelength band between 5 mm - 3 cm
- Light scattered from structures of this scale remains inside optical cavity and interact with main IFO beam → complicated and hard to predict behaviour
- **No existing actuator designed to target this band.**



Continued R&D

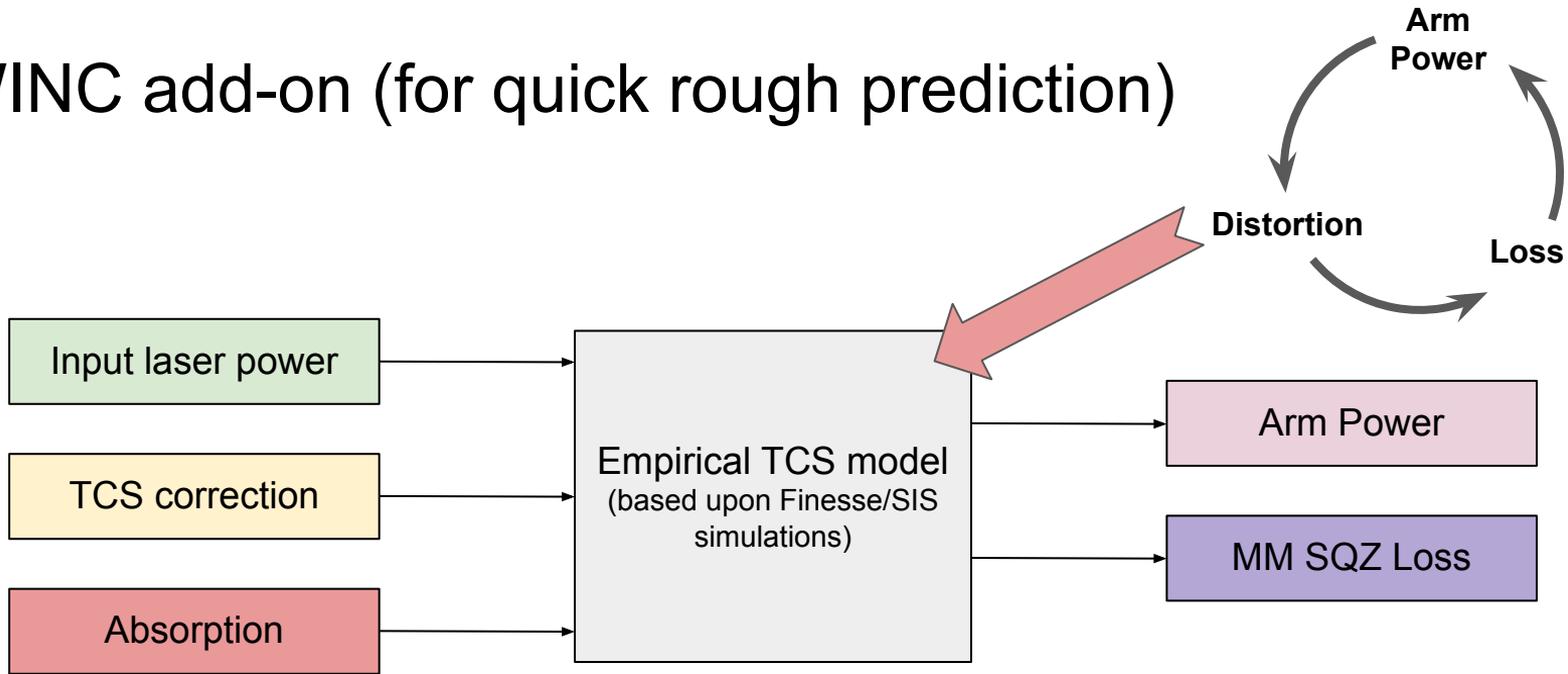
- **MC models:**
 - Working with the sites for better representation of errors in actuators/ sensors
 - Run SIS/ Finesse with MC dataset (rather than just projecting)
- **Full IFO models:**
 - Explore differential effects
 - Noise coupling (intensity noise/ frequency noise)
 - Effects on control signal
- **Transient dynamics:** varying thermal state of test masses → IFO beam changes dynamically → change thermal state
 - Incorporate FEA into SIS/ Finesse to solve simultaneously
 - Simulate and compare to measured transient response (power monitoring/ wavefront sensing channels)
- **O4 model:**
 - Focus back on O4 IFO model to verify simulation
- **A# TCS requirement on sensing + actuating:**
 - Set requirements on errors of TCS actuators
 - Optimise new actuators (front surface heaters/ CO2 upgrade) for full aperture correction
 - Developing correction capability for medium spatial wavelength (1-7 cm)

Key take-away messages

- Existing TCS is not ready for correction at 1.5 MW, will need a factor of 20-30 of distortion suppression
 - Single-pass OPD loss $\lesssim 0.2\%$ for both 1.5 MW arm power + 1% SQZ loss at 500 Hz
- **We're yet to find a robust TCS solution that supports A# target performance**
- Significant improvement in sensing is required to reliably correction out to at least twice IFO beam size
- Actuation at medium spatial wavelength is required to suppress OPD loss to required level

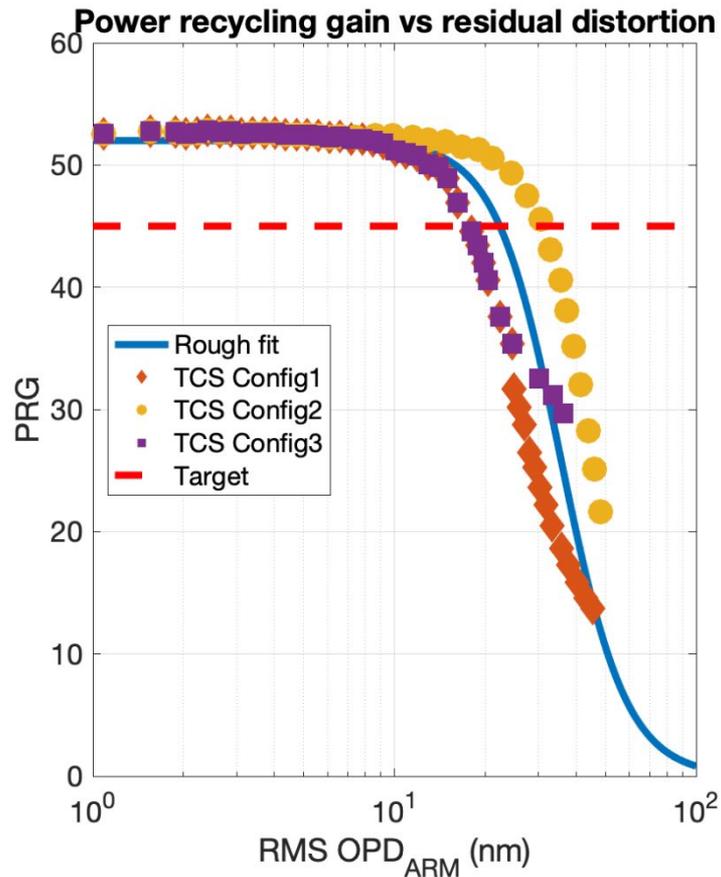
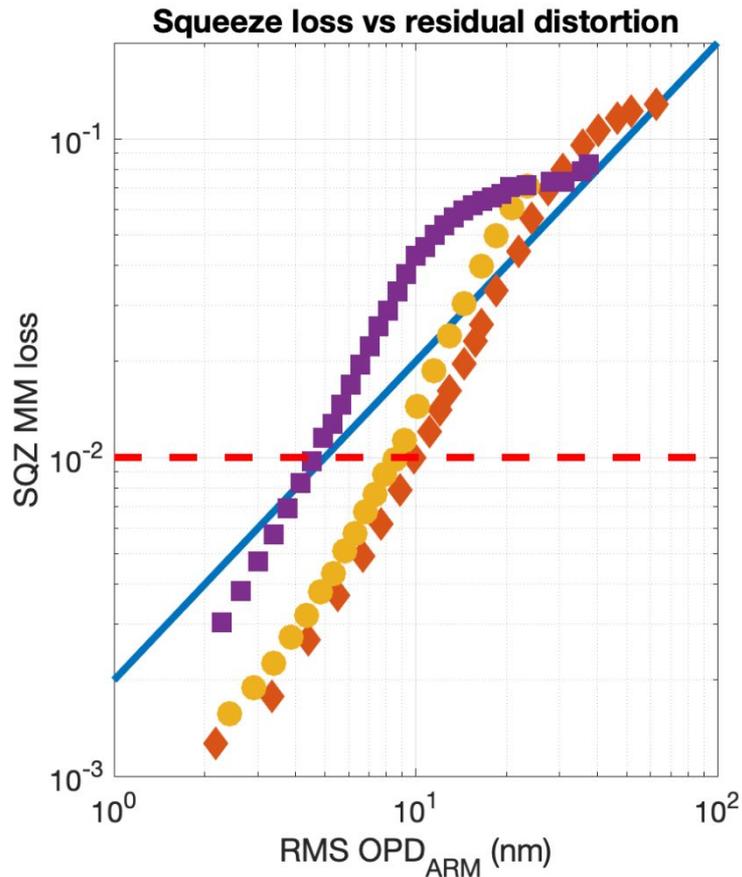
SUPPLEMENT SLIDES

GWINC add-on (for quick rough prediction)

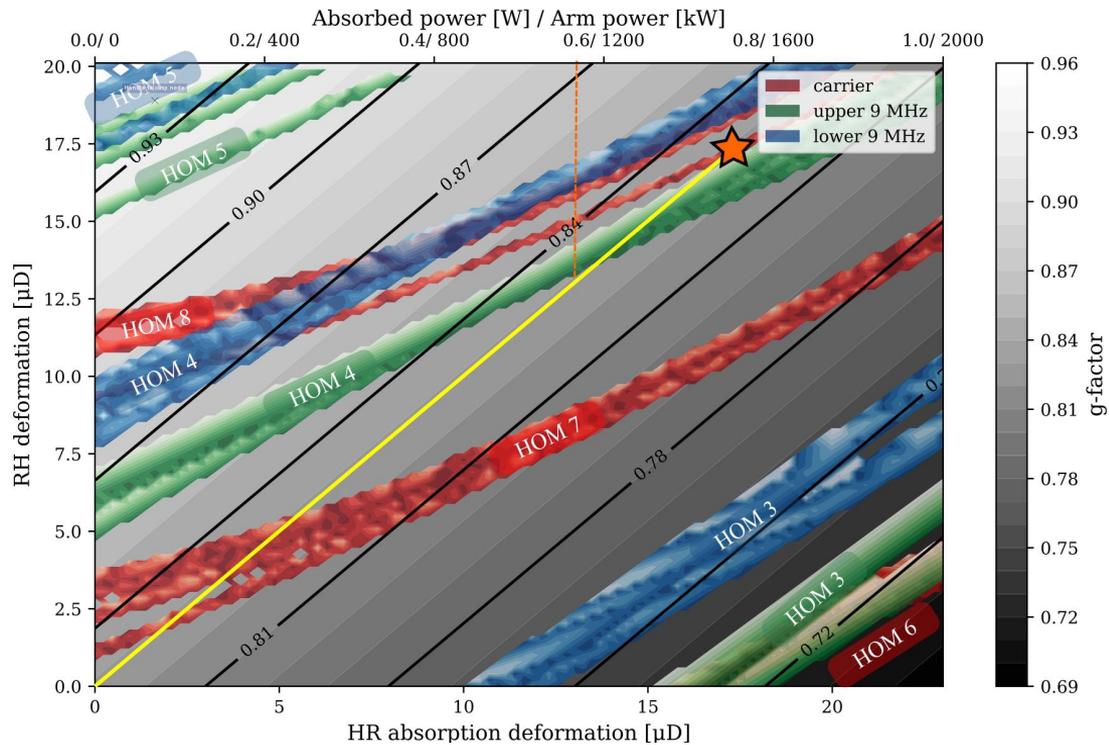
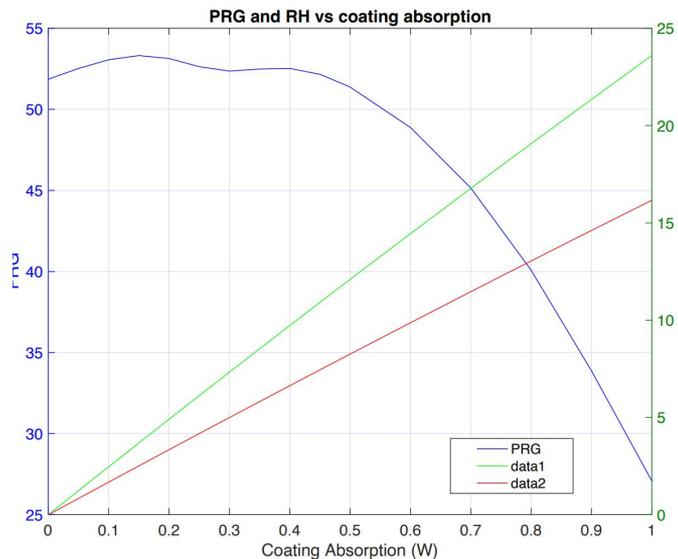


- Code roughly predicts self-consistent IFO performance
- (based upon simulation data).
- Incorporates real simulation data without GWINC having to run full Finesse/SIS

GWINC add-on (empirical data)



Perfectly removal of thermal lens with CO2



Effects of changing larger aperture

